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ACTIVATION DOSE RATE IN ACCSESS TO THE INNER DETECTOR

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ISTC Project #1800-p

Abstract

The present note reports on the results obtained in evaluating activation dose rate for long-access scenario to the inner detector. Contributions of individual materials/systems to activation dose rate are studied. Activation dose rate fields for different opening layouts are calculated.

Moscow, 20 June 2002

1. Introduction

Being operated in harsh radiation environment, the ID detector is to be activated to a significant level that makes problems for maintenance procedures. Induced radioactivity is produced by elementary particles and depends on flux, energy spectra of the particles, activation cross-section, type and mass of irradiated material, exposure time and time after shut down.

Interactions of hadrons with stable nuclei produce most contribution to induced radioactivity. From the methodical viewpoint, its is convenient to divide the energy range onto two sub-ranges: (1) from thermal energies to 20 MeV, and (2) above 20 MeV. The point is that different processes of radionuclide production predominate in the energy ranges. At energy below 20 MeV, neutron induced reactions like (n,γ) , (n,p), (n,α) , and (n,2n) predominate. While, at energy above 20 MeV hadron-induced spallation reactions (x,Spall), were X is proton, neutron, Pi+, or Pi-, are most important. The division is also convenient due to different representation and availability of activation cross-sections. Neutron cross-sections are studied well enough for energy region below 20 MeV, as they are widely used in reactor applications. For energy above 20 MeV activation cross-sections are studied in less detail. As a rule, only proton cross-sections are studied well enough and used as estimation for other hadrons— neutrons and pions.

The note reports on the results achieved during the implementation of the ISTC #1800-p project. The basic aim for the note is to present preliminary evaluation of activation dose rate in the ID long-access scenario on the base of previously developed activation code and associated data sets.

The results reported in the note should be treated as preliminary estimation because the ID design is not yet finalized and a great attention is made to outline the need for more correct estimation of material inventory.

In the general long-access scenario [1] the following systems will contribute to radiation environment: LAr Barrel and EndCap Calorimeter, Inner detector beam-pipe (VI), LAr beam-pipe (VA), Pixel Detector, Semiconductor Tracker (SCT), Transition Radiation Tracker (TRT), and their services. Activation dose rate field produced by every separate system/subsystem is calculated for different exposure and cooling time assumptions, but due to extremely large volume of the obtained data here we give only summary results. A more detailed data is available and may be useful for estimating doses in scenarios involving disassembly of the inner detector. As soon as such scenarios will be developed, the activation dose rate fields at any dismantling step may be easily got as superposition of doses from the systems which are still in place.

All the results are normalized to nominal beam-luminosity 10^{34} cm⁻²s⁻¹.

2. The simulations

2.1 Induced activity

It is convenient to use activation integral (production rate) for calculation of induced activity. The integral, calculated per one target nuclear, shows the rate of a nuclear reaction:

$$q = \int_{0}^{\infty} \sigma(E) \varphi(E) dE$$

where, $\sigma(E)$ - activation cross-section, $\varphi(E)$ - flux of particles.

Having solved the balance equation for the number of radioactive nuclei, one could come to the formula for activity A, Bq per unit volume

$$A_{\rm v} = nq(1 - \exp(-\lambda T))\exp(-\lambda t) \tag{1}$$

where λ is the decay constant, $\lambda = \ln(2)/T_{1/2}$ and $T_{1/2}$ is half life;

n - number of target nuclei per unit of volume;

T - is exposure time in the steady flux;

t - time after shut down.

In (1) we disregard any burning-out processes for both stable and target nuclei. The same expressions one could formulate for the daughter radioactive nuclei produced by radioactive decay of radionuclide - the product of nuclear reaction. Practically, it is enough to consider a mass-chain of three radioactive nuclei, as there is not a radionuclide with half decay exceeding few hours, which would have a longer mass-chain.

In the case the flux (luminosity) cannot be considered as steady in time, its possible to approximate it with a step-wise function of time. So that, the formula (1) will transform into the following:

$$A_{v} = \frac{nq_{nom}}{W_{nom}} \left\{ \sum_{j=1}^{J} W_{j} \left(1 - \exp(-\lambda \Delta T_{j}) \right) \exp\left(-\lambda \left(t + T - \sum_{i=1}^{j} \Delta T_{i} \right) \right) \right\}$$
(2)

where q_{nom} - is activation integral calculated for the nominal W_{nom} luminosity; W_j – luminosity during the time period ΔT_j ; $T = \sum_{i=1}^{J} T_j$ - full exposure time.

Number of target nuclei per unit volume in formulas (1) and (2) are calculated using:

$$\boldsymbol{n} = P \rho \, N_A / A, \tag{3}$$

where, P - natural abundance of the isotope in the material; ρ - density; N_A - Avogadro constant; A- atomic weight of the element.

Being defined as number of decays per second (Bq), activity is not a really convenient value. Activation processes results in great many radionuclides, which properties vary greatly. Since every material (and subsistem) in every particular moment of time will have a unique radinuclide inventory, it is impossible to conclude which of them is more dangerous by their activity only. A more convenient value is the so-called "gamma-equivalent" defined as the product of gamma-factor Γ by activity. Gamma-equivalent k_e , Sv.m²s⁻¹, is equal to the dose rate from a point-wise radionuclide source with activity *A* at the distance 1 m without any shielding.

$$k_e = A \Gamma_H$$
 ,

 $\Gamma_{H_s} \frac{\text{Sv} \cdot \text{m}^2}{\text{Bq} \cdot \text{s}}$, is "gamma-factor", which is constant for a given radionuclide emitting I

gamma rays with different energy $E_{0i},\,\mbox{MeV}$ and absolute intensity $n_i,\,\mbox{photons}$ per decay:

$$\Gamma_{H} = \frac{\sum_{i=1}^{I} \left(E_{0i} n_{i} \mu_{en,m}^{tiss}(E_{0i}) w \right) 1.602 \cdot 10^{-13}}{4\pi}$$
(5)

where $\mu_{en,m}^{tiss}(E_{0i})$ - mass energy attenuation coefficient for energy E_{0i} emitted by the radionuclide in the biological tissue, m²/kg;

w= 1 Sv/Gy - tissue weighting factor for photons; Factor 1.602E-13 is used to transform energy E_{0i} from MeV to Joles.

If the activated material contains more than one radionuclide, then the gammaequivalent will be the sum for all the radionuclides.

Since the gamma-equivalent is defined as dose rate from point-wise radionuclide source, it is quite a convenient value to compare radioactive sources of arbitrary radionuclide inventories. In addition, if one can disregard self-attenuation of photons in a source of complex geometry, the dose rate will correlate with the total gamma-equivalent¹.

The described methods for simulation of induced activity and gamma-equivalent have been implemented in the ACTIVATION-2 code [2,3]. In addition, the code allows to calculate a distributed volume source of photons, which is used in the study as input for simulation of photons transport with radiation transport codes DOT-III [4]. The ACTIVATION-2 code is equally applicable for study of both low energy neutrons and high-energy hadron activation if relevant group activation cross-sections libraries are available.

2.2 Dose rate

Both simple engineering methods and radiation transport codes are used in the present study to simulate dose rate fields. Engineering methods are based on simplification of real geometry and radiation source distribution that enables an analytical solution. A complex geometry can be represented as a set of sources of simple shape and dose rate will be the sum over the sources. Being properly used, engineering methods allow to get rather a precise estimation for dose rate. Though applicability of every particular method is limited, and its use must be justified on case-by-case basis. If geometry is complex enough or radiation source is not uniform, the only way to get correct solution is to use venerable codes for simulating radiation transport in real geometry. In this study we use DOT-III two-dimensional discrete ordinate radiation transport code.

The average density of material in the Inner Detector is rather low. As a result, one can disregard attenuation of gamma radiation in materials of the detector. To estimate dose rate from VI beam-pipe, VA beam-pipe, Pixel, SCT, TRT, and their services we use the following engineering method.

An Inner Detector sub-volume was represented as a set of thin circular radiation sources with the center positioned on the Z-axis and dose rate in a point (Z_0,R_0) is sum of contributions from all the sources:

$$H = 3600 \sum_{i} \frac{k_{i}}{\sqrt{\left(R_{0}^{2} - R_{i}^{2}\right)^{2} + 2\left(Z_{0} - Z_{i}\right)^{2}\left(R_{0}^{2} + R_{i}^{2}\right) + \left(Z_{0} - Z_{i}\right)^{4}}},$$
(8)

where \dot{H} - equivalent dose rate, Sv/h, k_i is gamma-equivalent of source *i*, Sv.m²/s;

 R_i and Z_i -radius of the ring and its position along z-axis, m.



¹ Dose from localized source correlates with total gamma-equivalent; dose on the surface of thick (with considerable self-absorption) source correlates with specific gamma-equivalent; dose rate from extended low-density source (negligible self-absorption) correlates with volumetric gamma-equivalent.

At that the doses will be somewhat conservative as no attenuation of gamma radiation in the source was taken into account. In addition, one should carefully consider partitioning of the source– finite size of Z/R mesh should be much less than the distance to the point were the dose is calculated (because dose rate for $Z_i=Z_0$ and $R_i=R_0$ is infinitely high). As a result, dose rate may be overestimated in the region close to the source surface by some 30%.

Dose rate fields from LAr calorimeter were calculated with DOT radiation transport code and DLC-23/CASK cross-section library [5]. Calculations were done in P_3 approximation of cross-section angular dependence and S_{16} flux angular mesh with distributed photon source simulated by ACTIVATION-2 code.

3 Input data

In order to simulate induced activity one should know:

- flux and spectra of incident particles;
- cross-section of nuclear reactions producing radioactive nuclei;
- concentration of target nuclei and the geometry;
- operation scenario: time of operation *T* and time of cooling *t*.

3.1 Hadron Fluxes

Fluxes in the region $0 \le R \le 12$ m, $0 \le Z \le 24$ m were produced by Mike Shupe with GEANT/GCALOR. The following data together with a readback procedure are available [6]:

- Fluxes with step by z-axis $\Delta Z=10$ cm and step by r-axis $\Delta R=0.1$ cm (0<R<4 cm), $\Delta R=1$ cm (4<R<120 cm), and $\Delta R=1$ cm (120 cm<R)
- 1. High energy neutrons above 20 MeV;
- 2. Fast neutrons 2.19 MeV to 20 MeV;
- 3. Intermediate neutrons 3.78 keV to 2.19 MeV;
- 4. Moderated neutrons 0.414 eV to 3.78 keV;
- 5. Thermal neutrons 10E-5 to 0.414 eV;
- 6. Protons above 20 MeV;
- 7. Pi minus above 20 MeV;
- 8. Pi plus above 20 MeV;
- 9. Stars, threshold 50 MeV.
- Neutron spectra on 10 cm x 10 cm grid (R< 50 cm) and 100 cm x 100 cm (0<R< 500 cm) grid, 61 energy groups.
- Charged hadron spectra on 10 cm x 10 cm grid (R< 50 cm) and 50 cm x 50 cm (0<R< 500 cm) grid, 21 energy groups:
- 1. protons,
- 2. π -pions,
- 3. π + pions.

The data was calculated for baseline geometry of November 2001.

3.2 Cross-sections

Cross-sections of nuclear reactions producing radioactive nuclei are usually available in form of data libraries.

Historically, neutron cross-sections, ranging from thermal energies up to 20 MeV,

are studied rather well, because they are extensively used in fission reactor applications. There are a number sources available, e.g ENDF, JANDL, IRDF.

Calculated proton cross-sections for threshold reactions are available up to energy 200 MeV from MENDL-2 data library [7]. Proton reaction data up to energy 10 GeV are also available in the form of experimental or calculated data compilations for a limited list of materials [8,9].

Cross-section data set for protons was prepared in the same energy group structure as flux spectra. By now the data set includes Be, C, N, O, F, Al, Ar, Ti, Mn, Fe, Ni, Cu, Au, Pb. For other elements we use cross-sections of material with a most close atomic number. For example, in the study we use cross-sections for Mn instead of Cr, Cu instead of Zn, and Pb instead of W.

There were no pion activation cross-sections data found so far. For the purpose of this study, proton cross- sections are used for all hadrons with energy above 20 MeV. The estimation is rather valid for neutrons and results are certainly conservative for pions (up to 30%), that can be concluded from the energy dependence of hadrons inelastic cross-sections.

3.3 Geometry and Concentrations

3.3.1 LAr Calorimeter

LAr calorimeter geometry/materials were adopted from geometry/material description file (version of November 2001) used by Mike Shupe for hadrons transport calculation with GEANT/GCALOR [6].

Barrel calorimeter geometry description and material composition are given in Tables 1 and 2. EndCap calorimeter geometry description and material composition are given in Tables 3 and 4.

The GEANT/GCALOR geometry data file is rather comprehensive to reflect all the distinct features relevant to radiation transport, but for the purpose of activation study it is desirable to know concentration of some minor chemical element (impurities) as well. Concentration of the impurities such as Co, Ag, Sb is negligible for radiation transport, but activation of the impurities by thermal neutrons result in production of long-lived radionuclides and may dominate dose rate in some cases. Since no concentrations of the impurities are available, we have to use the following assumptions:

- Cobalt content is a usual impurity to nickel. In the study we assume that cobalt makes up 2% of nickel weight. The value is adopted on the base of analysis of Co/Ni ratio in stainless steels and assumed to be the upper limit. Though the real content of cobalt may vary within a factor of 10 even in steel. This results in significant uncertainty for great cooling/exposure times, as half decay time of ⁶⁰Co (the only important radionuclide produced by low energy neutrons in cobalt) is 5.27 year.
- Silver and antimony are usual impurities to copper and lead. There is no data available on concentration of the elements in copper to produce any secure assumptions. For the lead we use concentrations adopted from Chemical Lead UNS L51120 specifications (Pb>99.9%, Ag 0.002 0.02%, As+Sb+Sn<0.002%, Bi<0.005%, Cu 0.04 0.08%, Fe<0.002%, Zn< 0.001) [10]. Though previous study has shown that such concentrations do not produce significant contribution to activation [11].

3.3.2 ID beam-pipe (VI)

Geometry of VI was adopted from LHCVC1I_0003 drawing. Geometry description of VI is given in Table 5. Materials are beryllium and Aluminum Alloy 5000 Series. Composition of aluminum alloy was adopted from specifications available on [10]: Al 94.8%, Cr - 0.05 - 0.25%, Cu<0.1%, Fe< 0.4%, Mg 4%, Mn 0.4 – 1%, Si<0.4%, Ti<0.15%, Zn<0.25%.

3.3.3 LAr beam-pipe (VA)

Geometry of VA was adopted from LHCVC1A_0001 drawing. Geometry description of VA is given in Table 6. Material is 316L stainless steel. Composition of stainless steel was adopted from UNS S31603 specification [10]: C 0.03%, Cr 16-18%, Fe 62-69 %, Mn 2%, Mo 2-3%, Ni 10-14%, Si 0.75%. Concentration of cobalt was assumed to make up 2% of nickel weight.

Previous study has shown that the dose rate from stainless steel VA will be extremely high – up to several mSv/h [12]. Possible design/material changes are being studied currently to decrease the doses. So the results of VA calculations should be considered as preliminary.

3.3.4 Pixel detector

Geometry and composition of the Pixel detector was taken from inventory of metals spreadsheet produced by Marco Olcese [13]. The geometry and composition for the Pixel detector are given in Table 7 and 8. Concentration of cobalt was assumed to make up 2% of nickel weight.

The inventory is not comprehensive -- non-metallic elements such as carbon and silicon were omitted. Though content of the materials can be recalculated from file prepared by Ivan Bedajanek [14], which gives us approximately 0.6 kg of silicon and 30 kg carbon. Content of silicon is negligible as compared to aluminum – 26 kg in pixel (without type 2 services). Content of carbon is not negligible, but activation in carbon is by order of magnitude less then in aluminum [report 1] and will hardly produce a noticeable contribution.

3.3.5 SCT

SCT geometry and materials were adopted from the file prepared by Ivan Bedajanek [15]. Geometry and materials of SCT Barrel are given in Tables 9 and 10. Geometry and materials of SCT Forward are given in Tables 11 and 12. Concentration of cobalt was assumed to make up 2% of nickel weight. Major source of Ni (and Co) is nickel-plated Type 2 cables and stainless steel cooling pipes.

The description of SCT Forward is far from being complete. Density of materials in forward modules was assumed to be the same as in barrel modules. A more correct estimation for material inventory is highly desirable.

3.3.7 TRT

TRT geometry and materials were adopted from the file prepared by Ivan Bedajanek [16]. Geometry and materials of SCT Barrel are given in Tables 13 and 14. Concentration of cobalt was assumed to make up 2% of nickel weight. Major source of Ni (and Co) is nickel-plated Type 2 cables and stainless steel cooling pipes.

3.4 Operation scenario

Two scenarios of LHC operation were assumed for the purpose of the study.

- LHC is operated at high luminosity during T=100d.
- LHC is operated for 10 years-- 120 days per year run at high luminosity and the rest of the year LHC is shut down.

In the both cases, activation was studied for cooling time t= 1d, 3d, 5d, 7d, 15d, 30d, and 100 d.

4. Results

4.1 Activation of materials/systems

Results of activation study of Inner Detector systems and VA beam pipe are given in Tables 15-24. The results are expressed in terms of gamma-equivalent induced by lowenergy neutrons and high-energy hadrons. Contribution of every individual material is given in percents to subtotal (neutron or hadron activation). The last row is the total gamma-equivalent induced by both neutrons and hadrons. The results are given for T=100 days, 10 years and t= 1, 3, 5, 7, 15, 30, and 100 days after shutdown. Since the volume of information is too large, here we have to limit consideration to cooling time t= 7 days.

Activation in VA beam-pipe section is at least by order of magnitude larger than any ID subsystem and needs special consideration. We advisedly exclude it from the further analysis of activation because VA will be removed to allow long access to the Inner Detector. Nevertheless, contribution of VA to dose rate around ID is taken into account (see section 4.2).

Distribution of gamma-equivalent among ID systems is given on Fig. 1. On can see that activation is distributed rather uniformly amongst the systems with the only exception for VI beam-pipe. Activation in every individual system after 10 years of operation is about twice as high than after 100 days (high luminosity was assumed for both operation scenarios, see 3.4).

Despite total gamma-equivalents of all systems is rather similar, it is hardly possible to conclude that all the systems will produce the similar dose rate. In addition to total gamma-equivalent, one should take into account also dimensions of the system, distribution of activity over the volume, and distance to the accessible point. From a very general idea, it is very likely that services will produce greater contribution to the dose rate, as their volume is much smaller.

Contribution of low-energy neutrons and high-energy hadrons to activation of separate ID systems is given on Fig. 2. One can see that activation in every individual system is dominated by hadrons. Contribution of low energy neutrons to total activation depends on particular system and also varies with operational scenario. For example, relative contribution of neutrons grows up with operation time for all the services and either remains the same or decreases for detectors (TRT, SCT, and Pixel).

Contribution of individual materials to total gamma-equivalent induced in the Inner Detector is given on Fig. 3. The most important materials are aluminum, iron, cobalt, nickel, copper, and silver. At that, low-energy neutrons dominate activation of cobalt and silver. It is interesting to note that amount of cobalt is by 2000 times less than copper (Fig. 4), while their contributions are similar. Such a great relative importance of cobalt can be explained by high thermal neutrons activation cross-section and high gamma-ray emission (2.5 MeV per decay) of the activation product ⁶⁰Co. It is ⁶⁰Co that will dominate activation

for cooling time exceeding 1 year, as its half decay (5.25 year) is rather great comparing to many others activation products.

It is very likely that lack of information on the exact content of cobalt and silver in the Inner Detector materials is a significant source of uncertainty. In the study we assume that content of cobalt is to correlate with nickel. Concentration of cobalt was assumed to make up 2% of nickel weight (or 2000 ppm in stainless steel). Real content of cobalt in stainless steel is unknown and may vary significantly from the assumption. Content of cobalt in other materials is also unknown. For example, an assumption that cobalt content in copper makes up 200 ppm, will increase the present estimation by factor of 1.5. Content of others important impurities in copper are silver and antimony (of order 2000 ppm each) also need to be studied.

4.2 Induced dose rate

Contribution of different ID systems, VA beam-pipe, and LAr calorimeter to total dose rate around Inner Detector for the long accesses scenario are given in Tables 25-36. The LAr End Cap is shifted by 325 cm along Z-axis. The dose rate are given for the following points:

R= 175 mm,	Z= 3340 mm
R= 400 mm,	Z= 3443 mm
R= 700 mm,	Z= 3440 mm
R= 175 mm,	Z= 3800 mm
R= 400 mm,	Z= 3800 mm
R= 700 mm,	Z= 3800 mm

Analysis of the data has shown that the major contributors to the dose rate are VA beam-pipe and LAr End Cap. When the last two are removed, Pixel detector and ID services will determine dose rate.

Additional information on dose rate fields in the long access scenario are given in Addendum 1. The following opening layouts are studied by the moment:

- 1. LAr End Cap shifted by 325 cm along Z-axis, all ID systems and VA beampipe are in place;
- 2. LAr End Cap is removed, all ID systems and VA beam-pipe are in place;
- 3. LAr End Cap and VA beam-pipe are removed, all ID systems are in place;
- 4. LAr End Cap and VA beam-pipe are removed, Pixel Detector and VI are removed, others ID systems are in place;

Other opening layouts are to be studied:

- 5. Pixel and VI, SCT forward, and TRT End Cap with forward services are removed on one side to allow access inside LAr Barrel;
- 6. All ID systems in place except for TRT C.

Dose rate fields from dismantled VA beam-pipe are given in Addendum 2. Dose rate fields from dismantled Pixel & VI beam-pipe are given in Addendum 3. Dose rate fields from LAr Barrel and End Cap are given in Addendum 4.

4.3 Comparison of activation dose rate from SCT Barrel

Doses from SCT Barrel have been estimated by C.Buttar et al in ATL-INDET-2002-013 [17]. Despite the authors have found that SCT Barrel does not pose any serious problems from radiological point of view, the results are valuable for the purpose of comparison with the results of the present study.

Only barrel modules were taken into account in the ATL-INDET-2002-013. The estimation was made at assumption of average beam-luminosity of 5×10^{33} cm⁻²s⁻¹. LHC operation year was defined as 180 days running followed by 185 days of shutdown. Radionuclide production rate for innermost layer of barrel modules was produced with the Monte Carlo particle transport code FLUKA and used for other layers. Gamma and beta dose rate were reported at the distance of 10 cm, 30 cm, and 100 cm from both cylindrical and front surface.

We produced estimation of gamma dose rate from barrel modules taking into account the mentioned assumptions made by C.Buttar et al. The results are given in tables 37-38. Quite a satisfactory agreement (within 20-40%) was found. This gives us some confidence that the data and codes used in the current study are reliable.

5. Conclusions

Major contributors to the dose rate in ID general long access layout are VA beampipe and LAr End Cap. Contact gamma dose rate on the surface of VA makes up to 5 mSv/h for cooling time 5 days. Dose rate near LAr End Cap (without VA) makes up few hundreds μ Sv/h. These will pose serious problems for access to the Inner Detector.

When VA beam-pipe and LAr End Cap are removed, the Pixel detector and ID services will determine dose rate. Gamma dose rate near Pixel PP1 may exceed 100 μ Sv/h for cooling time 5 days.

The current study has shown that spallation activation induced by high-energy hadrons produces dominant contribution to gamma dose rate from the Inner Detector. Low-energy neutrons produce a comparable contribution to activation of ID services after a long operation time and cooling time exceeding few weeks.

The most important ID materials contributing to gamma dose rate are aluminum, iron, cobalt, nickel, copper, and silver. Low-energy neutrons dominate activation of cobalt and silver, while high-energy hadrons dominate activation of aluminum, nickel, and copper.

Major sources of silver are SCT modules and electronics. Silver inventory seems to be incomplete and needs further verification, especially for SCT Forward. Another possible source of silver are copper cables, as silver is usual impurity in copper.

Major source of cobalt is stainless steel and other nickel-based materials. Actual content of cobalt is unknown that may result in considerable uncertainty of dose rate estimations from ID services for cooling time exceeding few months. Though, the dose rate from the services after 100 d cooling does not exceed few tens μ Sv/h.

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Fig. 1 Gamma-equivalent vs. ID subsystems at cooling time t=7 days





Fig. 2 Gamma-equivalent induced by neutrons/hadrons in ID subsystems for exposure time (a) T=100 d and (b) T=10 y, cooling time t =7 days



Fig. 3 Gamma-equivalent vs. ID materials cooling time t=7 days



Fig. 4 Material break down of Inner Detector

Geometry description of the LAr Barrel Calorimeter

El EMENT	Matorial					
			72[om]		D2[om]	Waterial
Perrel inner warm well	1		204			
Darrel inner vall wall eastion 1	1	0	304	110	120 5	
Barrel inner cold wall section 1	2	7.5	1.5	134.1	100.0	
Barrel inner cold wall section 2	3	7.5	40	134.9	100.0	
Barrel inner cold wall section 5	4	40	105	130.0	100.0	
Darrel inner cold wall section 4	5	112	190	130.4	130.5	
Barrel inner cold wall section 5	0	195	240	100.0	130.5	
Barrel inner cold wall section of	/	240	302.3	130.0	130.0	
Barrel inner cold corner section 1	0	302.3	310.1	130.5	100.0	
Barrel inner cold corner section 2	9	205.2	320.3	107.1	150.5	
Barrel cold well and inner costion	10	323.3	320.7	157.1	100.00	
Barrel cold wall end inner section	10	320.7	328.7	100.00	185	
Barrel cold wall end outer section	12	320.7	330.2	100	219	
Solenoid Dreebewer detector	13	0	200	123.1	142.0	
Presnower detector	14	0	300.8	140.5	143.6	PRESHOWER
preshower	15	0	300.8	138.5	140.5	LIQ_ARGON
Middle accordion volume	16	0	134.1	151	197.9	LAr EM 1.8 PB
North accordion volume wedge	17	134.1	145	157.2	197.9	LAr EM 1.8 PB
before eta=.8						
	18	145	155	168.9	197.9	LAr EM 1.8 PB
	19	155	165	180.1	197.9	LAr EM 1.8 PB
	20	165	175.8	191.5	197.9	LAr EM 1.8 PB
North accordion volume wedge after eta=.8	21	134.1	145	151	157.2	LAR EM 1.2 PB
	22	145	155	151	168.9	LAR EM 1.2 PB
	23	155	165	151	180.1	LAR EM 1.2 PB
	24	165	175.8	151	191.5	LAR EM 1.2 PB
North accordion volume cylinder after eta=.8	25	175.8	300.8	151	197.9	LAR EM 1.2 PB
North accordion end volume (tapered)	26	300.8	315	151	197.9	LAR EM 1.2 PB
Accordion front materials	27	0	300.8	144	151	EM IN TAB
Accordion exit materials	28	0	315	197.9	214	EM OUT TAB
Barrel outer cold wall	29	0	299.6	214	217	ALUMINUM
Barrel outer cold wall vertical	30	292.6	299.6	217	228	ALUMINUM
Barrel cold wall flange	31	299.6	322.7	221.5	226.5	ALUMINUM
Barrel cold wall flange connector	32	322.7	331.7	219	228	ALUMINUM
Liquid at end of EM accordion	33	315	326.7	156.55	219	LIQ ARGON
Barrel outer warm wall	34	0	285	222	225	ALUMINUM
Barrel outer warm vertical	35	285	290	222	271.1	ALUMINUM
Barrel outer warm horizontal	36	285	339	271.1	277.5	ALUMINUM
flange						
Barrel warm flange connector 1	37	334	339	251.6	271.1	ALUMINUM
Barrel warm flange connector 2	38	339	340.5	251.6	269	ALUMINUM
End warm vertical bulkhead	39	336.7	340.5	185	251.6	ALUMINUM
	40	338.5	340.5	142	185	ALUMINUM
	41	339.3	340.5	122.02	142	ALUMINUM
Barrel warm front corner	42	315	340.5	120.8	122.02	ALUMINUM
Barrel warm front corner	43	312.5	315	115	117.1	ALUMINUM
Barrel warm front corner	44	304	316	117.3	120.8	ALUMINUM
Barrel warm front corner	45	304	306.5	115	117.3	ALUMINUM

	MATERIAL											
ELEMENT	ALUM	COILMIX	PRE	LIQ	LAr EM 1.8	LAR EM 1.2	EM IN TAB	EM OUT				
			SHOWER	ARGON	PB	PB		TAB				
Н		1.02E-03	6.96E-03		1.81E-03	2.98E-03	6.24E-03	3.71E-03				
С			3.06E-03		2.82E-03	1.65E-02						
0		4.80E-03	7.91E-03		8.75E-04	9.60E-04	2.93E-02	1.75E-02				
Si	2.45E-04	1.39E-03	2.14E-03		2.54E-04	2.78E-04	8.51E-03	5.06E-03				
AI	6.02E-02	3.15E-02										
Ar			6.49E-03	2.11E-02	1.25E-02	1.37E-02	3.35E-03	8.96E-03				
Ca		6.91E-04	1.06E-03		1.26E-04	1.38E-04	4.22E-03	2.51E-03				
Ti	5.37E-05											
Cr	6.60E-05				1.70E-03	2.20E-03		4.25E-03				
Mn	3.12E-04				1.79E-04	2.31E-04		4.47E-04				
Fe	1.23E-04				6.24E-03	8.08E-03	1.17E-07	1.56E-02				
Ni					8.78E-04	1.14E-03		2.20E-03				
Со					1.76E-05	2.27E-05		4.39E-05				
Cu	2.70E-05	8.09E-03	5.11E-03		2.29E-05	1.68E-05	4.10E-06	2.03E-06				
Zn	6.56E-05				2.79E-07	2.04E-07	4.98E-08	2.47E-08				
As					2.43E-07	1.78E-07	4.35E-08	2.16E-08				
Ag					3.38E-06	2.47E-06	6.04E-07	3.00E-07				
Sn					1.53E-07	1.12E-07	2.74E-08	1.36E-08				
Sb					1.50E-07	1.09E-07	2.68E-08	1.33E-08				
Pb					8.78E-03	6.43E-03	1.57E-03	7.79E-04				
Bi					4.36E-07	3.19E-07	7.79E-08	3.87E-08				

Composition of LAr Barrel materials

ELEMENT	Element	ELEME	NT GEOME	TRY (ring	g/disk)	Material
	ID	Z1[cm]	Z2[cm]	R1[cm]	R2[cm]	
EC EM inner volume	1	367.7	385	30.7	47	EC EMI
	2	385	402	32.1	56.2	EC EMI
	3	402	419.5	33.5	64.9	EC EMI
EC EM outer volume	4	367.7	385	47	208.9	EC EMO
	5	385	402	56.2	208.9	EC EMO
	6	402	419.5	64.9	208.9	EC EMO
G10 support bars inside EC EM	7	367.7	385	28.9	30.7	G10
	8	385	402	30.3	32.1	G10
	9	402	419.5	31.7	33.5	G10
EC HEC1A volume north	10	426.5	456.7	37	208.9	EC HAD1
EC HEC1B volume north	11	456.7	510.9	47.3	208.9	EC HAD2
EC HEC2 volume north	12	512	610.8	47.3	208.9	EC HAD3
EC front bumper block	13	374.7	379.2	18.5	23.8	G10
EC cylindrical support tube	14	466 85	635	45.7	46.5	ALUMINUM
Liquid argon layer outside the	15	466.85	635	46.5	47.3	
support tube	10	100.00	000	10.0	17.0	
EC support tube back flange at	16	635	644.5	46.5	49.5	ALUMINUM
rear of 5						
EC Plug 1 - main copper	17	627.5	644.5	59	193.5	PLUG BRASS
absorber at back of EC						
EC Plug 2 – small plug at back of	18	610.8	623	47.5	59.5	PLUG BRASS
HEC2 near beam-line						
Cable fill in pocket at back of	19	623	644.5	49.5	59	LAR CABLES
cylindrical transition		004.0	0077			
Liquid argon and cables in front	20	361.2	367.7	30	208.9	LAR CABLES
Liquid argon and cables outside	21	261.2	644 5	208.0	212 /	
the hadronic modules	21	301.2	044.5	200.9	212.4	LAR CABLES
Liquid argon and cables at rear	22	610.8	627.5	69	208.9	LAR CABLES
of HEC2		010.0	021.0	00	200.0	
Liquid argon and cables at rear	23	419.5	426.5	37	208.9	LAR CABLES
of EMEC	-			_		
Liquid argon and cables at rear	24	510.9	512	47.3	208.9	LAR CABLES
of first hadronic compartment						
EC front warm wall	25	350	351.5	18.2	226	ALUMINUM
Poly around beam pipe at front	26	350	362	6	18.2	POLYLITH
of EC (plugging FCAL hole)						
EC flange block at front of 2X	27	351.5	374.7	18.2	19.7	ALUMINUM
(2Y)						
EC warm wall north nearer I.P.	28	374.7	454	18.1	18.5	ALUMINUM
(2X)						
Connecting washer, 2X to 2 (2Z)	29	454	455	5.1	18.5	ALUMINUM
EC inner warm wall	30	454	662.5	4.8	5.1	ALUMINUM
EC outer warm wall	31	351.5	616	223	226	ALUMINUM
EC outer warm wall vertical	32	616	619	223	240.5	ALUMINUM
EC outer warm wall horizontal	33	616	662.5	240.5	247.5	ALUMINUM
flange						

Geometry description of the LAr End Cap Calorimeter

Table 3 (continuation)

ELEMENT	Element	ELEME		TRY (rine	a/disk)	Material
	ID	Z1[cm]	Z2[cm]	R1[cm]	R2[cm]	
EC rear warm wall	34	662.5	668.5	4.8	247.5	ALUMINUM
EC front cold wall	35	354.7	361.2	22.8	217.5	ALUMINUM
EC inner cold wall north	36	464.35	644.5	6.1	6.7	ALUMINUM
EC inner cold wall north front	37	374.7	461.85	26.8	27.8	ALUMINUM
near I.P.						
EC flange	38	361.2	374.7	22.8	27.8	ALUMINUM
EC outer cold wall	39	361.2	619	214	217.5	ALUMINUM
EC outer back corner cold wall	40	619	644.5	214	224.5	ALUMINUM
EC back cold wall	41	644.5	658.3	6.1	224.5	ALUMINUM
EC inner back cold wall	42	658.3	662.5	9.5	13.1	ALUMINUM
EC back cold wall thin section	43	658.3	659	6.1	9.5	ALUMINUM
near beam-ine						
FC EM volume north	44	466.85	532	7.2	45	FC EM
Cold wall in front of EM	45	461.85	464.35	6.1	45.7	ALUMINUM
Liquid argon and cables outside	46	480.5	644.5	45	45.7	LAR CABLES
FCAL						
Liquid argon and cables behind EM	47	532	532.5	7.9	45	LAR CABLES
	48	532.5	577.65	8.9	44	FC HAD1
	49	532.5	577.65	7.9	8.9	COPPER
	50	532.5	577.65	44	45	COPPER
Liquid argon and cables at back of FC H1	51	577.65	580.15	8.6	45	LAR CABLES
	52	580.15	604.7	9.6	44	FC HAD1
	53	580.15	577.65	8.6	9.6	COPPER
	54	580.15	577.65	44	45	COPPER
Liquid argon and cables at back of FC H2	55	604.7	607.2	9.5	45	LAR CABLES
Plug3	56	607.2	639.6	9.5	44.7	PLUG BRASS
Notch	57	639.6	644.5	14.5	44.7	PLUG BRASS
Services in gap between electronics crates and fingers	58	612	667.5	331.3	388	GAP MAT

Geometry description of the LAr End Cap Calorimeter

									L						
ELEMENT	EC EMI	EC EMO	EC HAD1	EC HAD2	EC HAD3	LAR CABLES	PLUG BRASS	FC EM	FC HAD1	POLY LITH	GAP MIX	G10	ALUM	LIQUID ARGON	COPPER
Н	2.8E-02	3.2E-02				6.5E-04	2.0.00			7.7E-02	3.6E-02	1.5E-03			
Li										2.2E-03					
C	2.0E-03	2.3E-03								3.7E-02	2.1E-02				
0						6.2E-03					3.5E-03	1.1E-02			
F										2.2E-03					
Al													6.0E-02		
Si						1.3E-03						5.7E-02			
Ar	1.3E-02	1.3E-02	5.1E-03	5.4E-03	3.0E-03	1.8E-02		3.1E-04	3.3E-03					2.1E-02	
Ca						8.9E-04			7.5E-04			4.0E-02			
Ti													5.4E-05		
Cr											6.3E-03		6.6E-05		
Mn											6.6E-04		3.1E-04		
Fe	4.6E-03	5.3E-03									2.3E-02		1.2E-04		
Ni									1.4E-03		3.2E-03				
Co	1.2E-05	1.4E-05							2.9E-05		6.2E-05				
Zn	3.2E-07	2.8E-07					1.6E-03						6.6E-05		
Cu	2.6E-05	2.3E-05	6.4E-02	6.3E-02	7.3E-02		7.2E-02	7.4E-02	1.1E-02		1.3E-02		2.7E-05		8.5E-02
As	2.8E-07	2.5E-07													
Sb	1.7E-07	1.5E-07													
Sn	1.8E-07	1.5E-07					3.1E-03								
Ag	3.9E-06	3.4E-06													
W									4.2E-02						
Pb	1.0E-02	8.9E-03					7.5E-04								

Composition of LAr End Cap calorimeter

##	Z _{min} , cm	Z _{max} , cm	R _{min} , cm	R _{max} , cm	Material	Mass,	Comment			
						kg				
1	0	343.9	3.38	3.46	Be	1.093	Outer tube			
2	0	355	2.9	2.98	Be	0.970	Inner tube			
3	355	365	2.9	2.98	Al	0.040	Inner tube			
4	350.5	357.5	3.38	3.46	Al	0.032	Outer tube			
5	343.9	350.5	3.38	3.46	Al	0.031	Bellows (*			
6	363.6	365	2.98	4.3	Al	0.114	Flange			
(*	(* - under study now – assumed as tube									

Material zones of the VI beam pipe section (right half)

Table 6

##	Z _{min} , cm	Z _{max} , cm	R _{min} , cm	R _{max} , cm	Material	Mass, kg	Comment
1	365	366.4	2.9	4.3	SS 316L	0.346	Flange
2	366.4	387.6	2.9	2.98	SS 316L	0.063	Tube
3	373.2	373.28	2.98	8.3	SS 316L	0.075	Pump wall
4	373.28	378.8	8.23	8.3	SS 316L	0.206	Pump wall
5	378.8	378.88	2.98	8.3	SS 316L	0.262	Pump wall
6	374.8	378	4.5	4.7	SS 316L	0.317	Pump electrode
7	374.8	378	6.8	7	SS 316L	0.224	Pump electrode
8	387.6	395.8	2.9	3.04	SS 316L	0.472	Bellows
9	395.8	415.1	2.9	2.98	SS 316L	0.045	Tube
10	415.1	423.3	2.9	3.04	SS 316L	0.472	Bellows
11	423.3	855	2.9	2.98	SS 316L	0.045	Tube
12	855	863.2	2.9	3.04	SS 316L	0.317	Bellows
13	863.2	870	2.9	2.98	SS 316L	0.262	Tube
14	868.6	870	2.98	4.3	SS 316L	0.206	Flunge
15	428.9	849	3.92	4	SS 316L	0.075	Tube

Material zones of the VA beam pipe section

Table '	7
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ELEMENT	Element	ELEM		IETRY (ring	g/disk)
	ID	Z1[cm]	Z2[cm]	R1[cm]	R2[cm]
B-layer	1	0	40	4.55	7.4
Layer 1	2	0	40	8.3	11.1
Layer 2	3	0	40	11.7	14.4
Disk 1	4	49	50	8.5	14.8
Disk 2	5	57.5	58.5	8.5	14.8
Disk 3	6	64.5	65.5	8.5	14.8
B-layer end	7	40	44.2	4.55	7.4
Layer 1 end	8	40	44.2	8.3	11.1
Layer 2 end	9	40	44.2	11.7	14.4
Disk 1 cooling connections	10	49	50	14.8	17
Disk 2 cooling connections	11	57.5	58.5	14.8	17
Disk 3 cooling connections	12	64.5	65.5	14.8	17
Barrel radial services	13	44.2	48.4	4.55	17
Barrel/disk type 0 services	14	44.2	70	17	21.5
along frame	45	10	44.0	00 5	04.5
Outer frame connections	15	42	44.2	20.5	21.5
	16	70	107	17	21.5
l ype 1 services	1/	107	328	1/	21.5
PP1 zone 1	18.1	328	333.5	20.5	22.5
PP1 zone 2	18.2	328	333.5	11.5	20.5
PP1 zone 3	18.3	328	333.5	7.5	11.5
PP1 zone 4	18.4	333.5	334	7.5	22.5
PP1 zone 5	18.5	334	335.5	20.5	40
PP1 zone 6	18.6	334	335.5	11.5	20.5
PP1 zone 7	18.7	335.5	341.5	11.5	40
PP1 zone 8	18.8	341.5	344.3	11.5	40
PP1 zone 9	18.9	334	344.3	7.5	11.5
Central PST	19	0	80	22.7	22.8
Pixel to PST to SCT	20	75	80	22.8	28.5
	01	00	222 5	20.7	22.0
	21	80	333.5	22.1	22.ŏ
Type 2 services	22	342	344.3	40	280

Geometry description of the Pixel detector

						C	Composi	tion of	the Pixe	l detecto	or							
Element									MATE	ERIAL								
ID	Al	Cu	Ni	Со	Sn	Pb	Ag	Au	Fe	Cr	In	Ru	Pd	Mg	Mo	Ti	Mn	Zn
1	425.0	109.7	8.51	0.17	6.87	6.36	15.82	0.23	37.63	15.26	0.04	0.06	0.02	1.00	1.81	9.15		
2	587.4	187.4	10.51	0.21	11.87	10.98	27.32	0.40	39.08	15.91	0.07	0.10	0.04	1.74	1.88	15.80		
3	803.8	256.8	13.27	0.27	16.24	15.03	37.38	0.54	46.53	18.97	0.09	0.14	0.05	2.37	2.23	21.63		
4	107.6	17.3	0.41	0.01	1.15	1.07	2.65	0.04			0.01	0.01				1.54		
5	107.6	17.3	0.41	0.01	1.15	1.07	2.65	0.04			0.01	0.01				1.54		
6	107.6	17.3	0.41	0.01	1.15	1.07	2.65	0.04			0.01	0.01				1.54		
7	3.5	14.7	17.13	0.34	0.01				15.31	6.18	0.70				0.74			
8	6.0	25.3	29.69	0.59	0.02				27.09	10.93	1.22				1.31			
9	8.2	34.6	39.02	0.78	0.02				27.09	10.93	1.66				1.31			
10	12.4	1.6	1.60	0.03							0.13							
11	12.4	1.6	1.60	0.03							0.13							
12	12.4	1.6	1.60	0.03							0.13							
13	930.4	20.3	5.44	0.11						0.08				0.49				
14	4150.5	80.0	21.89	0.44						0.26	0.38			1.51		0.08	0.39	0.15
15	14.5	0.0	8.60	0.17					53.32	21.50					2.58			
16	619.5	631.8			31.83	16.66		0.02		0.85				4.12		1.07	5.28	2.03
17	11171.	380.3								6.60				31.96		8.27	40.94	15.74
18.1	28.9	51.6	8.60	0.17	11.62	6.92		0.02	53.32	21.72					2.58			
18.2	743.5	37.5								1.01				4.85		1.26	6.24	2.36
18.3	14.4	51.6			11.62	6.92		0.02		0.22								
18.4	729.1	63.3			2.49	1.48				1.08				4.85		1.26	6.24	2.36
18.5	0.0	189.1			41.81	23.27		0.12		0.79								
18.6	1458.2	74.9								2.01				9.69		2.52	1.24	4.78
18.7	2232.7	114.7								3.09				14.84		3.83	19.02	7.28
18.8	0.0	576.1			35.60	19.64		0.10		0.65								
18.9	0.0	140.3			11.62	6.47		0.02		0.14								
19	580.5	0.0																
20	7.3	0.0	4.30	0.09					26.66	10.75					1.29			
21	1103.0	0.0																
22	61256.	71111.	7864.5	157.29						4.99				30.99				

Geometry description of the SCT Barrel Detector

ELEMENT	Element	ELEMENT GEOMETRY (ring/disk)							
	ID	Z1[cm]	Z2[cm]	R1[cm]	R2[cm]				
Thermal shield 1	1	0	75.4	54.83	54.9				
Thermal shield 2	2	75.4	79	54	54.9				
Thermal shield 3	3	72.4	75.4	54	54.83				
Thermal shield 4	4	23.3	26.3	54	54.83				
Thermal shield 5	5	78.82	79	25	54				
Thermal shield 6	6	0	77	25	25.0175				
Barrel interlink	7	78.7	78.82	26	50				
SCT barrel 3 + Support cylinder	8	0	78.294	27.8	28.4				
Close out at the end of barrel	9	78.294	78.32	27.8	28.4				
End flange	10	78.32	78.7	25.8	28.4				
SCT barrel 4 +Support cylinder	11	0	78.294	34.9	35.5				
Close out at the end of barrel	12	78.294	78.32	34.9	35.5				
End flange	13	78.32	78.7	32.5	35.5				
SCT barrel 5 +Support cylinder	14	0	78.294	42.1	42.7				
Close out at the end of barrel	15	78.294	78.32	42.1	42.7				
End flange	16	78.32	78.7	39.5	42.7				
SCT barrel 6 +Support cylinder	17	0	78.294	49.201	49.801				
Close out at the end of barrel	18	78.294	78.32	49.2	49.8				
End flange	19	78.32	78.7	46.6	49.8				
SCT pipes	20	30.841	50	78	78.5				
Cables and cooling pipes from barrels to PPB1	21	78	79.84	50	114				
Cables and cooling pipes from PPB1 to PPB2	22	79.84	343	112.3	115				

Element								MATE	ERIAL							
ID	Н	Be	В	С	Ν	0	F	AI	Si	Ni	Со	Cu	Ag	Sn	Au	Pb
1	2.05			1448.15	5.75	16.47	336.76	1773.36								
2				538.16			172.63	169.99								
3	75.37			452.19												
4	75.37			452.19												
5				666.79				69.99								
6	4.47			118.86	12.54	35.90		245.15								
7	28.59			760.96	80.27	229.83										
8	18.05	114.625	52.99	2726.9	157.63	385.15	665.7	560.45	2259.84	7.68	0.155	493.825	19.2	11.71	2.11	18.625
9										7.39		17.25				
10	6.99			186.17	19.64	56.23										
11	22.56	143.28	66.24	3410.84	197.04	481.44	832.13	700.55	2824.8	9.6	0.19	617.28	24	14.64	2.64	23.28
12										9.26		21.60				
13	10.13			269.51	28.43	81.40										
14	27.07	171.935	79.49	4097.73	236.45	577.73	998.555	840.65	3389.76	11.52	0.23	740.735	28.8	17.57	3.17	27.935
15										11.15		26.02				
16	13.06			347.51	36.66	104.95										
17	31.585	200.59	92.735	4781.67	275.855	674.015	1164.98	980.75	3954.72	13.44	0.27	864.19	33.6	20.495	3.695	32.59
18										13.02		30.38				
19	15.31			407.54	42.99	123.09	509.39	2258.5		40.82		95.26				
20										25.7	0.51	59.9				
21								2800.0		600	12	1200				
22										10011.8	200.2	264856.				

					<u>,</u>
ELEMENT	Element	ELEMI	ENT GEOM	ETRY (ring	g/disk)
	UD		Z2[cm]	Rí[cm]	R2[cm]
I hermal_shield_1	1	81.10	81.20	25.10	61.00
Thermal_shield_2	2	82.00	82.02	50.00	59.00
Thermal_shield_3	3	82.05	84.00	58.20	59.90
Thermal_shield_4	4	82.00	82.50	59.90	61.00
Thermal_shield_5	5	82.50	273.30	59.90	61.00
Thermal_shield_6	6	82.50	273.30	61.00	61.09
Thermal_shield_7	7	274.90	274.92	25.80	57.20
Thermal_shield_8	8	274.92	275.72	25.80	57.20
Thermal_shield_9	9	278.60	278.70	25.80	61.50
Thermal_shield_10	10	275.80	278.50	25.80	29.15
Thermal_shield_11	11	81.30	278.70	25.55	25.80
Thermal_shield_12	12	81.30	81.85	25.80	30.50
SCT_disk_1	13	82.85	86.85	26.70	56.70
SCT disk 2	14	91.20	95.20	26.70	56.70
SCT disk 3	15	106.20	110.20	26.70	56.70
SCT disk 4	16	124.00	128.00	26.70	56.70
SCT disk 5	17	135.50	139.50	26.70	56.70
SCT disk 6	18	172.50	176.50	26.70	56.70
SCT disk 7	19	205.00	209.00	26.70	56.70
SCT disk 8	20	244 00	248.00	37 40	56 70
SCT disk 9	21	270.50	274 50	37 40	56 70
Cooling pipe 1	22	84.85	275.70	58.39	58.39
Cooling pipe 2	23	93 20	275 70	58.39	58 40
Cooling pipe 3	24	108 20	275 70	58 40	58 41
Cooling pipe 4	25	126.00	275.70	58.41	58.42
Cooling pipe 5	26	137 50	275 70	58 42	58 42
Cooling pipe 6	27	174 50	275 70	58 42	58 43
Cooling pipe 7	28	207.00	275.70	58.43	58.44
Cooling pipe 8	29	246.00	275 70	58 44	58 44
Cooling pipe 9	30	272 50	275 70	58 44	58 44
Power tape 1	31	84 85	275 70	59.85	59.85
Power tape 2	32	93.20	275.70	59.85	59.86
Power tape 3	33	108.20	275 70	59.86	59.87
Power tape 4	34	126.00	275.70	59.87	59.88
Power tape 5	35	137 50	275 70	59.88	59.88
Power tape 6	36	174 50	275 70	59.88	59.89
Power tape 7	37	207.00	275.70	59.89	59.89
Power tape 8	38	246.00	275.70	59.89	59.00
Power tape 9	30	272 50	275.70	59.00	59.00
Patch nanel 1	40	83.25	84.45	55 70	56 70
Patch_panel_2	-+0 //1	03.23	02.80	55 70	56 70
Patch_panel_2	42	106.60	107.80	55.70	56.70
Patch_panel_3	42	100.00	107.00	55.70	50.70
Patch papel 5	43	124.40	120.00	55.70	56.70
Patch paral 6	44	172.00	17/ 10	55.70	50.70
Patch_panel_7	40	205.00	174.10	55.70	50.7U
Patch_panel_?	40	200.80	200.00	55.70	50.70
Patch_panel_0	4/	244.0U	240.00	00.7U	56.70
	4ð	2/ 1.00	212.10		U1.0C
	49	2/3.00	350.00	114.00	115.00
Tipe II cables	50	272.50	273.00	55.90	114.00

Geometry description of the SCT Forward Detector

0.0TE 1D (• , •
SCI Forward Detector	composition
	composition

Element							Ν	IATERIAL	•						
ID	Н	Be	В	С	Ν	0	Al	Si	Ni	Co	Cu	Ag	Sn	Au	Pb
1							924.39								
2							166.76								
3				1232.45											
4				209.33											
5				79878.9											
6							1689.								
7							509.5								
8				6563.45											
9							2649.9								
10				2174.83											
11				11088.6											
12				636.82											
13	12.49	226.9	36.77	1448.49	61.80	87.17	77.00	583.23	4.90	0.10	294.10	20	9.60	2.16	14.30
14	17.76	401.3	65.04	1905.72	109.34	154.21	136.24	1031.88	8.67	0.17	520.33	35	16.99	3.81	25.31
15	17.76	401.3	65.04	1905.72	109.34	154.21	136.24	1031.88	8.67	0.17	520.33	35	16.99	3.81	25.31
16	17.76	401.3	65.04	1905.72	109.34	154.21	136.24	1031.88	8.67	0.17	520.33	35	16.99	3.81	25.31
17	17.76	401.3	65.04	1905.72	109.34	154.21	136.24	1031.88	8.67	0.17	520.33	35	16.99	3.81	25.31
18	17.76	401.3	65.04	1905.72	109.34	154.21	136.24	1031.88	8.67	0.17	520.33	35	16.99	3.81	25.31
19	12.49	226.9	36.77	1448.49	61.80	87.17	77.00	583.23	4.90	0.10	294.10	20	9.60	2.16	14.30
20	12.62	401.4	65.05	1593.24	109.34	154.22	136.24	1031.88	8.67	0.17	520.33	35	16.99	3.81	25.31
21	7.14	226.9	36.77	1135.98	61.80	87.17	77.00	583.23	4.90	0.10	294.10	20	9.60	2.16	14.30
22							285.90								
23							410.07								
24							376.42								
25							336.46								

Table 12 (continuation)

Element							MATERIA	L BRE	KDOWN						
ID	Н	Be	В	С	Ν	0	Al	Si	Ni	Со	Cu	Ag	Sn	Au	Pb
26							310.65								
27							227.51								
28							102.99								
29							44.53								
30							2.40								
31							959.25								
32							1299.91								
33							1193.21								
34							1066.54								
35							984.72								
36							721.17								
37							345.53								
38							149.39								
39							9.09								
40							1146.43								
41							764.28								
42							1146.43								
43							1146.43								
44							1146.43								
45							1146.43								
46							764.28								
47							764.28		2787.2	55.7	73240.				
48							477.68		2103.1	42.1	55263.				

ELEMENT	Element	ELEM	ENT GEON	IETRY (ring	g/disk)
	ID	Z1[cm]	Z2[cm]	R1[cm]	R2[cm]
Barrel TRT	1	0	71.2	55.8	107.3
TRT A	2	82.6	170.7	62	107.6
TRT B	3	172	271.6	62	107.6
TRT C	4	281.6	340.6	46	103.4
Barrel Module 1 services	5	77.2	78.5	60	115
Barrel Module 2 services	6	78.5	80	75	115
Barrel Module 3 services	7	80	81	90	115
Wheels A services	8	124	340	113	114
Wheels B services	9	225	340	112	113
Wheels C services	10	338	340	105	112
Barrel electronics	11	71.2	77.2	56	107
EC electronics	12	82.6	338	107.6	108.6
Squirrel cage	13	82.6	338	108.6	109.2
Module 1,2,3 services	14	81	340	114	115
TRT services	15	340	345	109.2	317

Geometry description of the TRT detector

							TRT	compos	sition							
Element							MAT	ERIAL E	BREAKDO	OWN					-	
ID	Cu	Al	Si	Fe	Mn	Cr	Ni	Со	Zn	Sn	Pb	Au	Ag	Ва	Ti	W
1												23.75				339.32
2												27.06				386.58
3												30.59				437.04
4												20.09				287.07
5	1532.23	325.90		1442.70	41.22	370.98	206.10	4.1								
6	2188.65	327.43		1422.99	40.66	365.91	203.28	4.0								
7	1765.40	241.74		1186.39	33.90	305.07	169.48	3.38								
8	41784.8	6381.80		5432.90	155.23	1397.03	776.13	15.5								
9	15720.1	2559.69		3599.70	102.85	925.64	514.24	10.2								
10	2108.27	487.11		585.99	16.74	150.68	83.71	1.6								
11	5497.73	6686.5	1458.10	1285.48	36.73	330.55	183.64	3.7	938.95	13.05	13.05	10.92	262.72	270.07	94.31	
12	15000.					77.50		0	35.00	2215.0	1476.5	12.50				
13	270.00	268000.		1075.00		670.0		0	670.00							
14	36037.0	5213.91		11746.1	335.60	3020.41	1678.01	33.6								
15	113634.	19902.8		24893.3	711.24	6401.15	3556.19	71.								

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					Ga	mma-equiv	alents in Tl	RT volume	by material						
					T=100 d							T=10 y			
	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
	Al	50.4	31.2	29.2	31.2	39.0	48.3	66.5	63.3	59.9	62.1	64.6	71.0	77.0	85.8
	Si	0.2	0.2	0.2	0.2	0.3	0.3	0.5	0.3	0.4	0.4	0.5	0.5	0.5	0.6
s	Ti	0.1	0.2	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0
ron	Mn	1.1	1.9	2.0	2.0	1.8	1.5	1.2	0.9	1.2	1.3	1.2	1.0	0.9	0.7
lad	Fe	5.0	8.0	8.3	7.7	5.6	3.7	2.2	3.7	4.5	4.2	3.8	2.6	1.7	1.0
<u>т</u>	Ni	0.9	1.5	1.7	1.7	1.8	1.9	1.5	0.7	0.9	0.9	0.9	0.8	0.8	0.5
	Cu	14.3	23.9	27.0	27.9	29.0	28.6	20.8	11.4	14.9	15.3	15.2	14.2	12.7	8.4
	W	27.9	33.0	31.4	28.9	22.4	15.4	7.2	19.6	18.1	15.7	13.8	9.7	6.3	2.9
	Subtotal	8.95E-10	4.51E-10	3.65E-10	3.29E-10	2.60E-10	2.07E-10	1.42E-10	1.31E-09	8.66E-10	7.79E-10	7.43E-10	6.70E-10	6.11E-10	5.20E-10
	Al	5.0	1.5	0.3	0.0	0.0	0.0	0.0	4.7	1.3	0.2	0.0	0.0	0.0	0.0
	Cr	0.2	0.5	0.9	1.2	1.8	1.5	0.3	0.2	0.5	0.7	0.9	1.0	0.8	0.2
	Fe	0.1	0.3	0.5	0.7	1.2	1.2	0.6	0.1	0.3	0.5	0.6	0.8	0.8	0.5
	Со	0.2	0.5	0.8	1.2	2.2	2.6	3.1	1.1	2.8	4.4	5.7	8.4	9.3	11.0
S	Ni	0.1	0.2	0.3	0.5	0.8	0.8	0.5	0.1	0.2	0.3	0.4	0.5	0.5	0.3
Lo Lo	Cu	27.6	5.6	0.7	0.1	0.0	0.0	0.0	25.9	4.7	0.5	0.1	0.0	0.0	0.0
eut	Zn	1.0	2.6	4.5	6.4	11.6	13.2	13.5	1.7	4.0	6.2	8.0	11.5	12.3	12.3
z	Ag	5.6	15.5	26.7	37.8	68.6	78.4	80.4	9.7	24.0	37.2	47.9	69.4	74.3	74.2
	Sn	0.3	0.8	1.3	1.7	2.4	2.0	1.4	0.4	0.9	1.3	1.6	2.0	1.8	1.5
	W	27.3	18.8	8.1	2.9	0.0	0.0	0.0	25.6	15.9	6.2	2.0	0.0	0.0	0.0
	Au	32.5	53.8	55.8	47.6	11.3	0.3	0.0	30.5	45.4	42.4	32.8	6.2	0.1	0.0
	Subtotal	1.93E-09	7.00E-10	4.03E-10	2.83E-10	1.53E-10	1.28E-10	1.03E-10	2.06E-09	8.28E-10	5.31E-10	4.11E-10	2.77E-10	2.48E-10	2.05E-10
Tota	I, Sv.m².s⁻¹	2.83E-09	1.15E-09	7.69E-10	6.13E-10	4.13E-10	3.36E-10	2.45E-10	3.37E-09	1.69E-09	1.31E-09	1.15E-09	9.47E-10	8.59E-10	7.25E-10

-		0			· ·					,					
					T=100 d							T=10 y			
	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
	Al	2.6	1.0	0.9	0.9	1.3	1.7	3.1	4.2	3.2	3.3	3.6	4.5	5.7	9.2
SU	Mn	5.5	5.8	5.8	5.7	5.4	5.0	5.9	6.0	6.4	6.5	6.5	6.4	6.4	7.7
dro	Fe	35.9	35.5	33.5	31.4	24.4	18.3	15.9	33.3	32.4	30.5	28.5	22.5	17.6	15.8
На	Ni	10.4	10.7	10.9	11.3	12.7	14.3	15.1	10.1	10.3	10.4	10.6	11.6	12.4	11.5
	Cu	45.6	47.0	48.9	50.7	56.2	60.8	60.1	46.4	47.7	49.3	50.8	55.0	57.9	55.8
	Subtotal	1.37E-09	1.11E-09	9.78E-10	8.83E-10	6.60E-10	4.86E-10	2.47E-10	1.57E-09	1.31E-09	1.18E-09	1.08E-09	8.54E-10	6.69E-10	3.93E-10
	Al	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0
	Cr	0.8	7.0	15.5	16.6	14.7	11.3	2.9	0.8	3.7	4.9	4.9	4.1	2.9	0.6
s	Mn	0.2	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1
ror	Fe	0.8	6.7	15.1	16.6	16.2	15.1	10.1	0.9	4.3	5.9	6.0	5.6	4.9	2.9
eut	Со	1.8	15.3	35.5	39.9	43.0	48.2	68.3	11.2	55.2	77.6	80.4	82.2	84.9	92.3
Z	Ni	1.2	10.4	23.6	26.0	26.0	25.3	18.6	1.3	6.0	8.3	8.5	8.0	7.2	4.1
	Cu	95.0	60.3	10.2	0.8	0.0	0.0	0.0	85.4	30.6	3.1	0.2	0.0	0.0	0.0
	Subtotal	3.35E-09	3.85E-10	1.66E-10	1.48E-10	1.37E-10	1.21E-10	8.33E-11	3.72E-09	7.57E-10	5.38E-10	5.19E-10	5.06E-10	4.88E-10	4.37E-10
Tota	al, Sv.m ² .s ⁻¹	4.72E-09	1.49E-09	1.14E-09	1.03E-09	7.96E-10	6.07E-10	3.30E-10	5.29E-09	2.07E-09	1.72E-09	1.60E-09	1.36E-09	1.16E-09	8.30E-10

Gamma-equivalents in TRT services by material (Type 1, 2, and 3)

					0	annna oqui									
					T=100 d							T=10 y			
	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
	Be	0.1	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0
	С	2.7	4.5	5.1	5.4	5.8	5.8	3.6	2.0	2.6	2.8	2.8	2.8	2.5	1.2
suc	Al	22.6	10.9	9.2	9.5	11.2	13.4	19.6	25.7	20.7	20.6	21.2	23.0	24.8	28.9
dro	Si	20.8	15.7	15.8	16.8	19.8	23.6	34.4	32.7	34.4	36.1	37.3	40.4	43.7	50.8
На	Ni	4.2	6.2	6.6	6.7	6.8	6.8	5.6	3.1	3.8	3.8	3.7	3.5	3.2	2.1
	Cu	29.1	42.2	44.9	45.1	43.8	41.4	31.7	22.4	26.9	27.0	26.4	24.1	21.5	14.7
	Pb	20.3	20.0	17.7	15.8	11.9	8.4	4.7	13.9	11.3	9.5	8.3	5.9	4.0	2.1
	Subtotal	2.96E-10	1.74E-10	1.49E-10	1.38E-10	1.16E-10	9.56E-11	6.16E-11	4.47E-10	3.25E-10	3.00E-10	2.88E-10	2.64E-10	2.42E-10	1.97E-10
	Al	2.1	0.6	0.1	0.0	0.0	0.0	0.0	1.8	0.4	0.1	0.0	0.0	0.0	0.0
	Со	0.4	1.0	1.3	1.5	1.9	2.0	2.4	2.3	4.7	5.6	6.1	7.0	7.4	8.6
s	Ni	0.4	1.0	1.3	1.5	1.7	1.6	1.0	0.4	0.8	0.9	1.0	1.0	0.9	0.6
ror	Cu	51.8	9.5	0.9	0.1	0.0	0.0	0.0	43.5	6.4	0.6	0.0	0.0	0.0	0.0
eut	Ag	19.9	49.7	65.8	75.7	92.9	96.2	96.5	30.7	61.8	74.1	80.5	90.0	91.5	90.7
Z	Sn	0.1	0.2	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.2	0.2	0.2	0.1	0.1
	Au	25.4	38.1	30.4	21.0	3.4	0.1	0.0	21.3	25.8	18.6	12.2	1.8	0.0	0.0
	Subtotal	2.37E-10	9.42E-11	7.07E-11	6.12E-11	4.88E-11	4.52E-11	3.71E-11	2.82E-10	1.39E-10	1.15E-10	1.06E-10	9.24E-11	8.72E-11	7.25E-11
Tota	l, Sv.m ² .s ⁻¹	5.33E-10	2.68E-10	2.20E-10	1.99E-10	1.64E-10	1.41E-10	9.86E-11	7.29E-10	4.64E-10	4.15E-10	3.94E-10	3.57E-10	3.29E-10	2.69E-10

Gamma-equivalents in SCT Barrel by material

					T=100 d							T=10 y			
	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
	Be	0.1	0.2	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0
	С	6.4	12.7	14.8	15.5	16.1	15.7	9.4	4.7	6.9	7.3	7.3	7.1	6.2	3.0
suc	Al	54.1	30.9	26.6	27.2	31.1	36.0	50.7	61.1	53.2	53.2	54.3	57.6	61.2	69.4
drc	Si	6.6	5.7	5.8	6.0	6.9	8.0	11.2	10.0	11.2	11.7	12.0	12.8	13.5	15.3
На	Ni	1.8	3.2	3.5	3.6	3.6	3.5	2.8	1.3	1.8	1.8	1.8	1.7	1.5	1.0
	Cu	20.4	35.0	37.9	37.5	34.7	31.4	22.7	15.6	20.4	20.4	19.7	17.4	15.0	9.9
	Pb	10.4	12.3	11.1	9.9	7.2	5.1	2.9	7.2	6.5	5.4	4.7	3.3	2.3	1.3
	Subtotal	5.67E-10	2.79E-10	2.34E-10	2.18E-10	1.88E-10	1.60E-10	1.06E-10	8.55E-10	5.67E-10	5.20E-10	5.04E-10	4.72E-10	4.38E-10	3.66E-10
	Со	0.3	0.6	0.7	0.8	1.0	1.1	1.3	1.6	2.7	3.2	3.5	4.0	4.2	4.9
	Ni	0.2	0.3	0.4	0.4	0.5	0.5	0.3	0.1	0.2	0.3	0.3	0.3	0.3	0.2
s	Cu	33.5	4.9	0.5	0.0	0.0	0.0	0.0	27.0	3.3	0.3	0.0	0.0	0.0	0.0
ror	Ag	26.4	52.5	67.1	77.1	94.8	98.2	98.3	39.1	65.4	76.7	83.4	93.7	95.4	94.8
eut	Sn	0.1	0.1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.2	0.1	0.1	0.1
Z	Au	33.7	40.3	31.0	21.4	3.5	0.1	0.0	27.2	27.3	19.3	12.6	1.9	0.0	0.0
	Al	5.9	1.3	0.2	0.0	0.0	0.0	0.0	4.8	0.9	0.1	0.0	0.0	0.0	0.0
	Subtotal	4.85E-10	2.42E-10	1.89E-10	1.63E-10	1.30E-10	1.20E-10	9.90E-11	6.01E-10	3.57E-10	3.03E-10	2.77E-10	2.41E-10	2.27E-10	1.88E-10
Tota	l, Sv.m ² .s ⁻¹	1.05E-09	5.22E-10	4.22E-10	3.81E-10	3.18E-10	2.80E-10	2.05E-10	1.46E-09	9.24E-10	8.23E-10	7.81E-10	7.13E-10	6.66E-10	5.55E-10

Gamma-equivalents in SCT Forward by material

-										/ 1	/				
					T=100 d							T=10 y			
s	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
Lon	Al	0.9	0.3	0.3	0.3	0.3	0.4	0.7	1.4	1.0	1.0	1.0	1.2	1.4	2.3
ladi	Ni	20.5	20.7	20.4	20.4	20.9	21.6	22.6	19.7	19.7	19.4	19.4	19.5	19.8	19.0
1	Cu	78.6	79.0	79.3	79.3	78.8	78.0	76.6	78.9	79.3	79.6	79.6	79.3	78.8	78.6
	Subtotal	1.54E-09	1.28E-09	1.17E-09	1.10E-09	9.09E-10	7.27E-10	3.70E-10	1.79E-09	1.53E-09	1.42E-09	1.34E-09	1.14E-09	9.44E-10	5.34E-10
suc	Со	2.1	19.8	52.3	59.8	62.2	65.5	78.5	12.0	61.5	87.8	90.8	91.6	92.7	96.0
utro	Ni	1.4	13.5	34.9	39.1	37.8	34.5	21.5	1.3	6.3	8.8	8.9	8.4	7.3	4.0
Ne	Cu	96.5	66.7	12.8	1.1	0.0	0.0	0.0	86.7	32.2	3.4	0.3	0.0	0.0	0.0
	Subtotal	5.84E-09	6.16E-10	2.33E-10	2.04E-10	1.95E-10	1.84E-10	1.50E-10	6.60E-09	1.37E-09	9.86E-10	9.56E-10	9.45E-10	9.29E-10	8.71E-10
Tota	al, Sv.m ² .s ⁻¹	7.38E-09	1.90E-09	1.41E-09	1.30E-09	1.10E-09	9.11E-10	5.19E-10	8.39E-09	2.90E-09	2.40E-09	2.29E-09	2.09E-09	1.87E-09	1.40E-09

Gamma-equivalents in SCT Barrel services by material (Type 1 and 2)

Table 20

Gamma-equivalents in SCT Forward services by material (Type 1 and 2)

					T=100 d			T=10 y							
Hadrons	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
	Ni	18.5	18.7	18.7	18.8	19.5	20.4	21.7	17.9	18.0	17.9	18.0	18.4	18.8	18.4
	Cu	81.5	81.3	81.3	81.2	80.5	79.6	78.3	82.1	82.0	82.1	82.0	81.6	81.2	81.6
	Subtotal	1.20E-09	1.01E-09	9.17E-10	8.54E-10	7.02E-10	5.56E-10	2.79E-10	1.38E-09	1.19E-09	1.10E-09	1.03E-09	8.74E-10	7.16E-10	3.99E-10
Neutrons	Со	1.9	18.5	50.7	58.6	61.0	64.3	77.7	13.1	63.1	87.5	90.2	91.0	92.1	95.7
	Ni	1.4	13.2	35.6	40.3	39.0	35.7	22.3	1.5	6.9	9.5	9.6	9.0	7.9	4.3
	Cu	96.7	68.3	13.7	1.1	0.0	0.0	0.0	85.4	30.0	3.0	0.2	0.0	0.0	0.0
	Subtotal	3.45E-09	3.56E-10	1.29E-10	1.12E-10	1.07E-10	1.01E-10	8.16E-11	3.85E-09	7.62E-10	5.36E-10	5.18E-10	5.11E-10	5.02E-10	4.70E-10
Tota	al, Sv.m ² .s ⁻¹	4.64E-09	1.36E-09	1.05E-09	9.67E-10	8.09E-10	6.57E-10	3.60E-10	5.24E-09	1.95E-09	1.63E-09	1.55E-09	1.39E-09	1.22E-09	8.69E-10

Gamma-equivalents in PIXEL and Ty	vpe 1 services by material
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		T=100 d								T=10 y							
drons	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d		
	AI	48.5	24.7	21.0	21.9	26.7	32.8	49.0	58.3	49.3	50.1	52.0	57.7	63.6	75.5		
	Ti	0.6	0.9	0.9	0.8	0.8	0.8	0.7	0.5	0.6	0.5	0.5	0.4	0.4	0.3		
	Mn	1.7	2.6	2.8	2.8	2.4	1.9	1.4	1.4	1.9	1.9	1.8	1.6	1.3	1.0		
	Fe	6.6	9.9	9.9	9.2	6.7	4.4	2.6	5.1	6.3	5.9	5.3	3.7	2.4	1.4		
На	Ni	9.3	15.4	17.2	17.9	19.1	19.8	16.8	7.7	10.4	10.8	10.8	10.6	9.9	6.7		
	Cu	22.4	34.8	37.6	37.8	36.7	34.3	25.7	18.7	24.1	24.4	23.8	21.7	19.1	13.0		
	Pb	10.9	11.7	10.6	9.6	7.6	6.1	4.0	8.3	7.5	6.4	5.7	4.3	3.3	2.1		
	Subtotal	2.19E-09	1.17E-09	9.72E-10	8.87E-10	7.16E-10	5.72E-10	3.56E-10	3.01E-09	1.99E-09	1.79E-09	1.70E-09	1.52E-09	1.36E-09	1.08E-09		
	Cr	0.4	1.6	2.1	2.2	1.9	1.4	0.3	0.4	0.9	1.0	1.0	0.8	0.6	0.1		
	Mn	0.5	0.1	0.2	0.2	0.2	0.2	0.2	0.5	0.2	0.2	0.2	0.2	0.2	0.2		
	Fe	0.2	0.9	1.2	1.3	1.3	1.1	0.7	0.3	0.7	0.8	0.8	0.7	0.7	0.5		
	Со	1.8	7.3	10.1	10.8	11.5	12.2	14.9	10.5	27.8	32.6	33.6	34.8	36.0	41.0		
s	Ni	1.8	7.3	9.9	10.3	10.3	9.5	6.0	1.7	4.5	5.2	5.3	5.1	4.6	2.7		
LO L	Cu	65.5	19.5	2.0	0.2	0.0	0.0	0.0	54.1	10.5	0.9	0.1	0.0	0.0	0.0		
ent	Zn	0.3	1.2	1.7	1.8	1.8	1.9	1.9	0.5	1.2	1.4	1.4	1.4	1.4	1.4		
z	Ag	11.4	46.4	63.7	67.4	70.9	72.5	75.0	17.3	45.8	53.5	54.8	55.7	55.7	53.5		
	Sn	0.3	1.3	1.6	1.6	1.3	1.0	0.7	0.4	0.9	1.0	1.0	0.9	0.7	0.6		
	Au	3.1	7.5	6.2	4.0	0.5	0.0	0.0	2.5	4.0	2.8	1.8	0.2	0.0	0.0		
	AI	14.3	6.4	1.0	0.1	0.0	0.0	0.0	11.8	3.4	0.4	0.0	0.0	0.0	0.0		
	Subtotal	1.89E-10	4.62E-11	3.35E-11	3.15E-11	2.93E-11	2.75E-11	2.19E-11	2.29E-10	8.61E-11	7.33E-11	7.11E-11	6.84E-11	6.57E-11	5.63E-11		
Tota	l, Sv.m ² .s⁻¹	2.38E-09	1.22E-09	1.01E-09	9.18E-10	7.45E-10	6.00E-10	3.78E-10	3.24E-09	2.07E-09	1.86E-09	1.77E-09	1.59E-09	1.42E-09	1.14E-09		

		T=100 d								T=10 y							
Hadrons	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d		
	Al	22.4	9.5	8.0	8.2	9.6	11.5	19.3	31.3	24.6	24.8	25.7	28.8	32.6	45.2		
	Ni	31.1	36.4	36.8	36.7	36.8	37.0	35.1	26.9	29.4	29.1	28.7	27.7	26.6	21.2		
	Cu	46.4	54.0	55.2	55.1	53.6	51.5	45.6	41.9	46.0	46.1	45.6	43.5	40.9	33.7		
	Subtotal	9.08E-10	6.52E-10	5.83E-10	5.46E-10	4.61E-10	3.78E-10	2.13E-10	1.18E-09	9.18E-10	8.48E-10	8.09E-10	7.18E-10	6.27E-10	4.29E-10		
Neutrons	Al	2.1	1.4	0.3	0.0	0.0	0.0	0.0	1.6	0.5	0.1	0.0	0.0	0.0	0.0		
	Со	5.1	32.7	54.5	57.8	59.9	63.2	76.8	27.6	76.6	88.3	89.4	90.2	91.4	95.3		
	Ni	3.9	24.6	40.2	41.8	40.1	36.8	23.2	3.4	9.3	10.5	10.5	9.8	8.6	4.7		
	Cu	88.9	41.3	5.0	0.4	0.0	0.0	0.0	67.4	13.6	1.1	0.1	0.0	0.0	0.0		
	Subtotal	1.37E-09	2.16E-10	1.29E-10	1.22E-10	1.17E-10	1.10E-10	8.85E-11	1.81E-09	6.52E-10	5.66E-10	5.58E-10	5.51E-10	5.41E-10	5.06E-10		
Tota	al, Sv.m ² .s ⁻¹	2.28E-09	8.68E-10	7.13E-10	6.68E-10	5.78E-10	4.89E-10	3.01E-10	2.99E-09	1.57E-09	1.41E-09	1.37E-09	1.27E-09	1.17E-09	9.35E-10		

Gamma-equivalents in PIXEL Services by material (Type 2 only)
	Ganina-equivalents in D bean-pipe by material														
					T=100 d							T=10 y			
	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
	Be	21.6	46.5	53.6	54.5	53.9	50.9	32.2	15.8	24.2	25.5	25.4	23.9	21.0	10.3
s	Al	73.2	44.0	36.6	36.4	39.3	44.1	64.3	80.2	70.5	69.4	69.9	72.5	76.3	87.8
Lon	Ti	0.3	0.6	0.5	0.5	0.4	0.4	0.3	0.2	0.3	0.3	0.2	0.2	0.2	0.1
ad	Mn	2.4	4.5	4.7	4.4	3.4	2.5	1.8	1.9	2.6	2.6	2.4	1.9	1.5	1.1
Т	Fe	1.7	3.1	3.0	2.7	1.7	1.1	0.6	1.2	1.6	1.4	1.3	0.8	0.5	0.3
	Cu	0.8	1.4	1.5	1.5	1.2	1.1	0.8	0.6	0.8	0.8	0.7	0.6	0.5	0.4
	Subtotal	2.06E-10	9.31E-11	7.87E-11	7.54E-11	6.87E-11	5.99E-11	3.81E-11	3.09E-10	1.96E-10	1.81E-10	1.77E-10	1.70E-10	1.59E-10	1.31E-10
	Al	84.1	75.8	38.4	7.0	0.0	0.0	0.0	83.1	68.8	26.1	3.9	0.0	0.0	0.0
	Ti	0.2	1.0	3.9	5.6	5.3	4.9	3.5	0.2	1.1	3.0	3.6	3.3	3.0	2.1
S	Cr	0.1	1.0	4.5	7.2	6.7	4.9	1.1	0.1	0.9	3.1	4.1	3.7	2.7	0.6
ron	Mn	1.7	5.7	26.6	44.6	49.8	51.5	56.0	2.4	11.0	38.2	52.7	56.1	57.1	60.2
eut	Fe	0.1	1.2	5.4	9.0	9.8	9.6	9.1	0.3	1.9	6.7	9.2	9.6	9.5	9.3
Ž	Zn	0.4	3.3	15.3	25.6	28.4	29.1	30.3	0.8	5.4	18.8	25.8	27.4	27.6	27.9
	Mg	12.9	11.6	5.9	1.1	0.0	0.0	0.0	12.7	10.6	4.0	0.6	0.0	0.0	0.0
	Subtotal	4.31E-12	5.20E-13	1.12E-13	6.64E-14	5.83E-14	5.46E-14	4.30E-14	4.36E-12	5.73E-13	1.65E-13	1.19E-13	1.10E-13	1.04E-13	8.46E-14
Tota	I, Sv.m ² .s ⁻¹	2.10E-10	9.36E-11	7.88E-11	7.54E-11	6.88E-11	6.00E-11	3.81E-11	3.13E-10	1.96E-10	1.81E-10	1.77E-10	1.70E-10	1.59E-10	1.31E-10

Gamma-equivalents in ID beam-pipe by material

	Gamma-equivalents in LAr beam-pipe by material														
					T=100 d				T=10 y						
	Material	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d	t= 1 d	t= 3 d	t= 5 d	t= 7 d	t= 15 d	t= 30 d	t= 100 d
SUG	Mn	9.2	9.5	9.8	10.0	10.6	10.5	11.3	10.2	10.7	11.1	11.5	12.6	13.4	16.1
adro	Fe	67.3	65.8	63.9	61.8	53.8	44.5	37.4	65.5	63.9	61.9	59.9	52.6	45.1	41.4
Нa	Ni	23.4	24.6	26.3	28.1	35.5	44.9	51.1	24.1	25.3	26.8	28.4	34.6	41.2	41.9
	Subtotal	9.37E-08	7.65E-08	6.57E-08	5.76E-08	3.87E-08	2.51E-08	1.16E-08	1.02E-07	8.50E-08	7.41E-08	6.59E-08	4.66E-08	3.25E-08	1.72E-08
	Cr	1.2	1.2	1.2	1.1	1.0	0.8	0.2	0.9	0.9	0.8	0.8	0.7	0.5	0.1
	Mn	0.8	0.5	0.5	0.5	0.5	0.6	0.9	0.9	0.7	0.7	0.7	0.7	0.8	1.0
suc	Fe	9.0	9.1	9.2	9.4	9.8	10.6	15.5	12.5	12.6	12.8	12.9	13.4	14.2	18.1
utro	Co	3.9	4.0	4.1	4.1	4.4	5.0	8.3	17.6	17.9	18.2	18.5	19.5	21.5	31.8
Nei	Ni	83.4	84.0	84.1	84.1	83.9	82.9	75.1	67.0	67.0	66.8	66.6	65.4	62.8	48.9
	Мо	1.6	1.2	1.0	0.8	0.4	0.2	0.0	1.1	0.9	0.7	0.5	0.3	0.1	0.0
	Subtotal	2.43E-09	2.37E-09	2.32E-09	2.28E-09	2.11E-09	1.84E-09	1.03E-09	3.48E-09	3.41E-09	3.36E-09	3.31E-09	3.11E-09	2.80E-09	1.84E-09
Tot	al, Sv.m ² .s ⁻¹	9.61E-08	7.89E-08	6.80E-08	5.99E-08	4.08E-08	2.69E-08	1.00E+02	1.06E-07	8.84E-08	7.74E-08	6.92E-08	4.97E-08	3.53E-08	1.91E-08

Туре	Element	Cooling time, t									
		1 d	3 d	5 d	7 d	15 d	30 d	100 d			
	ID beam pipe	7.17	2.57	2.00	1.89	1.73	1.56	1.21			
	LAr beam pipe	247	205	176	155	104	66.9	30.3			
	Pixel type 2 services	9.31	6.58	5.87	5.48	4.61	3.78	2.13			
	Pixel	145	63.5	51.3	47.4	40.3	34.0	24.1			
	SCT barrel	0.20	0.12	0.10	0.09	0.08	0.06	0.04			
Hadron	SCT forward	1.18	0.56	0.47	0.44	0.38	0.33	0.22			
activation	SCT barrel services	2.58	2.16	1.97	1.84	1.53	1.22	0.62			
	SCT forward services	4.03	3.39	3.09	2.88	2.36	1.86	0.93			
	TRT	1.57	0.77	0.61	0.55	0.43	0.34	0.24			
	TRT services	2.46	2.00	1.76	1.60	1.20	0.89	0.45			
	LAr Barrel	14.8	9.50	7.40	6.20	3.70	2.10	1.80			
	LAr EndCap	27.0	15.8	13.0	11.3	7.90	5.20	2.40			
	ID beam pipe	0.16	0.02	0.00	0.00	0.00	0.00	0.00			
	LAr beam pipe	6.39	6.14	5.99	5.87	5.44	4.78	2.87			
	Pixel type 2 services	8.98	1.44	0.87	0.82	0.79	0.74	0.58			
	Pixel	13.4	1.48	0.45	0.34	0.27	0.24	0.17			
	SCT barrel	0.16	0.06	0.05	0.04	0.03	0.03	0.02			
Neutron	SCT forward	0.88	0.44	0.34	0.30	0.24	0.22	0.18			
activation	SCT barrel services	9.48	0.99	0.37	0.32	0.31	0.29	0.24			
	SCT forward services	10.9	1.12	0.41	0.35	0.34	0.32	0.26			
	TRT	3.60	1.30	0.68	0.42	0.14	0.10	0.08			
	TRT services	5.80	0.65	0.28	0.24	0.23	0.20	0.14			
	LAr Barrel	17.0	1.00	0.70	0.67	0.61	0.51	0.40			
	LAr EndCap	2.50	0.90	0.60	0.45	0.42	0.40	0.38			
Total, µSv/h		541.5	327.5	274.3	244.5	177.0	126.1	69.8			

Dose rate at R= 175 mm, Z= 3340 mm for exposure time T=100 days and different cooling time

Dose rate at R= 175 mm, Z= 3340 mm	n for exposure time T=1	10 years and different cooling time
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Туре	Element	Cooling time, t								
		1 d	3 d	5 d	7 d	15 d	30 d	100 d		
	ID beam pipe	11.40	6.64	6.05	5.94	5.82	5.58	5.02		
	LAr beam pipe	270.00	227.00	198.00	177.00	126.00	87.30	45.70		
	Pixel type 2 services	12.10	9.38	8.66	8.26	7.34	6.41	4.43		
	Pixel	216.00	135.00	123.00	119.00	111.00	104.00	89.30		
	SCT barrel	0.30	0.22	0.20	0.19	0.18	0.16	0.13		
Hadron activation	SCT forward	1.80	1.18	1.08	1.05	0.99	0.93	0.78		
	SCT barrel services	3.00	2.57	2.38	2.24	1.92	1.58	0.89		
	SCT forward services	4.65	4.01	3.70	3.48	2.93	2.40	1.33		
	TRT	2.31	1.50	1.35	1.28	1.16	1.06	0.91		
	TRT services	2.84	2.37	2.14	1.96	1.55	1.22	0.72		
	LAr Barrel	18.70	14.60	11.80	10.00	6.40	5.90	5.50		
	LAr EndCap	32.00	21.40	18.00	15.90	11.80	9.00	6.70		
	ID beam pipe	0.16	0.02	0.01	0.00	0.00	0.00	0.00		
	LAr beam pipe	12.80	12.50	12.40	12.20	11.70	11.00	8.62		
	Pixel type 2 services	11.80	4.21	3.64	3.59	3.55	3.47	3.23		
	Pixel	13.70	1.82	0.79	0.67	0.60	0.56	0.46		
	SCT barrel	0.19	0.09	0.08	0.07	0.06	0.06	0.05		
Neutron	SCT forward	1.09	0.65	0.55	0.50	0.44	0.41	0.34		
activation	SCT barrel services	10.70	2.16	1.54	1.49	1.47	1.44	1.35		
	SCT forward services	12.20	2.40	1.69	1.63	1.61	1.58	1.48		
	TRT	3.69	1.40	0.77	0.51	0.23	0.19	0.15		
	TRT services	6.40	1.26	0.88	0.84	0.82	0.79	0.71		
	LAr Barrel	19.00	2.40	2.20	2.16	2.07	1.95	1.80		
	LAr EndCap	4.40	3.50	2.50	2.40	2.30	2.20	2.20		
Total, µSv/h		671.2	458.3	403.4	372.4	301.9	249.2	181.8		

Flammer 4	
Dose rate at R= 400 mm, Z=	3443 mm for exposure time T=100 days and different cooling time

Туре	Element	Cooling time, t								
		1 d	3 d	5 d	7 d	15 d	30 d	100 d		
	ID beam pipe	3.26	1.12	0.86	0.81	0.74	0.67	0.55		
	LAr beam pipe	214	177	153	134	90	58	26		
	Pixel type 2 services	30.40	21.40	19.00	17.80	14.90	12.20	6.86		
	Pixel	16.90	9.17	7.69	7.06	5.75	4.61	2.84		
	SCT barrel	0.19	0.11	0.09	0.09	0.07	0.06	0.04		
Hadron activation	SCT forward	0.96	0.46	0.38	0.36	0.31	0.27	0.18		
	SCT barrel services	2.53	2.11	1.93	1.80	1.50	1.20	0.61		
	SCT forward services	3.71	3.12	2.84	2.64	2.17	1.71	0.86		
	TRT	1.55	0.75	0.60	0.54	0.42	0.34	0.23		
	TRT services	2.48	2.01	1.78	1.61	1.21	0.89	0.46		
	LAr Barrel	14.80	9.40	7.40	6.20	3.70	2.10	1.80		
	LAr EndCap	23.00	13.40	11.00	9.60	6.70	4.70	2.20		
	ID beam pipe	0.08	0.01	0.00	0.00	0.00	0.00	0.00		
	LAr beam pipe	5.64	5.43	5.30	5.19	4.81	4.23	2.52		
	Pixel type 2 services	24.20	3.95	2.43	2.30	2.20	2.05	1.59		
	Pixel	3.64	0.39	0.12	0.09	0.06	0.05	0.03		
	SCT barrel	0.15	0.06	0.04	0.04	0.03	0.03	0.02		
Neutron	SCT forward	0.73	0.37	0.28	0.25	0.20	0.18	0.15		
activation	SCT barrel services	9.23	0.97	0.36	0.31	0.30	0.28	0.23		
	SCT forward services	10.30	1.06	0.38	0.33	0.32	0.30	0.24		
	TRT	3.56	1.30	0.67	0.41	0.13	0.09	0.07		
	TRT services	5.84	0.66	0.28	0.25	0.23	0.20	0.14		
	LAr Barrel	17.00	1.00	0.70	0.67	0.61	0.51	0.40		
	LAr EndCap	2.30	0.90	0.50	0.37	0.35	0.33	0.30		
Total, µSv/h		396.4	256.1	217.6	192.7	136.7	95.0	48.6		

Table 28

Dose rate at R= 400 mm, Z= 3443 mm for exposure time T=10 years and different cooling time

Туре	Element	Cooling time, t									
		1 d	3 d	5 d	7 d	15 d	30 d	100 d			
	ID beam pipe	5.22	3.02	2.75	2.69	2.65	2.55	2.33			
	LAr beam pipe	233	196	172	153	109	76	40			
	Pixel type 2 services	39.60	30.50	28.10	26.80	23.80	20.80	14.40			
	Pixel	23.50	15.70	14.20	13.60	12.20	10.90	8.69			
	SCT barrel	0.28	0.20	0.19	0.18	0.17	0.15	0.12			
Hadron	SCT forward	1.47	0.96	0.88	0.86	0.81	0.76	0.64			
activation	SCT barrel services	2.93	2.51	2.32	2.19	1.87	1.55	0.87			
	SCT forward services	4.28	3.68	3.40	3.20	2.70	2.21	1.23			
	TRT	2.27	1.47	1.32	1.25	1.13	1.03	0.89			
	TRT services	2.87	2.39	2.15	1.98	1.57	1.23	0.73			
	LAr Barrel	18.70	14.60	11.80	10.00	6.40	5.90	5.50			
	LAr EndCap	28.00	19.10	16.00	14.20	10.50	8.00	6.00			
	ID beam pipe	0.08	0.01	0.00	0.00	0.00	0.00	0.00			
	LAr beam pipe	11.00	10.80	10.70	10.50	10.10	9.40	7.32			
	Pixel type 2 services	31.60	11.30	9.80	9.65	9.52	9.32	8.61			
	Pixel	3.71	0.47	0.20	0.16	0.13	0.12	0.10			
	SCT barrel	0.18	0.09	0.07	0.07	0.06	0.05	0.04			
Neutron	SCT forward	0.90	0.54	0.46	0.42	0.36	0.34	0.28			
activation	SCT barrel services	10.40	2.10	1.49	1.45	1.43	1.40	1.31			
	SCT forward services	11.50	2.27	1.59	1.54	1.52	1.49	1.40			
	TRT	3.65	1.38	0.76	0.50	0.22	0.17	0.14			
	TRT services	6.45	1.26	0.88	0.85	0.83	0.80	0.71			
	LAr Barrel	19.00	2.40	2.20	2.16	2.07	1.95	1.80			
	LAr EndCap	4.20	3.00	2.10	2.07	2.00	1.95	1.90			
Total, µSv/h		464.8	325.7	285.4	259.3	201.0	157.7	104.7			

Туре	Element	Cooling time, t										
		1 d	3 d	5 d	7 d	15 d	30 d	100 d				
	ID beam pipe	1.20	0.43	0.34	0.32	0.29	0.26	0.20				
	LAr beam pipe	127.	105.	90.5	79.7	53.5	34.5	15.8				
	Pixel type 2 services	25.6	18.1	16.2	15.2	12.8	10.5	5.97				
	Pixel	5.69	2.91	2.41	2.21	1.81	1.47	0.94				
	SCT barrel	0.18	0.11	0.09	0.08	0.07	0.06	0.04				
Hadron	SCT forward	0.85	0.40	0.34	0.32	0.28	0.24	0.16				
activation	SCT barrel services	2.84	2.38	2.17	2.03	1.69	1.35	0.69				
	SCT forward services	3.91	3.29	3.00	2.79	2.30	1.82	0.91				
	TRT	1.73	0.84	0.67	0.60	0.47	0.38	0.26				
	TRT services	2.93	2.38	2.10	1.90	1.43	1.06	0.54				
	LAr Barrel	13.9	8.86	6.90	5.78	3.45	1.96	1.80				
	LAr EndCap	19.0	11.3	9.30	8.08	5.65	3.72	1.70				
	ID beam pipe	0.03	0.00	0.00	0.00	0.00	0.00	0.00				
	LAr beam pipe	3.50	3.38	3.31	3.24	3.00	2.63	1.54				
	Pixel type 2 services	28.5	4.46	2.66	2.50	2.41	2.27	1.81				
	Pixel	0.75	0.10	0.04	0.03	0.03	0.02	0.02				
	SCT barrel	0.14	0.06	0.04	0.04	0.03	0.03	0.02				
Neutron	SCT forward	0.65	0.33	0.25	0.22	0.17	0.16	0.13				
activation	SCT barrel services	10.3	1.08	0.40	0.35	0.34	0.32	0.25				
	SCT forward services	11.2	1.16	0.42	0.37	0.35	0.33	0.27				
	TRT	3.95	1.43	0.74	0.45	0.14	0.09	0.07				
	TRT services	6.83	0.77	0.32	0.29	0.26	0.23	0.16				
	LAr Barrel	15.6	1.03	0.72	0.69	0.63	0.52	0.44				
	LAr EndCap	2.00	0.65	0.43	0.32	0.31	0.30	0.29				
	Total, µSv/h	288.3	170.4	143.4	127.5	91.4	64.2	34.0				

Dose rate at R= 700 mm, Z= 3440 mm for exposure time T=100 days and different cooling time

Dose rate at R= 700 mm, Z= 3440 mm for exposure time T=10 years and different cooling time

Туре	Element	Cooling time, t								
		1 d	3 d	5 d	7 d	15 d	30 d	100 d		
	ID beam pipe	1.90	1.11	1.02	1.00	0.98	0.93	0.84		
	LAr beam pipe	138.0	116.0	102.0	90.8	64.8	45.0	23.7		
	Pixel type 2 services	33.5	26.0	24.0	22.9	20.4	17.9	12.4		
	Pixel	8.05	5.26	4.76	4.55	4.13	3.74	3.05		
	SCT barrel	0.27	0.20	0.18	0.18	0.16	0.15	0.12		
Hadron	SCT forward	1.29	0.85	0.78	0.76	0.71	0.67	0.56		
activation	SCT barrel services	3.30	2.83	2.62	2.47	2.11	1.74	0.98		
	SCT forward services	4.52	3.89	3.59	3.38	2.86	2.34	1.30		
	TRT	2.55	1.65	1.48	1.41	1.28	1.17	1.01		
	TRT services	3.38	2.82	2.54	2.34	1.85	1.46	0.86		
	LAr Barrel	18.4	13.9	11.3	9.58	6.33	6.23	5.90		
	LAr EndCap	23.0	15.8	13.2	11.7	8.66	6.81	5.11		
	ID beam pipe	0.03	0.00	0.00	0.00	0.00	0.00	0.00		
	LAr beam pipe	6.29	6.16	6.08	6.00	5.73	5.29	3.97		
	Pixel type 2 services	37.4	13.3	11.5	11.3	11.2	11.0	10.3		
	Pixel	0.79	0.13	0.08	0.07	0.06	0.06	0.05		
	SCT barrel	0.17	0.08	0.07	0.06	0.06	0.05	0.04		
Neutron	SCT forward	0.81	0.48	0.41	0.37	0.32	0.30	0.25		
activation	SCT barrel services	11.6	2.34	1.66	1.61	1.59	1.56	1.46		
	SCT forward services	12.5	2.48	1.74	1.69	1.67	1.64	1.53		
	TRT	4.04	1.52	0.83	0.54	0.22	0.17	0.14		
	TRT services	7.54	1.47	1.03	0.99	0.96	0.93	0.83		
	LAr Barrel	17.1	2.30	2.11	2.07	1.99	1.84	1.70		
	LAr EndCap	3.44	2.56	1.79	1.76	1.70	1.62	1.58		
Total, µSv/h		339.9	223.1	194.8	177.5	139.8	112.6	77.7		

Туре	Element	Cooling time, t									
		1 d	3 d	5 d	7 d	15 d	30 d	100 d			
	ID beam pipe	8.41	2.67	1.98	1.86	1.70	1.57	1.37			
	LAr beam pipe	1250.	1040.	893.	786.	527.	338.	153.			
	Pixel type 2 services	5.96	4.22	3.77	3.52	2.97	2.43	1.37			
	Pixel	8.56	4.57	3.81	3.49	2.84	2.28	1.41			
	SCT barrel	0.15	0.09	0.08	0.07	0.06	0.05	0.03			
Hadron	SCT forward	0.66	0.32	0.26	0.25	0.21	0.18	0.12			
activation	SCT barrel services	1.91	1.60	1.46	1.36	1.13	0.91	0.46			
	SCT forward services	2.54	2.13	1.94	1.81	1.49	1.18	0.59			
	TRT	1.11	0.54	0.43	0.39	0.31	0.25	0.17			
	TRT services	1.94	1.57	1.39	1.26	0.94	0.70	0.36			
	LAr Barrel	11.3	7.07	5.51	4.62	2.76	1.56	1.53			
	LAr EndCap	31.0	18.5	15.2	13.2	9.24	6.08	3.03			
	ID beam pipe	0.25	0.03	0.01	0.00	0.00	0.00	0.00			
	LAr beam pipe	33.0	31.5	30.7	30.1	27.9	24.5	15.2			
	Pixel type 2 services	6.21	0.99	0.60	0.56	0.54	0.51	0.40			
	Pixel	1.16	0.14	0.05	0.04	0.03	0.03	0.02			
	SCT barrel	0.12	0.05	0.04	0.03	0.03	0.02	0.02			
Neutron	SCT forward	0.51	0.26	0.20	0.17	0.14	0.13	0.10			
activation	SCT barrel services	6.99	0.73	0.27	0.24	0.23	0.22	0.17			
	SCT forward services	7.18	0.74	0.27	0.23	0.22	0.21	0.17			
	TRT	2.33	0.83	0.44	0.28	0.10	0.07	0.06			
	TRT services	4.61	0.52	0.22	0.19	0.18	0.16	0.11			
	LAr Barrel	14.2	0.75	0.52	0.50	0.45	0.38	0.30			
	LAr EndCap	3.10	0.90	0.60	0.45	0.42	0.41	0.40			
	Total, µSv/h	1403.2	1120.7	962.7	850.6	580.9	381.8	180.4			

Dose rate at R= 175 mm, Z= 3800 mm for exposure time T=100 days and different cooling time

Dose rate at R= 175 mm, Z= 3800 mm for exposure time T=10 years and different cooling time

Туре	Element	Cooling time, t								
		1 d	3 d	5 d	7 d	15 d	30 d	100 d		
	ID beam pipe	13.70	7.75	7.06	6.91	6.82	6.59	6.18		
	LAr beam pipe	1360.	1150.	1000.	894.	637.	441.	230.		
	Pixel type 2 services	7.76	6.01	5.55	5.30	4.71	4.11	2.84		
	Pixel	11.90	7.93	7.16	6.83	6.15	5.52	4.42		
	SCT barrel	0.23	0.17	0.16	0.15	0.14	0.13	0.10		
Hadron	SCT forward	1.00	0.66	0.60	0.59	0.55	0.52	0.43		
activation	SCT barrel services	2.22	1.90	1.76	1.66	1.42	1.17	0.66		
	SCT forward services	2.93	2.52	2.33	2.19	1.85	1.51	0.84		
	TRT	1.64	1.07	0.96	0.92	0.83	0.76	0.66		
	TRT services	2.23	1.86	1.68	1.55	1.22	0.96	0.57		
	LAr Barrel	15.20	11.80	9.51	8.06	5.96	5.60	5.22		
	LAr EndCap	37.00	25.30	21.30	18.80	13.90	9.46	7.04		
	ID beam pipe	0.26	0.03	0.01	0.01	0.01	0.01	0.00		
	LAr beam pipe	74.7	73.1	72.2	71.4	68.9	64.9	53.3		
	Pixel type 2 services	8.14	2.92	2.52	2.49	2.46	2.41	2.24		
	Pixel	1.20	0.18	0.09	0.08	0.07	0.07	0.06		
	SCT barrel	0.15	0.07	0.06	0.05	0.05	0.04	0.04		
Neutron	SCT forward	0.63	0.38	0.32	0.29	0.25	0.24	0.20		
activation	SCT barrel services	7.85	1.59	1.14	1.10	1.09	1.07	1.00		
	SCT forward services	8.02	1.59	1.11	1.08	1.06	1.04	0.98		
	TRT	2.41	0.91	0.51	0.35	0.17	0.14	0.12		
	TRT services	5.09	1.00	0.70	0.67	0.65	0.63	0.56		
	LAr Barrel	15.9	1.88	1.72	1.69	1.62	1.41	1.30		
	LAr EndCap	5.03	4.28	3.06	2.94	2.82	2.67	2.67		
Total, µSv/h		1585.2	1304.9	1141.5	1029.1	759.7	551.9	321.4		

	Dose rate at R= 400 mm, Z=	3800 mm f	or exposure	time T=10	0 days and c	lifferent coo	oling time	
Туре	Element			C	ooling time	,t		
		1 d	3 d	5 d	7 d	15 d	30 d	100 d
	ID beam pipe	2.91	0.96	0.72	0.68	0.62	0.57	0.48
	LAr beam pipe	358.	297.	256.	225.	151.	97.4	44.2
	Pixel type 2 services	6.15	4.36	3.89	3.64	3.06	2.51	1.42
	Pixel	6.37	3.35	2.79	2.56	2.08	1.68	1.05
	SCT barrel	0.15	0.09	0.08	0.07	0.06	0.05	0.03
Hadron	SCT forward	0.64	0.30	0.25	0.24	0.21	0.18	0.12
activation	SCT barrel services	1.94	1.62	1.48	1.38	1.15	0.92	0.47
	SCT forward services	2.54	2.13	1.94	1.81	1.49	1.18	0.59
	TRT	1.12	0.54	0.43	0.39	0.31	0.25	0.17
	TRT services	1.99	1.61	1.43	1.29	0.97	0.72	0.37
	LAr Barrel	11.5	7.32	5.70	4.78	2.85	1.66	1.42
	LAr EndCap	27.0	16.4	13.5	11.7	8.20	5.66	2.61
	ID beam pipe	0.08	0.01	0.00	0.00	0.00	0.00	0.00
	LAr beam pipe	9.27	8.91	8.70	8.52	7.89	6.94	4.16
	Pixel type 2 services	6.50	1.03	0.62	0.59	0.57	0.53	0.42
	Pixel	0.87	0.11	0.04	0.03	0.03	0.02	0.02
	SCT barrel	0.12	0.05	0.04	0.03	0.02	0.02	0.02
Neutron	SCT forward	0.49	0.25	0.19	0.17	0.13	0.12	0.10
activation	SCT barrel services	7.07	0.74	0.28	0.24	0.23	0.22	0.18
	SCT forward services	7.23	0.75	0.27	0.24	0.23	0.21	0.17
	TRT	2.33	0.83	0.44	0.27	0.10	0.07	0.06
	TRT services	4.74	0.53	0.23	0.20	0.18	0.16	0.11
	LAr Barrel	12.6	0.87	0.61	0.58	0.53	0.42	0.33
	LAr EndCap	3.64	0.81	0.54	0.44	0.42	0.41	0.40

58.9

121.9

Dose rate at R= 400 mm, Z= 3800 mm for exposure time T=10 years and different cooling time

300.2

264.8

182.3

350.6

475.3

Total, µSv/h

Туре	Element			С	ooling time	,t		
		1 d	3 d	5 d	7 d	15 d	30 d	100 d
	ID beam pipe	4.69	2.68	2.44	2.39	2.36	2.27	2.11
	LAr beam pipe	391.	329.	288.	257.	183.	127.	66.5
	Pixel type 2 services	8.01	6.21	5.73	5.47	4.86	4.25	2.93
	Pixel	8.92	5.90	5.33	5.09	4.59	4.14	3.33
	SCT barrel	0.23	0.17	0.15	0.15	0.14	0.12	0.10
Hadron	SCT forward	0.97	0.63	0.58	0.57	0.53	0.50	0.42
activation	SCT barrel services	2.25	1.92	1.78	1.68	1.44	1.19	0.67
	SCT forward services	2.93	2.52	2.32	2.19	1.85	1.52	0.84
	TRT	1.66	1.08	0.97	0.93	0.84	0.77	0.67
	TRT services	2.30	1.92	1.73	1.59	1.26	0.99	0.58
	LAr Barrel	14.2	10.7	8.61	7.30	4.76	4.62	4.40
	LAr EndCap	32.1	23.2	19.4	17.2	12.7	8.29	6.22
	ID beam pipe	0.08	0.01	0.00	0.00	0.00	0.00	0.00
	LAr beam pipe	18.5	18.1	17.8	17.6	16.9	15.8	12.4
	Pixel type 2 services	8.53	3.05	2.64	2.60	2.57	2.52	2.35
	Pixel	0.91	0.14	0.08	0.07	0.06	0.06	0.05
	SCT barrel	0.14	0.07	0.06	0.05	0.05	0.04	0.04
Neutron	SCT forward	0.61	0.36	0.31	0.28	0.25	0.23	0.19
activation	SCT barrel services	7.95	1.61	1.15	1.11	1.10	1.08	1.01
	SCT forward services	8.08	1.60	1.12	1.09	1.07	1.05	0.99
	TRT	2.40	0.90	0.51	0.35	0.17	0.14	0.12
	TRT services	5.23	1.03	0.72	0.69	0.67	0.65	0.58
	LAr Barrel	13.20	1.90	1.74	1.71	1.64	1.44	1.33
	LAr EndCap	4.51	3.56	2.49	2.45	2.37	2.06	2.01
	Total, µSv/h	539.4	418.3	365.7	329.6	245.2	180.7	109.8

Туре	Element			С	ooling time	, t		
		1 d	3 d	5 d	7 d	15 d	30 d	100 d
	ID beam pipe	1.13	0.39	0.30	0.29	0.26	0.24	0.19
	LAr beam pipe	172.	142.	123.	108.	72.7	47.0	21.5
	Pixel type 2 services	5.21	3.70	3.31	3.09	2.61	2.14	1.21
	Pixel	3.96	2.05	1.70	1.56	1.27	1.03	0.65
	SCT barrel	0.15	0.09	0.07	0.07	0.06	0.05	0.03
Hadron	SCT forward	0.58	0.28	0.23	0.22	0.19	0.16	0.11
activation	SCT barrel services	1.99	1.66	1.52	1.42	1.18	0.95	0.48
	SCT forward services	2.52	2.12	1.93	1.80	1.48	1.17	0.59
	TRT	1.12	0.54	0.43	0.39	0.31	0.25	0.18
	TRT services	2.14	1.73	1.53	1.39	1.04	0.77	0.39
	LAr Barrel	10.5	6.69	5.21	4.37	2.61	1.67	1.43
	LAr EndCap	21.8	12.9	10.6	9.21	6.44	4.33	2.00
	ID beam pipe	0.03	0.00	0.00	0.00	0.00	0.00	0.00
	LAr beam pipe	4.78	4.62	4.52	4.43	4.10	3.60	2.10
	Pixel type 2 services	6.05	0.96	0.57	0.54	0.52	0.49	0.39
	Pixel	0.51	0.07	0.03	0.03	0.02	0.02	0.01
	SCT barrel	0.12	0.05	0.04	0.03	0.02	0.02	0.02
Neutron	SCT forward	0.45	0.23	0.18	0.15	0.12	0.11	0.09
activation	SCT barrel services	7.25	0.76	0.28	0.25	0.24	0.22	0.18
	SCT forward services	7.33	0.76	0.28	0.24	0.23	0.22	0.17
	TRT	2.25	0.79	0.42	0.26	0.10	0.07	0.06
	TRT services	5.09	0.57	0.24	0.21	0.20	0.18	0.12
	LAr Barrel	10.9	0.69	0.48	0.46	0.42	0.40	0.31
	LAr EndCap	2.33	0.78	0.52	0.39	0.38	0.37	0.35
	Total, µSv/h	270.2	184.4	157.4	138.8	96.5	65.5	32.6

Dose rate at R= 700 mm, Z= 3800 mm for exposure time T=100 days and different cooling time

Dose rate at R= 700 mm, Z= 3800 mm for exposure time T=10 years and different cooling time

Туре	Element			С	ooling time	,t		
		1 d	3 d	5 d	7 d	15 d	30 d	100 d
	ID beam pipe	1.81	1.05	0.96	0.94	0.92	0.89	0.81
	LAr beam pipe	188.	158.	138.	123.	88.1	61.3	32.3
	Pixel type 2 services	6.79	5.27	4.86	4.64	4.13	3.61	2.49
	Pixel	5.58	3.66	3.31	3.16	2.86	2.59	2.10
	SCT barrel	0.22	0.16	0.15	0.14	0.13	0.12	0.10
Hadron	SCT forward	0.88	0.58	0.53	0.52	0.49	0.45	0.38
activation	SCT barrel services	2.31	1.98	1.83	1.73	1.48	1.22	0.69
	SCT forward services	2.91	2.50	2.31	2.18	1.84	1.51	0.84
	TRT	1.67	1.09	0.98	0.94	0.85	0.79	0.68
	TRT services	2.47	2.06	1.86	1.71	1.35	1.06	0.63
	LAr Barrel	14.2	10.6	8.61	7.30	4.74	4.51	4.39
	LAr EndCap	26.1	18.0	15.1	13.4	9.91	7.77	5.83
	ID beam pipe	0.03	0.00	0.00	0.00	0.00	0.00	0.00
	LAr beam pipe	8.48	8.30	8.18	8.08	7.70	7.11	5.30
	Pixel type 2 services	7.94	2.84	2.46	2.43	2.40	2.35	2.19
	Pixel	0.54	0.10	0.06	0.05	0.05	0.05	0.04
	SCT barrel	0.14	0.07	0.06	0.05	0.05	0.04	0.04
Neutron	SCT forward	0.56	0.33	0.28	0.26	0.23	0.21	0.18
activation	SCT barrel services	8.14	1.65	1.18	1.14	1.12	1.10	1.03
	SCT forward services	8.20	1.62	1.14	1.10	1.09	1.07	1.00
	TRT	2.32	0.86	0.49	0.33	0.17	0.14	0.11
	TRT services	5.62	1.10	0.77	0.74	0.72	0.69	0.62
	LAr Barrel	12.3	1.71	1.57	1.54	1.48	1.42	1.31
	LAr EndCap	3.90	3.01	2.11	2.08	2.01	1.93	1.88
	Total, µSv/h	311.1	226.6	196.8	177.5	133.8	101.9	64.9

	Result	ts of the cu	rrent study	<u>y</u>								
Distance from Barrel front		T= 180 d			T= 10 y							
surface Z ₀ , cm	t= 1 d	t= 7 d	t= 30 d	t= 1 d	t= 7 d	t= 30 d						
10	4.64	2.25	1.67	6.57	4.16	3.55						
30	2.98	1.45	1.08	4.24	2.69	2.28						
30 2.50 1.10 1.21 2.05 100 0.96 0.46 0.34 1.35 0.86												
]	Results of 1	the study b	y C.Buttar	• et al.								
Distance from Barrel front		T= 180 d			T= 10 y							
surface Z ₀ , cm	t= 1 d	t= 7 d	t= 30 d	t= 1 d	t= 7 d	t= 30 d						
10	7.15	2.78	2.28	9.77	5.37	4.79						
30	4.59	1.78	1.46	6.27	3.45	3.07						
100	1.44	0.56	0.46	1.96	1.08	0.96						

Gamma dose rate (μ Sv/h) along Z axis.

	Result	ts of the cu	rrent study	y										
Distance from Barrel		T= 180 d			T= 10 y									
cylindrical surface R ₀ , cm	t= 1 d	t= 7 d	t= 30 d	t= 1 d	t= 7 d	t= 30 d								
10	7.09	3.43	2.56	10.04	6.36	5.41								
30	3.97	1.92	1.44	5.63	3.57	3.04								
100	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$													
100 1.19 0.57 0.43 1.67 1.06 0.91 Results of the study by C.Buttar et al.														
]	Results of t	the study b	y C.Buttar	· et al.										
] Distance from Barrel	Results of t	the study b T= 180 d	y C.Buttar	et al.	T= 10 y									
Distance from Barrel cylindrical surface R ₀ , cm	Results of t t= 1 d	the study b T= 180 d t= 7 d	y C.Buttar t= 30 d	et al. t= 1 d	T= 10 y t= 7 d	t= 30 d								
Distance from Barrel cylindrical surface R ₀ , cm 10	Results of t t= 1 d 10.53	the study b T= 180 d t= 7 d 4.09	y C.Buttar t= 30 d 3.36	et al. t= 1 d 14.39	T= 10 y t= 7 d 7.91	t= 30 d 7.06								
Distance from Barrel cylindrical surface R_0 , cm 10 30	Results of 1 t= 1 d 10.53 5.85	the study b T= 180 d t= 7 d 4.09 2.28	y C.Buttar t= 30 d 3.36 1.87	et al. t= 1 d 14.39 8	T= 10 y t= 7 d 7.91 4.39	t= 30 d 7.06 3.92								

Addendum 1



Fig. A1.1 General detector opening layout to calculations of access dose rate.

Table 1 (continuation)

												-				
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
5- 10	5	620.4	680.3	1447.5	5172.8	3017.9	2051.2	2700.9	4250.9	3852.4	3431.2	3264.5	3220.6	3268.7	3289	1955.3
10- 20	10	551.2	587.4	902.6	1637.8	1418.1	1103.3	1352	1939.4	1845.4	1695.7	1648.3	1663.6	1718.1	1775.6	1164.8
20- 30	10	456.3	479.9	605.1	796.7	799.2	718	836.3	1101.6	1095.1	1040.9	1035.5	1064.7	1108.7	1175.3	837.1
30- 45	15	394.7	406	433.6	492.6	514.3	506.6	570.3	702.5	720.6	706.6	715.3	743.4	784.4	837.6	617.9
45- 60	15	347.8	352.5	333.2	349.6	364.2	374.8	412.7	483.7	507.1	512.5	522.3	543.7	569.7	602.4	445.8
60- 75	15	289.6	291.5	274.8	278	286.4	297	323	366.6	388.4	396.7	404.6	417	428.1	440.9	316.4
75-95	20	247.9	246.7	231.8	229.1	231	239.2	257	283.4	300.7	309.3	310.3	314.1	316	313.8	214.6
95- 115	20	239	228.9	202.2	192.6	190.9	195.4	206.7	222.3	235.9	238.4	236.2	233	231	223.9	145.1
115- 125	10	223.8	215.3	183.2	172	168.9	171.6	178.8	190.1	199.7	199.7	195.6	189.1	187.3	179.1	112
125- 150	25	177.4	171.8	157.9	151.3	148.5	149.4	153.9	161.9	166.1	166	157.8	152.2	150.2	142.7	86.4
150- 175	25	138.5	135.6	128.2	125.4	123.8	123.4	126.2	131	132	129	119.2	115.4	113.4	107	62.2
175-200	25	110.1	108.6	105.3	104.1	103.2	103.1	105.1	107.8	106.5	102.5	92.5	90.7	88.1	82.3	45.2
200-225	25	89.9	88.3	86.5	86	85.4	86	89.4	89.5	87.2	82.5	73.9	73.5	69.9	65.1	34.2

Equivalent dose rate in the ID access scenario for T= 100d, t=1d

Table A1.1

			L	quivalei			e genera	a access	Social		100 u, t	- 5 0	1		-	
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5															
5- 10	5	362.9	407.5	948.8	3661.8	2134.7	1442.3	1913.6	3040.9	2754	2435.9	2293.7	2233.9	2233.8	2213.9	1236
10- 20	10	316.1	350.3	585	1125.8	981.1	761.2	944.2	1373.6	1299.3	1179.1	1127.3	1112.3	1118	1123.9	670.7
20- 30	10	258.8	280.5	380.3	527.2	536.9	484.5	574.1	768.1	758	707.3	687.6	685.3	691.4	700.5	439.5
30-45	15	215.3	226.6	260.6	310.7	333.2	333.3	383.9	480.9	488.7	468.4	461.8	464.5	473.4	485.8	317.8
45-60	15	180.3	186.1	190	209.6	227.1	239.8	271.5	323.9	335.9	331.6	329.6	333.7	339.8	348.5	231.8
60- 75	15	145.5	148.6	150.4	160	173	185.2	208.1	240.4	252.2	252	252.4	254	256.1	258.6	168.8
75-95	20	119.9	121.3	121.6	127.1	134.8	145.3	161.7	182.2	191.5	194.2	192.2	191.5	190.7	187.8	117.9
95- 115	20	107.2	106.2	102.2	103.5	108.3	116.1	126.8	139.6	148	147.8	146.1	143.1	140.7	136.8	82.4
115- 125	10	98.4	96.9	90.9	91	94.4	99.7	108.1	118.2	124.4	123.4	121.2	117	115.1	110.9	64.6
125- 150	25	81.3	80.6	79.1	79.4	81.6	85.6	91.5	99.2	102.5	102.6	98.1	95.1	92.9	89.3	50.8
150- 175	25	66.7	66.1	65.7	66.2	67.6	70	74.6	79	80.5	79.3	74.8	72.7	70.9	68	37.7
175-200	25	55.9	55.2	55.4	56	56.9	58.4	61.4	64.2	64.5	62.6	58.7	57.1	55.6	53.4	28.4
200-225	25	47.3	46.7	47.1	47.6	47.7	48.8	51.5	53.1	52.7	50.7	47.1	46.4	44.6	43	22.1

Equivalent dose rate in the general access scenario for T= 100 d, t= 5 d

Table A1.1 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/7		540	350	365	380	405	430	480	530	580	605	630	645	660	670	070
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5															
5- 10	5	78.9	86.3	184.3	680.1	387.4	260.2	361.1	604.2	539.9	467.2	436.4	426.4	429.7	431.2	253.5
10- 20	10	69.5	73.6	113.8	211	181.2	140.3	179.9	272.2	254.9	227.5	217.3	215.8	221.3	229.5	148.6
20- 30	10	56.3	59.3	75.6	101	101.4	91.3	110.5	152.1	148.9	136.8	133.2	134.2	138.4	146.3	101.2
30- 45	15	48.7	50.1	53.3	61.4	64.5	64.1	74.7	94.9	95.8	90.7	89.3	90.5	93.5	98	67.5
45- 60	15	42.8	43.5	40.5	42.7	45.2	47.1	53.3	63.6	65.4	63.7	63.6	64.4	65.9	67.7	45.6
60- 75	15	34.3	34.8	32.5	33.3	35.1	36.5	41	46.8	49	48.6	48.3	48.7	49.2	49.5	32.3
75-95	20	28.2	28.5	26.6	26.7	27.7	29	32.1	35.7	37.2	37.1	36.9	36.5	36.5	36	22.4
95-115	20	25.5	24.9	22.9	21.9	22.5	23.3	25.3	27.7	28.6	28.5	28	27.3	27.3	26.4	15.5
115- 125	10	23.8	23	20.4	19.6	19.5	20.4	21.7	23.5	24	23.8	23.2	22.5	22.3	21.4	12.3
125- 150	25	19.5	18.7	17.6	17.3	17.1	17.8	18.5	19.5	19.7	19.6	19	18.3	18.3	17.4	9.7
150- 175	25	15.5	15.1	14.5	14.4	14.2	14.6	15.1	15.5	15.6	15.4	14.5	14.2	14.1	13.3	7.1
175-200	25	12.9	12.7	12	11.9	12	11.9	12.6	12.8	12.6	12.3	11.4	11.4	11.1	10.6	5.4
200-225	25	10.7	10.3	10.2	10	10	10.3	10.7	10.4	10.4	10	9.3	9.4	9	8.5	4.1

Equivalent dose rate in the general access scenario for T= 100 d, t=100d

Table 1 (continuation)

Equivalent dose rate in the ID access scenario for T= 10y, t=1d

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	I
5- 10	5	729.2	797.2	1662.4	5873.5	3376.9	2287.1	3002.2	4701.9	4261.1	3806	3633.6	3598.6	3673.2	3718.5	2254.4
10- 20	10	650.1	685	1033.7	1855.9	1595.2	1235.4	1506.4	2155.8	2049.5	1894.1	1852.4	1883	1961.7	2055.2	1390.5
20- 30	10	534.2	557.8	694.7	906.7	902.9	807.8	935.5	1227.6	1222.8	1171	1175.1	1219.1	1286.4	1391	1033.1
30- 45	15	462.6	474.5	499.7	562.7	583.8	572.2	641	786.8	810	801.3	818.5	859.1	916.1	993.1	758.1
45- 60	15	410.9	415.3	386.1	400.6	415.3	425.6	466	544.7	573	584.1	601.3	632.1	667.5	709.7	538.8
60- 75	15	341	342.3	319.1	319.6	327.9	337.7	365.9	414.2	441.6	455.2	466.5	484.5	502	516.9	378
75-95	20	290.3	289	269.1	263.9	265.9	273.1	292.6	322.1	343.9	355.6	359	364.6	369.3	368.2	258.2
95-115	20	278.3	266.7	234.5	222.3	219.6	224.6	236.5	254	270.2	275.4	273.3	269.8	269.2	261.4	173.3
115- 125	10	261.4	250.6	212.5	199.2	195.2	197.2	205.5	217.8	229.2	230.8	225.7	218.9	218	208.4	133.2
125- 150	25	208.4	201.1	183.7	175.8	172.4	172.5	177	185.6	191.7	191.8	182	175.6	174.5	164.9	102.2
150-175	25	163.2	159.3	150.5	146.8	144.2	143	145.2	150.7	152.1	149.6	136.8	133	131.2	122.5	72.6
175-200	25	131.4	128.4	124.3	122.4	120.4	119.3	121.5	124.5	122.9	118.2	105.7	104.5	101	93.4	52.5
200-225	25	107.1	104.6	102.3	100.9	99.6	100	103.5	103.5	100.7	94.7	84.4	84.4	79.2	73.3	39.3

Table A1.1 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5															
5- 10	5	470.3	522.4	1163.1	4347	2485.3	1673.6	2207.2	3489.5	3152.5	2792.8	2646.3	2598	2624.9	2628.2	1529.4
10-20	10	414.5	446.3	714	1341	1155.8	890.3	1095.1	1582.4	1500	1369.2	1324.6	1326.2	1358.8	1397.9	895
20- 30	10	336.3	357.4	468	634.3	639	572.6	671.5	892.7	883.4	833	822.6	837.2	865.8	912	631.9
30- 45	15	282.7	294.4	325.2	379.5	401.3	397.6	453.3	564.1	576.2	559.9	561.7	578.3	604.3	638.6	453.3
45- 60	15	243	247.9	242	260.2	276.9	289.5	324.1	384	401	401.6	406.9	419.2	436.2	455.1	327.2
60- 75	15	196.1	199	194	201.5	213.3	225.7	250.4	287.4	304.4	309.2	313.7	320.5	327.9	334.7	231.4
75-95	20	162.2	163.3	158.3	161.6	168.6	178.5	196.6	220	234	239.5	240.4	241.6	242.9	241.1	160.5
95- 115	20	146.2	143.5	134.1	132.9	136.7	144.2	156	171.2	181.9	184.5	182.9	179.8	178.9	173.6	110.2
115- 125	10	135.2	132.1	120.5	117.8	120.5	125.2	134.2	145.2	153.5	154.1	151.3	146.3	145.2	139.3	85.6
125- 150	25	112.2	109.8	104.7	103.7	104.9	108.3	114.4	122.3	127.3	128	121.9	118.2	116.9	111.5	66.4
150- 175	25	91.8	90	87.7	87	87.5	89.5	93.2	98.8	100.2	99.4	92.3	90	88.5	84	48
175-200	25	76.2	74.7	74.3	74	73.9	74.6	77.6	80.8	80.5	78.6	71.7	70.8	68.8	64.6	35.5
200-225	25	64.6	63.1	62.4	62.4	61.9	62.8	65.5	66.8	66.3	62.8	57.4	57.3	54.3	50.8	26.8

Equivalent dose rate in the general access scenario for T= 10y, t= 5 d

Table A1.1 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,		0.0	350	365	380	405	430	480	530	580	605	630	645	660	670	0,0
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5															
5- 10	5	169	182.1	355.8	1218.4	657.1	432.9	575.1	920.1	822	725.4	694.5	700.5	729.1	753.1	491.1
10- 20	10	151.9	153.7	218.2	381.1	315.5	239	292.2	423.3	400	369.5	367	383.3	413.6	453.8	340
20- 30	10	120.9	123.2	147	186.5	180.7	159.2	183.7	243	241.8	233.9	239.1	256.5	282.7	327.1	275.9
30- 45	15	104.9	106.7	106.8	116.6	118.3	114.5	127.5	157.1	162.5	163.2	169.6	184.3	203.5	229.6	190.7
45- 60	15	95.5	96.1	83.1	83.8	85.3	86.4	93.9	109.7	116.2	120.5	126.6	136.4	147.4	159.1	128
60- 75	15	77.1	77.6	68.7	67.1	67.9	69.3	74.3	84.1	90.5	95.5	98.7	104.6	110.2	114.5	89.2
75- 95	20	63.9	63.9	57.3	55.5	55.1	56	59.6	66.1	71.6	74.7	76.5	78.2	80.8	80.9	60.4
95- 115	20	58.7	56.9	49.9	46.6	45.8	46.4	48.9	52.9	56.5	58.3	58	57.8	58.7	56.9	40.3
115- 125	10	55.4	52.9	44.9	42.2	41.1	41.3	43.2	45.3	48.3	49	47.9	46.7	47.3	44.8	30.7
125- 150	25	45.3	43.8	39.6	37.3	36.5	36.4	37.4	38.6	40.9	40.5	38.4	37.3	37.8	35	23.3
150- 175	25	36.4	35.4	33.3	32.2	31.5	30.9	30.7	31.9	32.6	31.8	28.6	28.1	28	25.4	16.2
175-200	25	30.3	29.4	28	27.1	26.4	25.4	26.2	26.9	26.1	25.1	21.7	22	21.1	19	11.4
200-225	25	25.6	24.5	23.5	22.8	22	22	22.5	22.2	21.5	19.7	16.9	17.6	16.2	14.6	8.1

Equivalent dose rate in the general access scenario for T= 10y, t= 100 d



Fig. A1.2. Detector opening layout to calculations of access dose rate -- Lar EndCap removed.

												,				
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	-	-	-	198.4	116.1	99	96	104.4	133.9	193.6	268.2	359.2	476.8	655.1	734.8
5- 10	5	258	233	216.1	161.8	113.1	96.3	93	100.5	129.5	184.1	251.1	336	436.5	562.7	602.5
10- 20	10	226.9	202.4	162.7	136.2	110	94.5	90.4	97.3	127	177.2	230.5	307.9	397	500.7	532.6
20- 30	10	186.3	173.7	143.6	123.4	105.5	91.6	86.6	92.8	121.6	163.6	211.8	277.1	346.2	436	469.9
30- 45	15	183.4	175.8	134.8	115.2	99.8	87.9	80.7	86.1	110.3	144.6	184.4	235.4	293	360.5	380.7
45- 60	15	185	179.8	128.3	108.6	93.5	83.3	75.5	80.4	100.3	130.1	158.7	194.7	231.8	273.8	282.3
60- 75	15	159	155.1	120	102.2	88.6	78.6	71.8	75.6	92.3	114	133.6	156.2	175.3	194.5	193.8
75- 95	20	142.9	138.2	111.7	95.7	82.2	73.7	68.4	69.6	81.6	97.5	106	116.6	124	126.4	121.4
95-115	20	153.7	141.3	107.2	88.8	76.3	68.3	63.2	62.5	71.6	77.8	80.5	81.5	83.3	79.8	73.4
115- 125	10	149.3	139	101.3	83.5	71.9	64.7	59	57.9	63.6	65.9	65.1	62.3	63.2	57.7	51.5
125- 150	25	112.7	105.7	87.7	76	66.7	60	54.5	53.1	54.1	55.3	49.6	46.6	46.6	41.1	35.8
150- 175	25	84.3	80.5	70.2	63.9	57.8	52	47.8	46	44.4	42.1	33.8	31.8	31.3	26.3	22
175- 200	25	63.9	61.6	56.3	52.6	48.4	44.4	41.4	39.2	35.9	32.3	23.4	22.8	21.2	16.5	12.5
200-225	25	49.7	47.7	44.4	42	38.9	36.7	36.3	32.9	29.1	24.6	16.6	17.2	14.4	10.4	6.9

Equivalent dose rate in the ID access scenario without LA beam-pipe for T= 100d, t=1d

Table A1.2

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5															
5- 10	5	348.3	392.8	933.3	3645.1	2116.5	1421.7	1888.6	3006.5	2702.5	2357.9	2184.7	2090.8	2051.9	1981.1	982.4
10- 20	10	302.3	336.1	570	1109.8	963.5	741.4	920	1340.2	1248.8	1105.2	1029.5	984.1	956.9	925.9	460
20- 30	10	245.7	267.1	366.1	512.1	520.4	465.9	551.3	736.7	710.4	640.1	599.1	572.1	554.1	536.9	266.3
30- 45	15	203.4	214.5	247.8	297.2	318.4	316.7	363.8	453	447.6	411.5	386.7	369.8	357.6	347.2	172.3
45-60	15	169.8	175.4	178.8	197.6	214.1	225.2	253.6	299.2	300.1	281.1	265.4	254.5	246.4	239.4	118.7
60- 75	15	135.9	138.9	140.3	149.3	161.4	172	191.7	217.8	219.9	208.8	198.3	190.6	184.8	180.1	89.3
75-95	20	111.4	112.7	112.6	117.6	124.4	133.3	146.6	162	163.9	157.5	150	144.6	140.8	137.1	68
95- 115	20	99.7	98.5	94.1	94.8	98.5	104.8	113.2	122.4	124.1	119.9	114.8	111.3	108.4	105.9	52.6
115- 125	10	91.3	89.6	83.1	82.6	85	89.2	95.8	102.5	103.8	100.7	96.4	93.7	91.5	89.4	44.3
125- 150	25	74.4	73.6	71.6	71.4	72.8	76	80.6	85	86	84	80.2	78.3	76.4	74.8	37.1
150- 175	25	60.1	59.4	58.7	58.9	59.8	61.7	65	67.6	68.2	66.5	63.5	62.2	60.8	59.7	29.7
175-200	25	49.8	49	49.1	49.5	50.1	51.3	53.5	55.2	55.3	54	51.8	50.6	49.7	48.9	24.3
200-225	25	41.8	41.2	41.6	42.1	42.3	43.1	44.7	46	46	45	42.9	42.2	41.5	41	20.3

Equivalent dose rate in the ID access scenario for T= 100 d, t= 5 d -- Lar EndCap removed

Table A1.2 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5															
5- 10	5	76	83.4	181.1	676.7	383.7	255.9	355.7	596.5	527.7	448.3	408.8	387.5	377.1	362	179
10- 20	10	66.7	70.8	110.8	207.7	177.6	136.1	174.7	264.8	243.5	210.2	193.2	182.7	176.5	170.1	84.1
20- 30	10	53.6	56.5	72.7	97.9	97.9	87.4	105.6	145.2	138.5	121.8	112.6	106.5	102.7	99.1	49
30- 45	15	46.2	47.6	50.6	58.5	61.4	60.5	70.3	89	87.1	78.4	72.8	69.1	66.5	64.3	31.6
45- 60	15	40.5	41.2	38.1	40.2	42.4	44	49.6	58.7	58.3	53.5	50.1	47.8	46.1	44.6	21.9
60- 75	15	32.3	32.8	30.4	31.1	32.7	33.9	37.9	42.6	42.7	39.8	37.5	35.9	34.7	33.7	16.5
75-95	20	26.5	26.8	24.9	24.9	25.7	26.9	29.5	31.9	31.7	30	28.5	27.3	26.5	25.8	12.5
95-115	20	24.2	23.6	21.5	20.5	20.8	21.4	22.7	24.3	24.1	23	21.8	21.1	20.6	20	9.6
115- 125	10	22.6	21.8	19.1	18.2	17.8	18.4	19.2	20.5	20.1	19.2	18.3	17.8	17.3	17	8.1
125- 150	25	18.3	17.5	16.3	15.8	15.4	15.9	16.3	17	16.5	16	15.4	14.9	14.6	14.3	6.8
150- 175	25	14.2	13.8	13.1	12.9	12.6	13	13.4	13.4	13.2	12.8	12.2	11.9	11.7	11.5	5.4
175-200	25	11.6	11.4	10.7	10.7	10.8	10.7	11.2	11	10.8	10.5	10	9.8	9.6	9.5	4.5
200-225	25	9.7	9.4	9.3	9.1	9.1	9.3	9.3	9	9	8.8	8.4	8.2	8.1	8	3.7

Equivalent dose rate in the ID access scenario for T= 100 d, t= 100 d-- Lar EndCap removed

Table 2 (continuation)

Equivalent dose rate in the ID	access scenario without L	A beam_ning for T= 10v t=1d
	access scenario without L	A Dealth-Dide Iol $I = 100$. $I = 10$

												, ,				
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	-	-	-	271.2	144	121.4	118.2	129.8	169.3	241.9	337.7	453.6	609.7	828.9	922.2
5- 10	5	325.3	298.7	292.9	212.8	140.1	118.3	114.3	124.7	162.3	231.8	317.5	428.9	561.5	722.2	769.3
10- 20	10	288.8	255.9	208.5	172.2	135.9	115.8	111	120.8	158.2	222.2	292.7	393.7	513.2	654.2	696.3
20- 30	10	233.2	216.3	179.5	153.6	129.8	112.5	106.3	114.9	150.9	205.4	268.6	353.3	448.6	579.4	630
30- 45	15	227.1	217.9	166.6	141.9	122.4	107.9	99.4	106.5	137.6	182.7	234.5	300.7	376	469.2	497.9
45- 60	15	230	223.5	157.7	132.6	114.4	102.3	93	99.5	124.9	163.3	201.2	248.6	296.3	348.9	359.5
60- 75	15	196.2	190.9	146.9	124.2	108.3	95.6	88.2	93.2	115	143.7	168.5	197.8	223.7	246.2	243.4
75- 95	20	173.8	168.5	135.9	116	100.8	89.8	84	86.1	102.4	122.2	134.2	147.5	158	162.1	155.7
95- 115	20	183.7	169.6	129.1	107.4	92.8	84.1	78	77.7	89.2	98.6	101.8	103.5	106.9	102.8	94.4
115- 125	10	178.8	166.1	121.8	101.1	87.8	79	73.2	71.8	79.1	83.3	82.2	79.1	81.4	74.5	66.5
125- 150	25	136.7	128	105.9	92.5	81.9	73.6	67.2	65.6	68.2	69.9	62.9	59.2	60.7	53.3	46.6
150- 175	25	103.3	98.3	86.3	78.7	71.1	64	58.6	56.9	55.6	53.8	42.8	41	40.9	33.7	28.4
175-200	25	80.2	76.5	70.1	65.4	59.8	54.4	51.1	48.9	45.1	40.9	29.5	29.7	27.5	21	16.5
200-225	25	62.7	59.7	55.6	52.3	48.3	45.6	44.9	41	36.7	30.9	21.3	22.3	18.1	13.1	9.2

Table A1.2 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5															
5- 10	5	448.6	500.3	1139.8	4322.1	2457.9	1642.8	2169.4	3436.6	3072.2	2671.1	2472.9	2363.6	2319.1	2237.1	1110.7
10- 20	10	393.8	425.2	691.6	1317.1	1129.5	860.7	1058.8	1531.6	1422.4	1253.9	1166.6	1113.4	1083.3	1046.5	519.2
20- 30	10	316.8	337.5	446.9	611.7	614.3	544.7	637.4	845.1	810.4	727.5	679.6	648.8	627.4	608.1	302.1
30- 45	15	264.9	276.3	306.1	359.1	379	372.6	422.7	521.3	511.9	468.5	439.3	419.7	405.6	393.3	195.5
45- 60	15	226.9	231.6	224.9	242.1	257.1	267.2	296.7	345.7	344.5	321.1	302.3	289.1	280	271.7	134.9
60- 75	15	181.7	184.2	178.5	185.1	195.5	205.6	225.3	252.4	253.4	239.3	226.1	217	210.6	205	101.7
75-95	20	149.3	150.2	144.6	147.1	152.7	160.3	173.4	188.5	189.7	181	171.7	165.3	160.5	156.5	77.7
95- 115	20	134.9	132.1	121.9	119.8	121.9	127	134.9	143.8	144.1	138.9	131.9	127.4	124.3	121.4	60.2
115- 125	10	124.6	121.3	108.8	105	106.1	108.8	114.7	120.3	120.8	116.8	110.9	107.3	104.7	102.6	50.9
125- 150	25	101.8	99.2	93.2	91.2	91.2	93	96.9	100.2	100.6	97.7	92.2	89.8	87.9	86.2	42.6
150-175	25	81.4	79.4	76.6	75.3	75.1	76.3	78.5	80.6	80.1	78.1	73.4	71.7	70.3	69.2	34.1
175-200	25	66.4	64.9	64.2	63.7	63.4	63.8	65.2	66.1	65.4	63.7	60	58.7	57.8	56.6	28.1
200-225	25	56.2	54.7	54	54.2	53.6	53.9	54.5	55.4	54.9	53	50.1	49.2	48.2	47.1	23.5

Equivalent dose rate in the ID access scenario for T= 10y, t= 5 d--- Lar EndCap removed

Table A1.2 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
D/7		540	250	265	200-	405	420	400	F20	500-	60F	620	645	660	670	070
κ/Ζ,			350	305	300	405	430	400	530	000	605	030	045	000	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5															
5- 10	5	159.6	172.6	345.7	1207.5	645.1	419.4	558.1	895.7	783.8	666.8	609.1	579.4	564	542	268.7
10- 20	10	142.9	144.6	208.6	370.7	304	226.1	276	400.2	364	314.5	288.5	273.6	264.6	255.5	126.9
20- 30	10	112.4	114.5	137.8	176.7	169.9	146.9	168.6	221.6	208.5	183.8	168.6	160	154.3	149	74.2
30- 45	15	97	98.7	98.3	107.6	108.4	103.3	113.7	137.7	132.6	119.3	109.5	104.2	100.3	97	48.3
45- 60	15	88.3	88.8	75.4	75.6	76.3	76.3	81.5	92.4	90	82.4	75.8	72.2	69.7	67.5	33.8
60- 75	15	70.5	70.9	61.7	59.7	59.9	60.3	63.2	68.5	67	62.1	57	54.5	52.8	51	25.7
75-95	20	58.2	58.1	51.2	49.1	48.2	48.1	49.5	51.8	50.8	47.5	43.5	41.8	40.6	39.2	19.8
95- 115	20	53.9	52	44.7	41.1	39.5	39	39.3	40.2	39.2	36.5	33.6	32.5	31.4	30.6	15.5
115- 125	10	50.9	48.3	40	36.8	34.8	33.9	34.1	33.9	33.2	31	28.5	27.5	26.6	26	13.3
125- 150	25	40.8	39.2	34.5	31.8	30.2	29.3	29.3	28.7	28.1	26.2	23.8	23.2	22.5	22	11.1
150- 175	25	31.6	30.5	28.1	26.7	25.7	24.9	24.3	23.5	22.9	21.2	19.2	18.5	18.1	17.7	8.9
175-200	25	25.6	24.7	23.3	22.5	21.8	20.8	20.6	19.7	18.8	17.5	15.7	15.2	14.9	14.7	7.4
200-225	25	21.9	20.9	19.9	19.3	18.5	18	17.2	16.8	15.7	14.7	13.1	12.8	12.6	12.5	6.2

Equivalent dose rate in the ID access scenario for T= 10 y, t= 100 d-- Lar EndCap removed



Fig. A1.3. Detector opening layout to calculations of access dose rate – Lar EC and VA removed.

		E			:			:. f T					Table /	41.3 (co	ntinuatio	n)
		Equ	ivalent c	lose rate		J access	s scenar		100 a, i	= 5 a - 1	Lar EC a	ina va r	emovea			
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5				42.2	22	14.9	11.5	7.8	5.2	4.5	2.3	2	1.9	1.8	0.6
5- 10	5	87.5	71.2	50.7	34.8	21.9	14.9	11.5	7.8	5.2	4.5	2.3	2	1.9	1.8	0.6
10- 20	10	68.9	58.9	38.5	29.4	21.4	14.7	11.5	7.8	5.5	4.5	2.3	2	1.9	1.8	0.6
20- 30	10	51.2	46.7	34.1	27	20.6	15	11.2	7.6	5.6	4.5	2.3	2	1.9	1.8	0.6
30- 45	15	51.2	48.5	32.6	25.5	19.7	15.2	10.9	7.7	5.7	4.4	2.3	2	1.9	1.8	0.6
45- 60	15	52.5	50.9	31	23.9	18.9	15.2	10.3	7.8	5.7	4.2	2.3	2	1.9	1.8	0.6
60- 75	15	41.9	40.8	28.7	22.4	18.6	14.5	10.5	7.7	5.5	4.2	2.3	1.9	1.9	1.8	0.6
75- 95	20	35.8	34.5	26.1	21.5	17	13.9	10.4	7.5	5.5	4.2	2.2	1.9	1.9	1.6	0.6
95- 115	20	38.1	35.3	25.6	20	15.9	13.2	9.7	7	5.3	3.8	2.1	1.9	1.8	1.5	0.6
115- 125	10	37.5	34.6	24	18.7	15	12.1	9.3	6.9	5.3	3.9	2	1.9	1.8	1.5	0.6
125- 150	25	27.8	25.9	20.9	17	13.8	11.5	8.9	6.4	5	3.9	1.9	1.9	1.6	1.5	0.6
150- 175	25	21	19.7	16.8	14.5	12.2	10.1	8.3	6.1	4.9	3.6	1.9	1.8	1.5	1.4	0.6
175-200	25	16.4	15.1	13.8	12.3	10.6	8.9	7.5	5.6	4.3	3.3	1.9	1.6	1.4	1.4	0.6
200-225	25	12.8	11.9	11.1	10.3	8.8	7.5	6.4	5.1	4	3.1	1.6	1.5	1.4	1.4	0.6

		Equi	valent d	oso rato	in the II		scenari	o for T-	100 d t	-100d	l ar EC a	and $\sqrt{\Lambda}$ r	Table /	A1.3 (coi	ntinuatio	n)
		240		350-	365-	380-		430-	100 u, t 480-	-1000- 530-		605-		645-	660-	670
R/Z.		540	350	365	380	405	430	480	530	580	605	630	645	660	670	070
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5				20.5	7.8	5	3.8	2.5	1.5	1	0.6	0.6	0.6	0.6	0.6
5- 10	5	28.8	25.2	23	15.1	7.7	5	3.7	2.5	1.5	1	0.6	0.6	0.6	0.6	0.6
10- 20	10	24.4	20.6	14.9	11.3	7.4	5	3.7	2.5	1.5	1	0.6	0.6	0.6	0.6	0.6
20- 30	10	18.2	16.4	12.4	9.8	7.2	5.1	3.7	2.5	1.7	1	0.6	0.6	0.6	0.6	0.6
30- 45	15	18.4	17.3	11.4	8.9	6.8	5	3.6	2.4	1.7	1	0.6	0.6	0.6	0.6	0.6
45- 60	15	19	18.4	11	8.3	6.6	5	3.6	2.4	1.7	1	0.6	0.6	0.6	0.6	0.6
60- 75	15	15	14.7	9.9	7.7	6.3	4.6	3.7	2.3	1.6	1	0.6	0.6	0.6	0.6	0.6
75- 95	20	12.5	12.3	8.9	7.1	5.8	4.6	3.7	2.3	1.5	1	0.6	0.6	0.6	0.6	0.6
95- 115	20	12.8	11.8	8.7	6.5	5.4	4.3	3.2	2.3	1.5	1	0.6	0.6	0.6	0.6	0.6
115- 125	10	12.6	11.6	8.1	6.3	4.7	3.9	2.9	2.3	1.4	1	0.6	0.6	0.6	0.6	0.6
125- 150	25	9.6	8.6	6.8	5.7	4.4	3.8	2.8	2.1	1.2	1	0.6	0.6	0.6	0.6	0.6
150- 175	25	6.9	6.4	5.3	4.6	3.7	3.3	2.7	1.8	1.2	1	0.6	0.6	0.6	0.6	0.6
175-200	25	5.3	5	4.1	3.8	3.4	2.8	2.5	1.6	1.2	1	0.6	0.6	0.6	0.6	0.6
200-225	25	4.3	3.9	3.6	3.2	2.8	2.6	2.1	1.3	1.1	0.9	0.6	0.6	0.6	0.6	0.6

Table A1.3 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5				104.6	40.2	26.5	19.9	13.4	9	7.1	4.1	3.8	3.2	3.1	1.7
5- 10	5	147.4	128.5	118.2	76.5	39.7	26.4	19.8	13.4	9	7.1	4.1	3.6	3.2	3.1	1.7
10- 20	10	124.1	104.9	76.2	57.1	38.3	26.3	19.7	13.4	9.2	7.1	4.1	3.6	3.2	3.1	1.7
20- 30	10	92	82.8	62.3	48.9	36.7	26.3	19.4	13.4	9.5	7.1	4.1	3.6	3.2	3.1	1.7
30- 45	15	89.2	84.4	57.4	44.9	34.5	26.3	18.8	13.3	9.6	7	4	3.5	3.2	3	1.6
45- 60	15	91.8	88.4	54.4	41.8	32.7	26	18.4	13.4	9.7	7.1	4	3.3	3.2	3	1.3
60- 75	15	73.6	71.2	50	39.2	31.5	24.8	18.1	12.8	9.8	7.1	4	3.3	3.2	3	1.3
75-95	20	62.4	60.3	45.2	36.8	29.4	23.5	17.7	12.5	9.6	6.9	4	3.3	3.2	3	1.3
95- 115	20	64.3	59.6	43.3	34	27.1	22.1	16.6	12.1	9	6.9	4	3.2	3.2	3	1.3
115- 125	10	63	58.2	41	31.8	25.9	20.5	15.9	11.4	8.7	6.8	3.8	3.2	3	3	1.3
125- 150	25	48.3	44.6	35.2	29	23.7	19.2	15.1	10.7	8.5	6.8	3.4	3.2	3	3	1.2
150- 175	25	36.7	33.9	28.7	24.5	20.6	17.4	13.8	10.6	8.1	6.7	3.3	3.1	3	3	1.2
175-200	25	28.2	26.2	23.8	21.2	18.2	15.4	12.7	9.7	7.4	6.1	3.2	3	3	2.7	1.2
200-225	25	23.1	21.2	19.2	17.9	15.3	13.2	10.8	8.8	7.1	5.4	3.1	3	2.7	2.2	1.2

Equivalent dose rate in the ID access scenario for T= 10y, t= 5 d– Lar EC and VA removed

		Г au	ivelent e		in the l			ia far T-	40.7 1-	400 - 1	ar 50 a		Table /	41.3 (coi	ntinuatio	n)
		Equ					s scenar	10 for 1 =	10y, t = 400		_arec a			C 4 F	000	070
		340	340-	350-	305-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660- 670	670
κ/Ζ,			350	305	300	405	430	400	530	000	005	030	045	000	070	-
cm	dR\d∠	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5				78.2	23.9	15.6	11	7.6	5	4.1	1.8	1.8	1.7	1.7	1
5- 10	5	81.9	76.8	85.7	53.8	23.5	15.5	11	7.6	5.1	4.1	1.8	1.8	1.7	1.7	1
10- 20	10	73.3	62	49.4	36.6	22.4	15.5	11	7.5	5.1	4.1	1.8	1.8	1.7	1.7	1
20- 30	10	54.4	48.7	38.1	29.8	21.1	15.3	10.9	7.5	5.2	4.1	1.8	1.8	1.7	1.6	1
30- 45	15	51.7	49.2	34	26.3	19.9	15.1	10.6	7.5	5.3	4.1	1.8	1.8	1.7	1.6	1
45- 60	15	53.6	52	31.5	24	18.7	14.7	10.5	7.4	5.3	4	1.8	1.7	1.7	1.6	1
60- 75	15	42.8	41.9	28.7	22.3	18	14.2	10.4	7.4	5.4	4	1.8	1.7	1.7	1.4	1
75- 95	20	35.9	35.1	25.8	20.8	16.7	13.2	9.9	7.1	5.3	3.9	1.8	1.7	1.7	1.4	1
95- 115	20	35.9	33.5	24.6	19.2	15.4	12.3	9.2	6.8	5.2	3.5	1.8	1.7	1.5	1.4	1
115- 125	10	35.2	32.2	22.8	18.1	14.4	11.4	9	6.3	5	3.5	1.8	1.7	1.4	1.4	1
125- 150	25	27.2	25.3	19.7	16	13.1	10.5	8.5	6	4.9	3.4	1.7	1.7	1.4	1.4	0.9
150- 175	25	20.2	19	15.9	13.8	11.8	9.9	7.9	5.9	4.8	3.3	1.7	1.4	1.4	1.3	0.7
175-200	25	15.9	14.9	13.1	11.7	10.3	8.6	7.3	5.5	4.2	3.1	1.6	1.4	1.3	1.3	0.7
200-225	25	13.5	12.4	11.1	10.1	8.8	7.7	6.2	5.1	3.7	2.8	1.4	1.3	1.3	1.3	0.6



Fig. A1.4. Detector opening layout to calculations of access dose rate – Lar EC, VA, Pixel, and VI removed.

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,		010	350	365	380	405	430	480	530	580	605	630	645	660	670	010
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	26.4	25	21.9	20.1	17.5	12.8	10.4	7.2	4.7	4.2	2	1.8	1.7	1.6	0.5
5- 10	5	26.5	25.1	22.1	20.3	17.5	12.8	10.4	7.2	4.7	4.2	2	1.8	1.7	1.6	0.5
10- 20	10	27	25.8	22.4	20.4	17.4	12.7	10.4	7.2	5	4.2	2	1.8	1.7	1.6	0.5
20- 30	10	28.4	27.3	23.7	20.7	17.2	13.1	10.1	7	5.1	4.2	2	1.8	1.7	1.6	0.5
30- 45	15	40	38.4	26	21	16.9	13.5	9.9	7.1	5.3	4.1	2	1.8	1.7	1.6	0.5
45- 60	15	47.7	46.2	26.9	20.8	16.7	13.7	9.4	7.2	5.3	3.9	2	1.8	1.7	1.6	0.5
60- 75	15	38.9	37.8	26	20.2	16.8	13.2	9.6	7.1	5.1	3.9	2	1.7	1.7	1.6	0.5
75- 95	20	33.8	32.5	24.3	19.8	15.6	12.7	9.6	6.9	5.2	3.9	1.9	1.7	1.7	1.4	0.5
95- 115	20	36.6	33.8	24.2	18.7	14.8	12.3	9	6.5	5	3.5	1.9	1.7	1.6	1.3	0.5
115- 125	10	36.3	33.4	22.9	17.6	14	11.3	8.6	6.4	5	3.6	1.8	1.7	1.6	1.3	0.5
125- 150	25	26.8	24.9	19.9	16.1	13	10.7	8.3	5.9	4.7	3.6	1.7	1.7	1.4	1.3	0.5
150- 175	25	20.1	18.8	16	13.7	11.5	9.4	7.7	5.7	4.6	3.4	1.7	1.6	1.3	1.2	0.5
175-200	25	15.7	14.4	13.1	11.6	10	8.3	7.1	5.3	4	3.1	1.7	1.4	1.2	1.2	0.5
200-225	25	12.1	11.2	10.5	9.7	8.2	7.1	6	4.8	3.7	2.9	1.4	1.3	1.2	1.2	0.5

Table A1.4 (continuation) Equivalent dose rate in the ID access scenario for T= 100 d, t= 5 d– Lar EC, VA, Pixel, and VI removed

Table A1.4 (continuation)

	_ ~	240	240	250	265	200	405	120	100	520	590	605	620	645	660	670
		340	340-	350-	305-	300-	405-	430-	400-	550-	000-	005-	030-	045-	000-	070
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	8.5	8.1	7.3	6.8	5.6	4.1	3.4	2.2	1.4	0.9	0.5	0.5	0.5	0.5	0.5
5- 10	5	8.5	8.1	7.3	6.8	5.6	4.1	3.3	2.2	1.4	0.9	0.5	0.5	0.5	0.5	0.5
10- 20	10	8.7	8.3	7.5	6.8	5.6	4.1	3.3	2.2	1.4	0.9	0.5	0.5	0.5	0.5	0.5
20- 30	10	9.3	8.9	8	6.9	5.6	4.2	3.3	2.2	1.6	0.9	0.5	0.5	0.5	0.5	0.5
30- 45	15	14	13.4	8.7	7	5.6	4.3	3.2	2.2	1.6	0.9	0.5	0.5	0.5	0.5	0.5
45- 60	15	17.1	16.5	9.3	7	5.6	4.3	3.2	2.2	1.6	0.9	0.5	0.5	0.5	0.5	0.5
60- 75	15	13.8	13.5	8.8	6.8	5.5	4.1	3.3	2.1	1.5	0.9	0.5	0.5	0.5	0.5	0.5
75-95	20	11.7	11.5	8.2	6.4	5.2	4.1	3.3	2.1	1.4	0.9	0.5	0.5	0.5	0.5	0.5
95- 115	20	12.2	11.2	8.1	6	4.9	3.9	2.9	2.1	1.4	0.9	0.5	0.5	0.5	0.5	0.5
115- 125	10	12.1	11.1	7.6	5.8	4.3	3.5	2.7	2.1	1.3	0.9	0.5	0.5	0.5	0.5	0.5
125- 150	25	9.1	8.1	6.4	5.3	4	3.4	2.6	1.9	1.1	0.9	0.5	0.5	0.5	0.5	0.5
150- 175	25	6.6	6.1	5	4.3	3.5	3.1	2.5	1.7	1.1	0.9	0.5	0.5	0.5	0.5	0.5
175-200	25	5.1	4.8	3.9	3.6	3.2	2.6	2.3	1.5	1.1	0.9	0.5	0.5	0.5	0.5	0.5
200-225	25	4.1	3.7	3.4	3	2.6	2.4	2	1.2	1	0.8	0.5	0.5	0.5	0.5	0.5

Equivalent dose rate in the ID access scenario for T= 100 d, t=100d– Lar EC, VA, Pixel, and VI removed

Table A1.4 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	43.7	41	37	33.8	29	21.7	17.5	12.1	8.2	6.4	3.5	3.2	2.7	2.6	1.5
5- 10	5	43.7	41.3	37.2	33.8	29	21.7	17.5	12.1	8.2	6.4	3.5	3	2.7	2.6	1.5
10- 20	10	44.7	42.4	38	34	28.8	21.7	17.4	12.1	8.4	6.4	3.5	3	2.7	2.6	1.5
20- 30	10	47.2	45.4	39.6	34.3	28.8	22.1	17.1	12.1	8.7	6.4	3.5	3	2.7	2.6	1.5
30- 45	15	67	64.6	43.6	35	28.2	22.5	16.7	12.1	8.8	6.3	3.4	2.9	2.7	2.5	1.4
45- 60	15	81.8	78.7	46	35	27.8	22.8	16.3	12.2	8.9	6.4	3.4	2.8	2.7	2.5	1.1
60- 75	15	67.2	65	44.3	34.2	27.6	22	16.2	11.7	9	6.5	3.4	2.8	2.7	2.5	1.1
75-95	20	58	56	41.2	33.1	26.4	21.1	16.1	11.4	8.8	6.3	3.4	2.8	2.7	2.5	1.1
95-115	20	61.1	56.4	40.3	31.3	24.8	20.1	15.1	11	8.3	6.3	3.4	2.7	2.7	2.5	1.1
115- 125	10	60.3	55.6	38.6	29.5	23.8	18.8	14.6	10.4	8	6.2	3.2	2.7	2.5	2.5	1.1
125- 150	25	46.2	42.5	33.2	27.1	21.9	17.7	13.9	9.8	7.8	6.2	2.9	2.7	2.5	2.5	1
150- 175	25	35	32.2	27.1	23	19.2	16.1	12.7	9.8	7.4	6.1	2.8	2.6	2.5	2.5	1
175-200	25	26.8	24.8	22.4	19.9	17	14.3	11.8	9	6.8	5.6	2.7	2.5	2.5	2.4	1
200-225	25	21.9	20	18.1	16.8	14.3	12.3	10	8.1	6.5	4.9	2.6	2.5	2.4	1.9	1

Equivalent dose rate in the ID access scenario for T= 10y, t= 5 d– Lar EC, VA, Pixel, and VI removed

Table A1.4 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	23.2	22.6	20.9	18.7	15.6	12.3	9.4	6.7	4.5	3.6	1.4	1.4	1.3	1.3	0.9
5- 10	5	23.6	22.6	21	18.9	15.6	12.3	9.4	6.7	4.6	3.6	1.4	1.4	1.3	1.3	0.9
10- 20	10	24.1	23.4	21.5	18.9	15.5	12.3	9.4	6.7	4.6	3.6	1.4	1.4	1.3	1.3	0.9
20- 30	10	25.6	25	22.5	19.1	15.5	12.4	9.3	6.7	4.7	3.6	1.4	1.4	1.3	1.3	0.9
30- 45	15	37.4	36.5	24.6	19.3	15.5	12.5	9.2	6.7	4.8	3.6	1.4	1.4	1.3	1.3	0.9
45- 60	15	46.9	45.5	25.8	19.4	15.4	12.5	9.1	6.6	4.8	3.6	1.4	1.3	1.3	1.3	0.9
60- 75	15	38.5	37.7	24.9	19	15.3	12.2	9.2	6.6	4.9	3.6	1.4	1.3	1.3	1.2	0.9
75- 95	20	33	32.2	23.1	18.4	14.7	11.6	8.8	6.3	4.8	3.5	1.4	1.3	1.3	1.2	0.9
95- 115	20	33.8	31.4	22.6	17.4	13.8	11	8.2	6.2	4.7	3.1	1.4	1.3	1.3	1.2	0.9
115- 125	10	33.5	30.5	21.2	16.6	13	10.2	8.1	5.7	4.5	3.1	1.4	1.3	1.2	1.2	0.9
125- 150	25	25.8	23.9	18.4	14.8	12	9.5	7.7	5.4	4.4	3	1.3	1.3	1.2	1.2	0.8
150- 175	25	19.1	17.9	14.8	12.8	10.8	9	7.2	5.4	4.4	2.9	1.3	1.2	1.2	1.1	0.6
175- 200	25	15	14	12.3	10.9	9.5	7.9	6.7	5	3.8	2.7	1.3	1.2	1.1	1.1	0.6
200-225	25	12.7	11.6	10.4	9.4	8.1	7.1	5.6	4.6	3.3	2.5	1.2	1.1	1.1	1.1	0.5

Equivalent dose rate in the ID access scenario for T= 10y, t= 100 d– Lar EC, VA, Pixel, and VI removed

Addendum 2



Fig. A2.1 Sketch of the VA Beam pipe section.

Table A2.1

Equivalent dose rate induced by high-energy hadrons from steel LAI beam Pipe for 1 – 1000, t-50														
R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	357.8	3406.9											2540.6	414.8
5	342.6	3305.9	2502.6	2566.8	2100.6	2669.3	4926.9	3712.1	2852.9	2533.3	2513.5	1764.9	2432.2	380.1
7	329.6	1589.9	1808.1	1804.0	1406.1	1753.6	3111.5	2395.1	1848.8	1645.4	1615.9	1230.7	1144.1	352.8
10	306.1	939.4	1185.2	1223.6	960.4	1196.1	2024.4	1600.2	1240.4	1105.1	1070.6	842.0	657.9	309.2
15	264.6	564.3	677.4	749.7	641.2	793.4	1258.5	1033.1	805.8	718.3	682.8	538.9	392.5	246.4
20	227.2	396.9	454.4	517.8	485.3	595.3	895.8	759.4	595.9	531.2	496.8	388.0	281.7	201.3
25	196.5	302.8	336.8	387.6	390.5	475.6	685.3	597.2	471.3	420.1	387.5	299.1	220.5	169.3
50	111.8	136.1	143.8	163.4	190.9	228.4	288.7	275.6	223.5	199.0	175.1	132.6	107.2	93.9
75	77.3	88.1	91.7	102.1	120.7	142.1	169.3	169.1	140.7	125.2	108.0	83.3	71.1	64.9
100	58.8	65.1	67.2	73.5	85.6	98.8	114.1	116.7	99.4	88.6	76.1	60.1	53.0	49.4
125	47.2	51.3	52.6	56.8	64.8	73.5	83.2	86.1	74.8	66.9	57.7	46.7	42.0	39.7
150	39.2	42.0	42.9	45.7	51.3	57.2	63.7	66.4	58.6	52.7	45.8	37.9	34.6	33.0
175	33.2	35.2	35.9	37.9	41.9	46.0	50.7	52.8	47.3	42.9	37.6	31.6	29.2	28.0
200	28.7	30.1	30.6	32.1	35.0	38.0	41.4	43.1	39.1	35.6	31.5	27.0	25.1	24.2
225	25.0	26.1	26.5	27.6	29.8	32.0	34.5	35.9	32.8	30.1	26.9	23.4	21.9	21.2

Equivalent dose rate induced by high-energy hadrons from steel LAr Beam Pipe for T= 100d, t=5d

Table A2.1 (continuation)

					<u> </u>				••••			,.		
R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	402.0	3824.9											2858.0	466.6
5	384.9	3711.8	2810.0	2879.9	2364.8	3008.9	5571.7	4182.9	3209.7	2850.7	2827.7	1984.6	2735.9	427.6
7	370.3	1785.3	2030.4	2024.6	1582.7	1976.9	3518.2	2698.8	2080.0	1851.5	1817.9	1384.0	1287.0	396.9
10	344.0	1055.0	1331.1	1373.6	1080.8	1348.6	2288.8	1803.1	1395.5	1243.5	1204.5	946.9	740.0	347.8
15	297.3	633.9	760.9	841.9	721.6	894.6	1422.5	1164.1	906.6	808.4	768.1	606.1	441.5	277.2
20	255.4	445.9	510.5	581.7	546.2	671.3	1012.3	855.8	670.4	597.8	559.0	436.4	316.8	226.4
25	220.8	340.3	378.5	435.6	439.6	536.4	774.3	673.0	530.3	472.8	436.0	336.5	248.0	190.4
50	125.8	153.1	161.8	183.9	215.0	257.6	326.0	310.6	251.5	223.9	197.1	149.2	120.6	105.7
75	87.0	99.2	103.3	114.9	136.0	160.2	191.1	190.6	158.4	140.9	121.6	93.7	80.0	73.1
100	66.2	73.3	75.7	82.8	96.4	111.4	128.7	131.5	111.9	99.7	85.6	67.7	59.6	55.6
125	53.2	57.8	59.3	64.0	73.0	82.9	93.8	97.0	84.2	75.3	64.9	52.5	47.3	44.7
150	44.1	47.3	48.3	51.5	57.8	64.5	71.9	74.8	66.0	59.4	51.6	42.6	38.9	37.1
175	37.4	39.7	40.4	42.7	47.2	51.9	57.1	59.5	53.3	48.3	42.3	35.6	32.9	31.5
200	32.3	33.9	34.5	36.2	39.4	42.8	46.6	48.6	44.0	40.1	35.5	30.4	28.3	27.3
225	28.2	29.5	29.9	31.1	33.5	36.1	38.9	40.4	37.0	33.9	30.3	26.3	24.7	23.9

Equivalent dose rate induced by high-energy hadrons from steel LAr Beam Pipe for T= 10y, t=5d
R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	60.8	568.8											440.7	72.1
5	58.2	552.1	421.6	436.7	359.9	466.2	901.6	666.9	504.4	443.1	438.4	306.8	421.6	66.1
7	56.0	267.0	305.5	307.2	241.3	306.9	568.8	430.2	326.8	287.9	281.9	214.0	198.5	61.3
10	52.1	158.6	200.9	208.6	165.1	209.9	369.6	287.4	219.3	193.5	186.8	146.5	114.2	53.8
15	45.2	95.9	115.2	128.1	110.6	139.6	229.4	185.5	142.4	125.9	119.2	93.8	68.3	42.9
20	38.9	67.7	77.5	88.7	84.0	105.0	163.0	136.4	105.3	93.2	86.8	67.6	49.0	35.1
25	33.7	51.8	57.7	66.5	67.7	84.1	124.5	107.3	83.3	73.7	67.7	52.2	38.4	29.5
50	19.4	23.6	24.9	28.4	33.4	40.6	52.1	49.5	39.6	35.0	30.7	23.2	18.8	16.4
75	13.5	15.4	16.0	17.9	21.3	25.3	30.4	30.3	24.9	22.1	19.0	14.6	12.5	11.4
100	10.3	11.4	11.8	12.9	15.1	17.6	20.5	20.9	17.6	15.7	13.4	10.6	9.3	8.7
125	8.3	9.1	9.3	10.0	11.5	13.1	14.9	15.4	13.3	11.8	10.2	8.2	7.4	7.0
150	6.9	7.4	7.6	8.1	9.1	10.2	11.4	11.9	10.4	9.3	8.1	6.7	6.1	5.8
175	5.9	6.2	6.4	6.7	7.4	8.2	9.0	9.4	8.4	7.6	6.6	5.6	5.2	5.0
200	5.1	5.3	5.4	5.7	6.2	6.8	7.4	7.7	6.9	6.3	5.6	4.8	4.4	4.3
225	4.4	4.6	4.7	4.9	5.3	5.7	6.2	6.4	5.8	5.3	4.8	4.1	3.9	3.8

Table A2.1 (continuation) Equivalent dose rate induced by high-energy hadrons from steel LAr Beam Pipe for T= 100d, t=100d

Table A2.1 (continuation)

					-)	07			-			- j , -		
R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	91.8	862.4											664.8	108.6
5	87.9	837.2	637.5	657.2	543.3	705.1	1350.6	995.2	755.4	666.1	660.2	462.0	636.0	99.6
7	84.6	404.2	461.6	462.5	364.1	463.8	852.0	641.9	489.4	432.8	424.4	322.2	299.3	92.4
10	78.7	239.9	303.4	314.2	249.1	316.9	553.8	428.8	328.3	290.8	281.3	220.5	172.2	81.0
15	68.1	144.7	173.9	193.0	166.8	210.6	343.7	276.9	213.3	189.2	179.4	141.2	102.8	64.6
20	58.7	102.1	117.0	133.6	126.5	158.3	244.2	203.6	157.7	140.0	130.6	101.7	73.8	52.8
25	50.8	78.2	86.9	100.2	102.1	126.6	186.6	160.1	124.8	110.8	101.9	78.5	57.8	44.4
50	29.2	35.5	37.5	42.8	50.3	61.0	78.1	73.9	59.2	52.6	46.1	34.9	28.2	24.7
75	20.3	23.2	24.1	26.9	32.0	38.0	45.6	45.3	37.3	33.1	28.5	22.0	18.7	17.1
100	15.5	17.2	17.8	19.5	22.7	26.4	30.7	31.3	26.4	23.5	20.1	15.9	14.0	13.1
125	12.5	13.6	14.0	15.1	17.3	19.6	22.3	23.0	19.9	17.7	15.3	12.3	11.1	10.5
150	10.4	11.1	11.4	12.2	13.7	15.3	17.1	17.8	15.6	14.0	12.1	10.0	9.2	8.7
175	8.8	9.4	9.5	10.1	11.2	12.3	13.6	14.1	12.6	11.4	10.0	8.4	7.7	7.4
200	7.6	8.0	8.2	8.5	9.3	10.1	11.1	11.5	10.4	9.5	8.4	7.2	6.7	6.4
225	6.7	7.0	7.1	7.4	7.9	8.5	9.2	9.6	8.7	8.0	7.2	6.2	5.8	5.6

Equivalent dose rate induced by high-energy hadrons from steel LAr Beam Pipe for T= 10y, t=100d

Table A2.2

	ĽЧu	valentu		induced	Dy 1000-	епегуу п	leutions			eannip		' 100u, t	-Ju	
R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	10.1	75.8											50.1	8.3
5	9.8	76.8	66.0	62.0	39.2	83.4	322.4	148.9	61.3	55.1	51.5	30.4	52.6	7.7
7	9.4	40.1	52.2	46.1	28.5	57.5	200.0	94.8	40.0	35.6	33.0	21.7	23.1	7.1
10	8.9	25.8	36.1	33.0	21.5	41.6	128.0	63.0	27.3	24.1	22.0	15.3	12.9	6.2
15	7.9	16.5	20.6	21.0	16.2	29.7	77.6	40.7	18.3	15.9	14.2	10.2	7.7	5.0
20	6.9	11.9	13.8	14.8	13.4	23.4	53.8	30.0	13.9	11.9	10.5	7.6	5.6	4.1
25	6.1	9.2	10.3	11.4	11.6	19.3	40.2	23.7	11.3	9.6	8.3	6.0	4.5	3.5
50	3.8	4.5	4.8	5.5	6.9	9.9	15.2	11.1	6.0	4.9	4.0	2.9	2.4	2.1
75	2.8	3.2	3.3	3.7	4.7	6.2	8.3	6.8	4.1	3.3	2.7	2.0	1.7	1.6
100	2.2	2.5	2.6	2.8	3.5	4.3	5.3	4.7	3.0	2.5	2.0	1.5	1.4	1.3
125	1.8	2.0	2.1	2.2	2.7	3.1	3.7	3.4	2.4	2.0	1.6	1.3	1.1	1.1
150	1.5	1.7	1.7	1.8	2.1	2.4	2.7	2.6	1.9	1.6	1.3	1.1	1.0	0.9
175	1.3	1.4	1.4	1.5	1.7	1.9	2.1	2.0	1.6	1.3	1.1	0.9	0.9	0.8
200	1.1	1.2	1.2	1.3	1.4	1.6	1.7	1.7	1.3	1.1	1.0	0.8	0.8	0.7
225	1.0	1.0	1.1	1.1	1.2	1.3	1.4	1.4	1.1	1.0	0.9	0.7	0.7	0.7

Equivalent dose rate induced by low-energy neutrons from steel LAr Beam Pipe for T= 100d, t=5d

Table A2.2 (continuation)

R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	20.5	147.1											67.0	11.2
5	19.8	149.7	144.8	133.4	89.4	143.6	425.4	187.9	81.7	73.4	68.5	40.7	70.5	10.2
7	19.1	82.4	117.8	101.9	62.2	96.6	263.9	120.0	53.2	47.5	43.9	29.1	31.0	9.5
10	18.0	55.1	82.3	73.8	44.6	68.2	168.9	80.0	36.3	32.1	29.3	20.5	17.3	8.3
15	15.8	35.4	45.8	46.1	31.8	47.2	102.5	51.8	24.3	21.1	19.0	13.6	10.3	6.7
20	13.7	25.0	29.5	31.5	25.3	36.4	71.3	38.3	18.5	15.9	14.0	10.1	7.5	5.5
25	11.9	18.9	21.3	23.3	21.1	29.6	53.4	30.4	15.0	12.7	11.1	8.0	6.0	4.7
50	6.8	8.2	8.7	9.8	11.4	14.7	20.5	14.4	7.9	6.5	5.4	3.9	3.2	2.9
75	4.6	5.3	5.5	6.2	7.4	9.1	11.3	8.9	5.4	4.4	3.6	2.7	2.3	2.1
100	3.5	3.9	4.0	4.4	5.2	6.2	7.3	6.2	4.0	3.3	2.7	2.1	1.8	1.7
125	2.8	3.1	3.2	3.4	3.9	4.5	5.1	4.5	3.2	2.6	2.1	1.7	1.5	1.4
150	2.3	2.5	2.6	2.7	3.1	3.5	3.8	3.5	2.6	2.2	1.8	1.4	1.3	1.3
175	2.0	2.1	2.1	2.2	2.5	2.7	3.0	2.8	2.1	1.8	1.5	1.3	1.2	1.1
200	1.7	1.8	1.8	1.9	2.0	2.2	2.4	2.3	1.8	1.5	1.3	1.1	1.0	1.0
225	1.4	1.5	1.5	1.6	1.7	1.8	1.9	1.9	1.5	1.3	1.2	1.0	0.9	0.9

Equivalent dose rate induced by low-energy neutrons from steel LAr Beam Pipe for T= 10y, t=5d

R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	4.8	35.8											22.0	3.7
5	4.7	36.3	32.1	30.0	19.3	38.4	140.3	64.3	26.8	24.1	22.6	13.3	23.1	3.4
7	4.5	19.2	25.6	22.5	13.8	26.3	87.0	41.0	17.5	15.6	14.4	9.5	10.1	3.1
10	4.2	12.5	17.7	16.1	10.3	18.9	55.7	27.3	11.9	10.5	9.6	6.7	5.7	2.7
15	3.7	8.0	10.1	10.2	7.7	13.4	33.8	17.6	8.0	7.0	6.2	4.5	3.4	2.2
20	3.3	5.7	6.7	7.2	6.3	10.5	23.4	13.0	6.1	5.2	4.6	3.3	2.5	1.8
25	2.9	4.4	4.9	5.4	5.4	8.7	17.5	10.3	4.9	4.2	3.6	2.6	2.0	1.5
50	1.7	2.1	2.2	2.5	3.1	4.4	6.7	4.8	2.6	2.1	1.8	1.3	1.1	0.9
75	1.3	1.5	1.5	1.7	2.1	2.8	3.6	3.0	1.8	1.4	1.2	0.9	0.8	0.7
100	1.0	1.1	1.2	1.3	1.5	1.9	2.3	2.0	1.3	1.1	0.9	0.7	0.6	0.6
125	0.8	0.9	0.9	1.0	1.2	1.4	1.6	1.5	1.0	0.9	0.7	0.6	0.5	0.5
150	0.7	0.7	0.8	0.8	0.9	1.1	1.2	1.1	0.8	0.7	0.6	0.5	0.4	0.4
175	0.6	0.6	0.6	0.7	0.8	0.8	0.9	0.9	0.7	0.6	0.5	0.4	0.4	0.4
200	0.5	0.5	0.5	0.6	0.6	0.7	0.8	0.7	0.6	0.5	0.4	0.4	0.3	0.3
225	0.4	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.5	0.4	0.4	0.3	0.3	0.3

Table A2.2 (continuation) Equivalent dose rate induced by low-energy neutrons from steel LAr Beam Pipe for T= 100d, t=100d

R/Z, cm	350	365	370	385	415	450	500	600	700	750	800	850	870	880
0	14.1	99.2											33.9	5.7
5	13.6	101.2	103.8	94.8	65.2	90.1	212.3	89.2	41.3	37.1	34.6	20.6	35.8	5.2
7	13.2	57.3	85.5	73.3	44.5	59.6	131.7	57.1	26.9	24.0	22.2	14.8	15.7	4.8
10	12.4	39.0	60.0	53.3	31.2	41.3	84.3	38.2	18.3	16.2	14.8	10.4	8.8	4.2
15	10.8	25.1	33.0	33.0	21.6	27.9	51.3	24.8	12.3	10.7	9.6	6.9	5.2	3.4
20	9.4	17.6	21.0	22.2	16.8	21.2	35.8	18.4	9.3	8.0	7.1	5.1	3.8	2.8
25	8.1	13.1	14.9	16.2	13.7	17.1	26.8	14.7	7.6	6.4	5.6	4.1	3.0	2.4
50	4.4	5.3	5.6	6.3	6.9	8.2	10.5	7.1	4.0	3.3	2.7	2.0	1.6	1.5
75	2.9	3.3	3.4	3.7	4.3	5.0	5.8	4.4	2.7	2.2	1.8	1.4	1.2	1.1
100	2.1	2.3	2.4	2.6	3.0	3.4	3.8	3.1	2.0	1.7	1.4	1.1	0.9	0.9
125	1.6	1.8	1.8	2.0	2.2	2.5	2.7	2.3	1.6	1.3	1.1	0.9	0.8	0.7
150	1.3	1.4	1.4	1.5	1.7	1.9	2.0	1.8	1.3	1.1	0.9	0.7	0.7	0.6
175	1.1	1.2	1.2	1.2	1.4	1.5	1.6	1.4	1.1	0.9	0.8	0.6	0.6	0.6
200	0.9	1.0	1.0	1.0	1.1	1.2	1.3	1.2	0.9	0.8	0.7	0.6	0.5	0.5
225	0.8	0.8	0.8	0.9	0.9	1.0	1.0	1.0	0.8	0.7	0.6	0.5	0.5	0.5

Table A2.2 (continuation) Equivalent dose rate induced by low-energy neutrons from steel LAr Beam Pipe for T= 10y, t=100d

Addendum 3



Fig. A3.1 Sketch of the Pixel Detector with VI beam pipe section.

Table A3.1

R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											67.50	7.94	3.22	1.74	1.15
10										42.02	18.75	6.98	3.13	1.73	1.15
23	35.51	24.38	14.67	6.66	5.54	5.55	8.25	18.46	29.70	20.86	8.58	5.13	2.83	1.65	1.12
30	25.72	17.59	10.33	5.23	4.19	4.17	6.30	11.85	17.99	14.78	6.76	4.39	2.62	1.59	1.10
40	17.88	12.51	7.92	4.34	3.37	3.32	4.82	7.35	9.69	8.67	5.01	3.55	2.32	1.49	1.06
50	13.23	9.53	6.48	3.79	2.90	2.83	3.82	4.99	5.28	5.10	3.80	2.91	2.06	1.39	1.01
75	7.27	5.63	4.36	2.90	2.25	2.10	2.39	2.56	2.55	2.48	2.16	1.88	1.51	1.15	0.89
100	4.59	3.78	3.16	2.32	1.84	1.67	1.68	1.67	1.66	1.61	1.47	1.33	1.15	0.94	0.77
125	3.17	2.75	2.40	1.88	1.54	1.37	1.30	1.25	1.22	1.18	1.10	1.03	0.92	0.79	0.67
150	2.33	2.09	1.88	1.55	1.30	1.14	1.05	1.00	0.97	0.95	0.88	0.83	0.76	0.66	0.59
200	1.42	1.33	1.25	1.09	0.95	0.84	0.75	0.71	0.69	0.67	0.64	0.60	0.56	0.51	0.47
250	0.97	0.92	0.89	0.81	0.72	0.65	0.59	0.55	0.52	0.51	0.49	0.47	0.44	0.41	0.38

Equivalent dose rate from Pixel + VI for T= 100d, t= 5d

Table A3.1 (continuation)

Equivalent dose rate from Pixel + VI for T= 100d, t= 7 d

				- 1-											
R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											62.89	7.35	2.97	1.60	1.06
10										38.45	17.37	6.44	2.89	1.59	1.06
23	32.03	22.39	13.48	6.18	5.17	5.18	7.66	16.93	27.17	19.13	7.90	4.72	2.60	1.52	1.03
30	23.25	16.12	9.46	4.85	3.88	3.88	5.83	10.87	16.43	13.54	6.22	4.04	2.42	1.47	1.02
40	16.20	11.46	7.26	4.01	3.12	3.08	4.45	6.74	8.86	7.96	4.59	3.27	2.13	1.38	0.98
50	12.00	8.70	5.95	3.48	2.69	2.62	3.52	4.57	4.86	4.68	3.49	2.67	1.89	1.28	0.93
75	6.61	5.14	3.99	2.67	2.06	1.94	2.19	2.35	2.34	2.28	2.00	1.73	1.38	1.06	0.82
100	4.18	3.46	2.89	2.11	1.70	1.54	1.56	1.55	1.53	1.48	1.35	1.23	1.06	0.87	0.70
125	2.89	2.50	2.19	1.72	1.41	1.25	1.20	1.14	1.12	1.09	1.01	0.94	0.84	0.72	0.62
150	2.12	1.90	1.72	1.41	1.20	1.06	0.96	0.91	0.89	0.87	0.82	0.77	0.69	0.61	0.54
200	1.30	1.22	1.14	1.01	0.88	0.77	0.69	0.65	0.64	0.62	0.58	0.56	0.51	0.47	0.42
250	0.87	0.84	0.80	0.74	0.66	0.59	0.53	0.49	0.48	0.47	0.45	0.43	0.41	0.38	0.35

Table A3.1 (continuation)

R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											56.77	6.33	2.50	1.34	0.88
10										31.23	15.18	5.52	2.43	1.34	0.88
23	24.95	18.37	10.98	5.34	4.54	4.57	6.56	13.99	22.21	15.69	6.64	3.99	2.18	1.27	0.86
30	18.20	13.11	7.71	4.13	3.37	3.37	4.94	8.98	13.38	11.12	5.21	3.40	2.02	1.23	0.83
40	12.75	9.27	5.91	3.36	2.67	2.64	3.74	5.59	7.26	6.55	3.82	2.73	1.79	1.16	0.80
50	9.50	7.02	4.84	2.90	2.28	2.23	2.96	3.80	4.02	3.88	2.90	2.22	1.58	1.07	0.77
75	5.26	4.14	3.24	2.19	1.73	1.63	1.84	1.96	1.96	1.90	1.65	1.43	1.15	0.88	0.68
100	3.34	2.79	2.35	1.74	1.40	1.28	1.30	1.28	1.26	1.23	1.13	1.03	0.88	0.72	0.59
125	2.32	2.02	1.77	1.41	1.17	1.04	0.99	0.95	0.93	0.91	0.85	0.78	0.69	0.60	0.51
150	1.72	1.54	1.40	1.17	0.98	0.87	0.80	0.77	0.74	0.72	0.68	0.63	0.57	0.50	0.45
200	1.05	0.97	0.92	0.81	0.72	0.64	0.58	0.54	0.52	0.50	0.48	0.46	0.43	0.39	0.35
250	0.71	0.68	0.66	0.60	0.54	0.49	0.43	0.41	0.40	0.39	0.37	0.36	0.33	0.31	0.29

Equivalent dose rate from Pixel + VI for T= 100d, t= 15d

Table A3.1 (continuation)

Equivalent dose rate from Pixel + VI for T= 100d, t= 30 d

						000 140				000, 1	<u> </u>				
R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											52.04	5.47	2.11	1.12	0.73
10										24.91	13.35	4.73	2.05	1.11	0.72
23	19.25	14.91	8.79	4.56	3.96	3.98	5.59	11.47	18.01	12.69	5.57	3.36	1.82	1.05	0.70
30	14.10	10.53	6.19	3.46	2.90	2.90	4.15	7.35	10.78	9.00	4.32	2.84	1.69	1.01	0.69
40	9.93	7.40	4.76	2.79	2.26	2.25	3.13	4.59	5.89	5.33	3.17	2.27	1.48	0.95	0.67
50	7.41	5.60	3.89	2.40	1.92	1.88	2.46	3.13	3.31	3.19	2.40	1.84	1.31	0.88	0.64
75	4.15	3.29	2.60	1.79	1.44	1.36	1.52	1.62	1.60	1.55	1.37	1.19	0.96	0.72	0.56
100	2.64	2.22	1.88	1.41	1.15	1.06	1.06	1.06	1.04	1.01	0.93	0.84	0.72	0.59	0.49
125	1.84	1.61	1.43	1.14	0.95	0.86	0.82	0.79	0.77	0.75	0.70	0.64	0.57	0.49	0.42
150	1.36	1.23	1.12	0.93	0.80	0.71	0.65	0.63	0.62	0.59	0.55	0.52	0.47	0.42	0.37
200	0.85	0.79	0.75	0.66	0.58	0.52	0.47	0.44	0.43	0.42	0.40	0.37	0.35	0.32	0.29
250	0.57	0.55	0.53	0.48	0.45	0.41	0.35	0.33	0.32	0.32	0.30	0.29	0.28	0.26	0.24

Table A3.1 (continuation)

R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											45.49	4.17	1.48	0.76	0.49
10										15.20	10.65	3.52	1.43	0.76	0.49
23	11.07	9.29	5.24	3.20	2.88	2.92	3.96	7.65	11.65	8.02	3.92	2.38	1.27	0.72	0.48
30	8.14	6.43	3.73	2.34	2.03	2.07	2.85	4.83	6.81	5.69	2.96	1.97	1.16	0.68	0.46
40	5.76	4.48	2.89	1.83	1.55	1.56	2.12	3.02	3.77	3.42	2.13	1.55	1.01	0.64	0.45
50	4.32	3.38	2.37	1.54	1.29	1.29	1.66	2.06	2.18	2.10	1.60	1.25	0.88	0.60	0.43
75	2.44	1.99	1.58	1.14	0.94	0.91	1.01	1.07	1.06	1.04	0.91	0.79	0.63	0.48	0.38
100	1.58	1.34	1.15	0.88	0.74	0.69	0.71	0.70	0.70	0.67	0.61	0.55	0.48	0.39	0.32
125	1.11	0.97	0.87	0.71	0.61	0.56	0.54	0.51	0.50	0.48	0.45	0.42	0.37	0.33	0.28
150	0.81	0.74	0.69	0.59	0.51	0.46	0.43	0.40	0.39	0.38	0.36	0.34	0.31	0.27	0.24
200	0.51	0.47	0.46	0.41	0.37	0.34	0.30	0.28	0.27	0.27	0.25	0.24	0.23	0.21	0.19
250	0.35	0.34	0.33	0.30	0.28	0.25	0.22	0.21	0.21	0.20	0.19	0.19	0.18	0.17	0.16

Equivalent dose rate from Pixel + VI for T= 100d, t= 100 d

Table A3.2

R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											235.32	21.40	7.55	3.86	2.48
10											54.75	18.05	7.29	3.82	2.47
23	53.97	44.32	25.35	15.80	14.36	14.63	19.99	39.23	59.71	40.48	19.95	12.14	6.43	3.62	2.40
30	39.47	30.69	17.97	11.45	10.11	10.30	14.42	24.68	34.68	28.62	15.06	10.01	5.89	3.47	2.35
40	27.84	21.38	13.90	8.96	7.68	7.80	10.68	15.32	19.09	17.19	10.80	7.85	5.13	3.25	2.26
50	20.87	16.13	11.39	7.55	6.36	6.40	8.34	10.46	10.97	10.58	8.10	6.30	4.46	2.99	2.14
75	11.76	9.51	7.63	5.51	4.62	4.50	5.09	5.38	5.36	5.20	4.58	3.98	3.21	2.42	1.86
100	7.58	6.44	5.53	4.30	3.65	3.45	3.53	3.50	3.44	3.35	3.06	2.79	2.41	1.96	1.60
125	5.31	4.71	4.21	3.46	2.98	2.76	2.66	2.57	2.51	2.45	2.26	2.11	1.90	1.62	1.37
150	3.96	3.61	3.33	2.84	2.49	2.28	2.11	2.02	1.98	1.92	1.80	1.70	1.54	1.36	1.19
200	2.48	2.34	2.22	2.00	1.80	1.63	1.47	1.41	1.37	1.34	1.25	1.20	1.12	1.03	0.92
250	1.71	1.65	1.59	1.47	1.35	1.23	1.13	1.06	1.04	1.01	0.96	0.92	0.88	0.81	0.75

Equivalent dose rate from Pixel + VI for T= 10 y, t= 5d

Table A3.2 (continuation)

Equivalent dose rate from Pixel + VI for T=	10 v	t= 7 d

										·•), •					
R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											229.39	20.72	7.29	3.71	2.38
10										73.82	53.16	17.47	7.04	3.66	2.36
23	50.42	42.28	24.11	15.32	13.97	14.23	19.35	37.64	57.09	38.68	19.23	11.70	6.20	3.48	2.30
30	36.96	29.17	17.10	11.05	9.81	10.00	13.91	23.66	33.07	27.35	14.47	9.63	5.66	3.34	2.25
40	26.12	20.29	13.23	8.62	7.42	7.54	10.30	14.69	18.23	16.44	10.37	7.55	4.94	3.12	2.16
50	19.61	15.28	10.83	7.23	6.14	6.19	8.03	10.03	10.53	10.14	7.78	6.06	4.29	2.88	2.06
75	11.10	9.01	7.26	5.27	4.44	4.33	4.88	5.17	5.14	5.00	4.40	3.82	3.07	2.32	1.78
100	7.15	6.11	5.26	4.10	3.49	3.31	3.38	3.36	3.31	3.21	2.94	2.67	2.31	1.88	1.53
125	5.04	4.46	4.01	3.30	2.86	2.64	2.55	2.47	2.42	2.35	2.18	2.03	1.82	1.55	1.32
150	3.75	3.43	3.15	2.70	2.37	2.17	2.03	1.94	1.89	1.84	1.73	1.63	1.48	1.31	1.15
200	2.35	2.23	2.11	1.91	1.71	1.56	1.42	1.34	1.31	1.27	1.20	1.15	1.08	0.98	0.88
250	1.62	1.57	1.52	1.40	1.29	1.17	1.06	1.01	0.98	0.96	0.92	0.89	0.83	0.77	0.72

Table A3.2 (continuation)

Equivalent dose rate from $Pixei + vi \text{ for } i = 10$	U V. t= 150	1
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										· • J , •					
R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											225.46	19.79	6.83	3.45	2.19
10										66.45	51.30	16.61	6.58	3.41	2.19
23	43.06	38.04	21.50	14.39	13.28	13.56	18.19	34.55	51.92	35.12	18.00	10.98	5.77	3.24	2.13
30	31.69	26.00	15.25	10.26	9.24	9.45	12.97	21.68	29.88	24.84	13.45	9.00	5.27	3.10	2.08
40	22.53	17.98	11.80	7.93	6.93	7.08	9.55	13.49	16.57	15.00	9.60	7.01	4.58	2.89	1.99
50	16.99	13.52	9.67	6.62	5.71	5.77	7.44	9.22	9.67	9.30	7.18	5.61	3.97	2.67	1.90
75	9.68	7.97	6.46	4.77	4.08	4.01	4.51	4.76	4.73	4.60	4.05	3.53	2.83	2.13	1.65
100	6.29	5.40	4.68	3.70	3.19	3.05	3.11	3.09	3.04	2.96	2.70	2.46	2.13	1.73	1.41
125	4.44	3.96	3.57	2.97	2.59	2.42	2.33	2.26	2.22	2.15	2.00	1.87	1.66	1.42	1.21
150	3.32	3.04	2.81	2.44	2.15	1.98	1.86	1.77	1.72	1.69	1.58	1.49	1.35	1.20	1.05
200	2.09	1.97	1.89	1.71	1.54	1.41	1.28	1.23	1.19	1.16	1.10	1.05	0.99	0.89	0.81
250	1.44	1.40	1.35	1.27	1.16	1.07	0.96	0.92	0.90	0.88	0.84	0.80	0.76	0.70	0.66

Table A3.2 (continuation)

Equivalent dose rate from Pixel + VI for T= 10 y, t= 30 d

						1000 140				10 J, t	00 0				
R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											217.27	18.68	6.34	3.19	2.02
10										59.43	48.80	15.61	6.12	3.14	2.01
23	36.87	34.17	19.07	13.48	12.56	12.85	17.03	31.70	47.18	31.75	16.72	10.21	5.36	2.98	1.96
30	27.24	23.15	13.56	9.51	8.66	8.89	12.06	19.83	26.98	22.46	12.41	8.34	4.88	2.86	1.91
40	19.45	15.92	10.52	7.28	6.46	6.61	8.83	12.34	15.03	13.62	8.83	6.47	4.22	2.66	1.83
50	14.72	11.96	8.61	6.04	5.27	5.37	6.85	8.45	8.84	8.51	6.59	5.16	3.66	2.45	1.75
75	8.46	7.04	5.76	4.32	3.74	3.70	4.15	4.36	4.35	4.22	3.72	3.23	2.60	1.96	1.51
100	5.51	4.78	4.17	3.33	2.91	2.78	2.86	2.84	2.79	2.71	2.48	2.26	1.94	1.58	1.29
125	3.91	3.50	3.17	2.67	2.35	2.21	2.14	2.07	2.02	1.96	1.83	1.70	1.52	1.30	1.10
150	2.93	2.70	2.50	2.19	1.95	1.80	1.70	1.62	1.58	1.54	1.43	1.36	1.24	1.10	0.95
200	1.85	1.76	1.68	1.53	1.39	1.28	1.18	1.11	1.08	1.06	1.00	0.96	0.90	0.81	0.73
250	1.29	1.25	1.21	1.13	1.04	0.96	0.87	0.84	0.82	0.79	0.76	0.72	0.69	0.64	0.59

Table A3.2 (continuation)

										,					
R/Z, cm	0	50	100	150	200	250	300	325	335	345	365	380	400	425	450
0											204.07	16.73	5.48	2.70	1.70
10										47.16	44.41	13.85	5.27	2.66	1.70
23	26.87	26.99	14.65	11.54	10.96	11.26	14.69	26.52	38.81	25.71	14.41	8.84	4.59	2.52	1.64
30	19.94	17.97	10.48	7.97	7.46	7.68	10.26	16.48	21.85	18.19	10.56	7.14	4.16	2.41	1.61
40	14.35	12.25	8.17	6.00	5.47	5.65	7.45	10.25	12.26	11.12	7.43	5.49	3.58	2.24	1.53
50	10.93	9.17	6.69	4.93	4.44	4.55	5.76	7.03	7.34	7.06	5.52	4.35	3.09	2.06	1.45
75	6.36	5.39	4.48	3.48	3.08	3.09	3.47	3.64	3.61	3.51	3.10	2.70	2.18	1.64	1.25
100	4.19	3.68	3.25	2.67	2.37	2.30	2.37	2.35	2.31	2.25	2.07	1.87	1.62	1.32	1.06
125	2.99	2.71	2.48	2.12	1.91	1.81	1.76	1.71	1.68	1.64	1.52	1.41	1.27	1.07	0.91
150	2.26	2.09	1.96	1.73	1.57	1.47	1.39	1.34	1.30	1.26	1.19	1.12	1.02	0.90	0.79
200	1.43	1.38	1.32	1.21	1.12	1.03	0.95	0.91	0.89	0.87	0.82	0.78	0.73	0.67	0.61
250	1.00	0.99	0.95	0.90	0.84	0.77	0.71	0.67	0.66	0.64	0.62	0.59	0.57	0.52	0.49

Equivalent dose rate from Pixel + VI for T= 10 y, t= 100 d

Addendum 4



Fig. A4.1. To calculations of dose rate from LAr End Cap.

Table A4.1

				Equiva	alent dos	se rate n	om lai	EC calor	imeterio	SI I = I0	υ a, ι= 5	a				
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	15.5	15.6	16.6	17.9	19.4	21.8	26.5	36.3	54.1	83.1	119.1	155.4	208.9	283.1	317.5
5- 10	5	14.6	14.7	15.5	16.7	18.2	20.6	25	34.4	51.5	78	109	143.1	181.9	232.8	253.6
10- 20	10	13.8	14.2	15	16	17.6	19.8	24.2	33.4	50.5	73.9	97.8	128.2	161.1	198	210.7
20- 30	10	13.1	13.4	14.2	15.1	16.5	18.6	22.8	31.4	47.6	67.2	88.5	113.2	137.3	163.6	173.2
30- 45	15	11.9	12.1	12.8	13.5	14.8	16.6	20.1	27.9	41.1	56.9	75.1	94.7	115.8	138.6	145.5
45- 60	15	10.5	10.7	11.2	12	13	14.6	17.9	24.7	35.8	50.5	64.2	79.2	93.4	109.1	113.1
60- 75	15	9.6	9.7	10.1	10.7	11.6	13.2	16.4	22.6	32.3	43.2	54.1	63.4	71.3	78.5	79.5
75- 95	20	8.5	8.6	9	9.5	10.4	12	15.1	20.2	27.6	36.7	42.2	46.9	49.9	50.7	49.9
95- 115	20	7.5	7.7	8.1	8.7	9.8	11.3	13.6	17.2	23.9	27.9	31.3	31.8	32.3	30.9	29.8
115- 125	10	7.1	7.3	7.8	8.4	9.4	10.5	12.3	15.7	20.6	22.7	24.8	23.3	23.6	21.5	20.3
125- 150	25	6.9	7	7.5	8	8.8	9.6	10.9	14.2	16.5	18.6	17.9	16.8	16.5	14.5	13.7
150- 175	25	6.6	6.7	7	7.3	7.8	8.3	9.6	11.4	12.3	12.8	11.3	10.5	10.1	8.3	8
175-200	25	6.1	6.2	6.3	6.5	6.8	7.1	7.9	9	9.2	8.6	6.9	6.5	5.9	4.5	4.1
200-225	25	5.5	5.5	5.5	5.5	5.4	5.7	6.8	7.1	6.7	5.7	4.2	4.2	3.1	2	1.8

Equivalent dose rate from LAr EC calorimeter for T= 100 d, t= 5 d

Table A4.1 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	3.1	3.3	3.5	3.7	4	4.7	5.9	8.4	13.3	20.7	30.5	43.8	61.1	85	94.6
5- 10	5	2.9	2.9	3.2	3.4	3.7	4.3	5.4	7.7	12.2	18.9	27.6	38.9	52.6	69.2	74.5
10- 20	10	2.8	2.8	3	3.3	3.6	4.2	5.2	7.4	11.4	17.3	24.1	33.1	44.8	59.4	64.5
20- 30	10	2.7	2.8	2.9	3.1	3.5	3.9	4.9	6.9	10.4	15	20.6	27.7	35.7	47.2	52.2
30- 45	15	2.5	2.5	2.7	2.9	3.1	3.6	4.4	5.9	8.7	12.3	16.5	21.4	27	33.7	35.9
45- 60	15	2.3	2.3	2.4	2.5	2.8	3.1	3.7	4.9	7.1	10.2	13.5	16.6	19.8	23.1	23.7
60- 75	15	2	2	2.1	2.2	2.4	2.6	3.1	4.2	6.3	8.8	10.8	12.8	14.5	15.8	15.8
75-95	20	1.7	1.7	1.7	1.8	2	2.1	2.6	3.8	5.5	7.1	8.4	9.2	10	10.2	9.9
95- 115	20	1.3	1.3	1.4	1.4	1.7	1.9	2.6	3.4	4.5	5.5	6.2	6.2	6.7	6.4	5.9
115- 125	10	1.2	1.2	1.3	1.4	1.7	2	2.5	3	3.9	4.6	4.9	4.7	5	4.4	4.2
125- 150	25	1.2	1.2	1.3	1.5	1.7	1.9	2.2	2.5	3.2	3.6	3.6	3.4	3.7	3.1	2.9
150- 175	25	1.3	1.3	1.4	1.5	1.6	1.6	1.7	2.1	2.4	2.6	2.3	2.3	2.4	1.8	1.7
175-200	25	1.3	1.3	1.3	1.2	1.2	1.2	1.4	1.8	1.8	1.8	1.4	1.6	1.5	1.1	0.9
200-225	25	1	0.9	0.9	0.9	0.9	1	1.4	1.4	1.4	1.2	0.9	1.2	0.9	0.5	0.4

Equivalent dose rate from LAr EC calorimeter for T= 100 d, t= 100 d

Table A4.1 (continuation)

							-				, ,	-				
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0- 5	5	22.9	23.6	24.9	26.6	29.2	32.8	40	55.8	84.5	128.5	186.4	251.1	339.4	458.4	506.6
5- 10	5	21.7	22.1	23.3	24.9	27.4	30.8	37.8	52.9	80.3	121.7	173.4	234.4	305.8	391.1	418.7
10- 20	10	20.7	21.1	22.4	23.9	26.3	29.6	36.3	50.8	77.6	115.3	158	212.8	275.5	351.4	375.8
20- 30	10	19.5	19.9	21.1	22.6	24.7	27.9	34.1	47.6	73	105.5	143	188.4	238.4	303.9	329.8
30- 45	15	17.8	18.1	19.1	20.4	22.3	25	30.6	42.8	64.3	91.4	122.4	158.6	198.7	245.3	257.8
45- 60	15	16.1	16.3	17.1	18.1	19.8	22.3	27.4	38.3	56.5	80.5	104.6	130.1	156.2	183.4	192.3
60- 75	15	14.4	14.8	15.5	16.4	17.8	20.1	25.1	35	51	69.9	87.6	103.5	117.3	129.7	129.7
75- 95	20	12.9	13.1	13.7	14.5	15.9	18.2	23.2	31.5	44.3	58.5	68.7	76.3	82.4	84.6	82.8
95- 115	20	11.3	11.4	12.2	13.1	14.8	17.2	21.1	27.4	37.8	45.6	51	52.4	54.6	52.2	50
115- 125	10	10.6	10.8	11.7	12.8	14.4	16.4	19.5	24.9	32.7	37.3	40.4	39	40.5	36.7	34.7
125- 150	25	10.4	10.6	11.5	12.5	13.7	15.3	17.5	22.1	26.7	30.3	29.7	28.4	29	25.3	23.8
150- 175	25	10.4	10.6	11.1	11.7	12.4	13.2	14.7	18.2	20.1	21.3	18.9	18.3	18.2	14.8	13.9
175- 200	25	9.8	9.8	10.1	10.3	10.5	10.8	12.4	14.7	15.1	14.9	11.7	12.1	11	8	7.4
200-225	25	8.4	8.4	8.4	8.2	8.3	8.9	11	11.4	11.4	9.8	7.3	8.1	6.1	3.7	3.3

Equivalent dose rate from LAr EC calorimeter for T= 10 y, t= 5 d

Table A4.1 (continuation)

				Equina							<u>, , , , , , , , , , , , , , , , , , , </u>					
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5	10.1	10.3	10.9	11.8	12.8	14.6	18.1	26	40.7	62	90.9	130.9	179.8	239.5	261.4
5- 10	5	9.4	9.5	10.1	10.9	12	13.5	17	24.4	38.2	58.6	85.4	121.1	165.1	211.1	222.4
10- 20	10	9	9.1	9.6	10.4	11.5	12.9	16.2	23.1	36	55	78.5	109.7	149	198.3	213.1
20- 30	10	8.5	8.7	9.2	9.8	10.8	12.3	15.1	21.4	33.3	50.1	70.5	96.5	128.4	178.1	201.7
30- 45	15	7.9	8	8.5	9	9.9	11.2	13.8	19.4	29.9	43.9	60.1	80.1	103.2	132.6	142.4
45- 60	15	7.2	7.3	7.7	8.2	9	10.1	12.4	17.3	26.2	38.1	50.8	64.2	77.7	91.6	94.2
60- 75	15	6.6	6.7	7	7.4	8	9	11.1	15.6	23.5	33.4	41.7	50.1	57.4	63.5	63.5
75-95	20	5.7	5.8	6.1	6.4	6.9	7.9	10.1	14.3	20.8	27.2	33	36.4	40.2	41.7	40.6
95- 115	20	4.8	4.9	5.2	5.5	6.3	7.4	9.6	12.7	17.3	21.8	24.4	25.3	27.3	26.3	24.8
115- 125	10	4.5	4.6	4.9	5.4	6.3	7.4	9.1	11.4	15.1	18	19.4	19.2	20.7	18.8	17.4
125- 150	25	4.5	4.6	5.1	5.5	6.3	7.1	8.1	9.9	12.8	14.3	14.6	14.1	15.3	13	12.2
150- 175	25	4.8	4.9	5.2	5.5	5.8	6	6.4	8.4	9.7	10.6	9.4	9.6	9.9	7.7	7.3
175-200	25	4.7	4.7	4.7	4.6	4.6	4.6	5.6	7.2	7.3	7.6	6	6.8	6.2	4.3	4
200-225	25	3.7	3.6	3.6	3.5	3.5	4	5.3	5.4	5.8	5	3.8	4.8	3.6	2.1	1.9

Equivalent dose rate from LAr EC calorimeter for T= 10 y, t= 100 d



Fig. A4.2. To calculations of dose rate from LAr Barrel.

Table A4.2

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5	8.1	7.1	5.8	6.1	6.3	4.1	4.4	3	1.7	1.7					
5- 10	5	8.1	7.1	5.9	6.2	6.3	4.1	4.4	3	1.7	1.7					
10- 20	10	8.1	7.2	5.9	6.1	6.2	4.2	4.4	3	2	1.7					
20- 30	10	8.1	7.3	6	6.2	6	4.6	4.1	3	2.2	1.7					
30- 45	15	8	7.3	6.4	6.2	5.6	5.1	3.9	3.1	2.4	1.6					
45- 60	15	7.8	7.4	6.6	5.9	5.5	5.4	3.7	3.3	2.4	1.5					
60- 75	15	7.8	7.6	6.7	5.8	5.7	5	3.9	3.2	2.4	1.5					
75-95	20	7.9	7.7	6.8	6.1	5.3	4.9	4	3	2.5	1.5					
95- 115	20	8	7.9	7	5.9	5.2	4.8	3.8	2.8	2.3	1.5					
115- 125	10	8.5	7.9	7.1	6	5.1	4.4	3.8	2.8	2.3	1.6					
125- 150	25	9	7.8	7.1	6	5	4.4	3.7	2.7	2.1	1.6					
150- 175	25	8.5	7.4	6.7	5.7	4.8	3.9	3.4	2.6	2	1.4					
175-200	25	7.2	6.2	5.9	5.3	4.4	3.8	3.3	2.5	1.9	1.3					
200-225	25	6	5.1	4.8	4.5	3.7	3.2	2.7	2.2	1.7	1.2					

Equivalent dose rate from LAr Barrel calorimeter for T= 100 d, t= 5d

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5	2.2	2	1.8	1.9	1.6	1.3	1.2	0.9	0.5	0.4					
5- 10	5	2.2	2	1.8	1.9	1.6	1.3	1.2	0.9	0.5	0.4					
10- 20	10	2.2	2	1.9	1.8	1.6	1.3	1.2	0.9	0.5	0.4					
20- 30	10	2.2	2	2	1.8	1.6	1.4	1.2	0.9	0.7	0.4					
30- 45	15	2.3	2.1	1.9	1.8	1.6	1.5	1.1	0.9	0.7	0.4					
45- 60	15	2.3	2.2	2	1.8	1.6	1.5	1.1	0.9	0.7	0.4					
60- 75	15	2.3	2.2	2	1.8	1.6	1.4	1.2	0.8	0.7	0.4					
75-95	20	2.3	2.3	2.1	1.7	1.5	1.4	1.2	0.8	0.7	0.4					
95- 115	20	2.3	2.2	2	1.7	1.5	1.3	1.1	0.8	0.7	0.4					
115- 125	10	2.5	2.3	2	1.7	1.4	1.2	1.1	0.8	0.6	0.4					
125- 150	25	2.7	2.2	2	1.7	1.4	1.2	1	0.7	0.6	0.4					
150- 175	25	2.3	2	1.8	1.6	1.3	1.1	1	0.7	0.6	0.4					
175-200	25	2	1.8	1.6	1.5	1.2	1.1	0.9	0.7	0.6	0.4					
200-225	25	1.9	1.5	1.4	1.3	1.1	0.9	0.8	0.6	0.5	0.3					

Table A4.2 (continuation) Equivalent dose rate induced by high-energy hadrons from calorimeter for T= 100 d, t= 100 d

Table A4.2 (continuation)

		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5	14.2	12.4	10.8	11.1	10.6	7.8	7.5	5.5	3.4	2.8					
5- 10	5	14.1	12.5	10.8	11	10.6	7.8	7.5	5.5	3.4	2.8					
10- 20	10	14.1	12.7	11	11	10.4	7.9	7.5	5.5	3.6	2.8					
20- 30	10	14.1	12.6	11.2	10.9	10.3	8.3	7.3	5.5	3.9	2.8					
30- 45	15	14	12.8	11.5	10.9	9.9	8.9	7.1	5.5	4.2	2.7					
45- 60	15	13.9	13	11.9	10.8	9.8	9.2	6.9	5.7	4.3	2.8					
60- 75	15	14	13.4	12.4	10.6	10	9	7	5.5	4.4	2.9					
75-95	20	14.3	13.9	12.4	10.9	9.6	8.7	7.1	5.2	4.3	2.8					
95- 115	20	14.4	14.3	12.7	10.8	9.3	8.5	6.6	5.1	4.1	2.8					
115- 125	10	15.8	14.5	12.7	10.7	9.2	7.8	6.6	4.9	3.9	2.7					
125- 150	25	16.8	14.3	12.7	10.8	9	7.7	6.5	4.6	3.7	2.8					
150- 175	25	15.3	13	12	10.2	8.4	7.1	5.9	4.7	3.7	2.7					
175-200	25	13	11.2	10.7	9.6	8.1	6.9	5.8	4.4	3.3	2.4					
200-225	25	11.4	9.7	9.1	8.3	7	5.8	4.9	3.9	3.1	2.1					

Equivalent dose rate induced by high-energy hadrons from calorimeter for T= 10 y, t= 5 d

			antaiont	4000 14) naarer				10 J, t				
		340	340-	350-	365-	380-	405-	430-	480-	530-	580-	605-	630-	645-	660-	670
R/Z,			350	365	380	405	430	480	530	580	605	630	645	660	670	
cm	dR\dZ	0	10	15	15	25	25	50	50	50	25	25	15	15	10	0
0-5	5	7.4	7.3	6.9	6.4	6.2	5.6	4.7	4.1	3.1	2	1.4				
5- 10	5	7.4	7.3	6.9	6.4	6.3	5.6	4.7	4.1	3.1	2.1	1.4				
10- 20	10	7.4	7.4	7	6.5	6.2	5.5	4.7	4.1	3.1	2.1	1.4				
20- 30	10	7.4	7.4	7.1	6.6	6.1	5.5	4.8	4	3.1	2.2	1.4				
30- 45	15	7.3	7.5	7.2	6.7	6	5.5	5	3.9	3.1	2.3	1.5				
45- 60	15	7.1	7.6	7.3	6.8	6.1	5.5	5	3.9	3	2.3	1.6				
60- 75	15	7.1	7.7	7.6	7	6.1	5.5	5	4	3	2.4	1.6				
75-95	20	7.2	8.1	7.9	7.1	6.3	5.4	4.9	3.9	2.9	2.4	1.6				
95- 115	20	7.2	8.2	8.1	7.4	6.2	5.3	4.7	3.7	2.9	2.3	1.5				
115- 125	10	7.6	9.3	8.3	7.2	6.1	5.2	4.3	3.7	2.7	2.1	1.5				
125- 150	25	8	9.8	8.3	7.2	6.1	4.9	4.2	3.6	2.5	2.1	1.5				
150- 175	25	7.4	8.4	7.2	6.6	5.7	4.7	3.9	3.3	2.6	2.2	1.5				
175-200	25	5.9	7.3	6.3	6	5.4	4.5	3.8	3.2	2.5	1.9	1.3				
200-225	25	4.5	6.8	5.8	5.3	4.8	4	3.3	2.7	2.2	1.7	1.2				

Table A4.2 (continuation) Equivalent dose rate induced by high-energy hadrons from calorimeter for T= 10 y, t= 100 d

Addendum 5



Fig. A5.1 General detector opening layout to calculations of access dose rate.

Table A5.1

Equivalent dose rate in the general access scenario for T= 2 y, t= 5 d

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0-5	5																	
5- 10	5					411.0	460.9	1062.5	4048.1	2349.5	1587.2	2110.3	3358.6	3036.7	2604.9	2468.4	2454.4	1401.2
10-20	10					358.8	394.3	651.9	1246.5	1083.6	839.8	1042.0	1516.7	1435.7	1274.1	1241.3	1264.8	786.9
20- 30	10					292.5	315.3	424.1	584.8	594.2	536.1	634.7	849.9	838.5	773.6	771.0	796.1	542.9
30- 45	15					243.6	255.4	291.4	345.5	369.5	369.5	425.4	532.8	541.6	517.6	527.3	551.8	388.7
45- 60	15					205.1	211.3	213.4	233.9	252.1	266.1	301.5	359.3	372.9	368.8	378.5	394.7	282.3
60- 75	15					164.9	168.4	169.1	179.0	192.1	205.9	231.0	266.9	280.8	282.0	286.6	291.9	202.5
75-95	20					135.4	136.7	136.4	141.7	150.4	161.7	179.9	202.3	213.8	215.9	214.8	211.9	140.1
95- 115	20					119.6	118.0	114.0	115.3	120.9	129.3	141.3	155.7	165.2	164.6	159.3	154.1	96.6
115- 125	10					109.0	107.4	101.4	101.5	105.6	111.7	121.0	131.8	138.9	137.0	130.4	124.7	75.4
125- 150	25					91.7	90.1	88.3	88.8	91.4	95.8	102.6	110.9	114.5	112.3	105.6	100.4	59.2
150- 175	25					75.7	74.5	73.7	74.1	75.8	78.1	82.9	88.4	90.0	86.2	80.5	76.3	43.0
175-200	25					63.0	62.1	62.4	63.1	63.9	65.6	68.8	71.8	72.2	68.0	63.5	59.6	32.1
200-225	25					53.8	52.8	52.7	53.2	53.5	55.0	57.8	59.4	59.1	54.7	51.0	47.6	24.5

Table A5.1 (continuation)

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R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0-5	5																	
5- 10	5					274.5	304.4	681.0	2572.3	1485.6	1004.1	1343.4	2161.9	1953.9	1669.9	1583.7	1585.1	924.6
10-20	10					240.1	260.1	419.9	794.3	688.0	533.6	665.8	976.4	923.5	818.5	802.3	827.7	533.4
20- 30	10					195.1	208.7	275.2	374.7	379.3	342.5	406.7	547.7	539.8	497.3	499.4	524.0	371.3
30- 45	15					164.6	171.7	190.8	223.4	237.6	237.1	273.4	343.4	348.6	332.5	339.9	357.9	258.2
45- 60	15					140.8	144.4	141.2	152.2	163.7	171.6	194.0	231.2	239.8	236.7	243.1	253.6	182.2
60- 75	15					112.7	114.4	112.1	117.5	125.2	133.1	148.8	171.4	180.5	180.8	183.5	186.9	129.7
75-95	20					92.1	93.3	91.0	93.7	98.3	104.6	115.9	130.3	137.4	138.5	137.4	135.5	89.7
95- 115	20					81.8	80.5	76.2	76.4	79.2	84.1	91.7	100.5	106.2	105.6	102.0	98.7	62.0
115- 125	10					74.9	73.4	68.0	67.1	69.2	72.8	78.6	85.0	89.3	88.0	83.6	79.9	48.5
125- 150	25					62.3	61.3	59.0	59.0	60.1	62.8	66.6	71.6	74.0	72.1	67.7	64.4	38.1
150- 175	25					50.9	49.9	49.2	49.3	49.9	51.5	53.9	57.2	58.1	55.6	51.8	48.9	27.9
175-200	25					42.7	41.6	41.6	41.8	42.1	42.8	44.8	46.9	46.8	43.7	40.9	38.3	20.7
200-225	25					36.0	35.2	35.2	35.2	35.2	36.1	37.9	38.4	38.6	35.3	32.9	30.6	15.9

Equivalent dose rate in the general access scenario for T= 2 y, t= 15 d

Table A5.1 (continuation)

								Ŭ				,						
ר/ ס		280	280-	290-	315-	340	340-	350-	365-	380-	405-	430-	480-	530-	580-	630-	660-	670
R/Z,			290	315	340		350	365	380	405	430	480	530	580	630	660	670	
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					202.3	222.1	481.9	1796.2	1028.4	694.2	939.2	1529.8	1377.5	1166.5	1110.7	1120.9	666.3
10-20	10					176.8	189.0	297.3	555.3	478.7	371.3	466.8	691.0	651.8	574.7	567.0	593.7	393.9
20- 30	10					143.1	151.4	196.3	263.6	266.1	239.8	286.1	387.3	381.2	349.9	354.3	377.7	278.4
30- 45	15					122.0	126.5	137.3	158.8	167.9	167.2	192.9	243.0	246.2	234.1	241.0	256.9	188.8
45- 60	15					106.2	108.5	102.5	109.4	116.5	121.7	137.4	163.5	169.2	166.7	171.8	179.3	129.9
60- 75	15					84.6	86.0	82.0	84.8	89.4	94.8	105.5	121.1	127.3	127.3	129.4	131.4	91.8
75- 95	20					69.0	69.4	67.0	67.7	70.6	74.7	81.9	92.2	97.2	97.3	96.8	95.5	63.7
95- 115	20					61.4	60.2	56.1	55.4	57.0	60.2	65.1	71.4	74.9	74.2	72.1	69.4	44.1
115- 125	10					56.6	55.0	50.1	49.1	50.0	52.2	56.1	60.2	63.1	61.8	59.1	56.2	34.4
125- 150	25					46.7	45.4	43.4	43.2	43.5	45.1	47.5	50.7	52.4	50.9	48.1	45.4	27.1
150- 175	25					37.9	37.1	36.3	36.2	36.6	36.8	38.4	40.9	41.3	39.4	36.8	34.4	19.8
175-200	25					31.6	30.9	30.7	30.5	30.4	30.8	32.1	33.4	33.1	31.1	29.0	27.0	14.8
200-225	25					26.8	25.9	25.4	25.6	25.6	26.0	27.2	27.6	27.4	25.2	23.3	21.5	11.4

Equivalent dose rate in the general access scenario for T= 2 y, t= 30 d

Table A5.1 (continuation)

				Lyuiva				jenerai	000000	5 300110		I - Z y,	1- 100	u				
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0-5	5																	
5- 10	5					114.5	125.0	261.1	940.3	529.1	354.5	487.0	805.6	720.3	608.1	585.5	596.0	366.2
10- 20	10					101.6	106.1	160.8	292.5	249.0	192.2	243.7	364.6	342.8	303.2	306.2	328.2	229.2
20- 30	10					81.9	84.7	106.8	140.6	139.9	125.5	150.6	205.0	201.5	186.8	195.5	218.3	178.8
30- 45	15					70.2	72.2	75.5	85.9	89.5	88.6	102.6	128.9	131.3	126.5	134.7	148.8	119.0
45- 60	15					61.7	63.1	57.6	60.3	62.9	65.1	73.7	87.2	90.8	90.7	96.1	102.6	78.9
60- 75	15					49.4	50.0	46.5	47.2	48.9	51.4	56.8	65.1	68.8	69.7	72.3	74.5	54.9
75-95	20					40.8	40.7	38.3	38.4	38.9	40.9	44.5	49.9	52.9	53.5	53.7	53.8	37.7
95- 115	20					36.4	35.3	32.4	31.6	31.9	32.9	35.8	39.0	40.9	40.9	40.0	38.8	25.4
115- 125	10					33.3	32.3	28.7	27.9	28.1	29.0	31.1	33.0	34.6	34.1	32.5	31.2	19.7
125- 150	25					27.7	26.6	25.4	24.6	24.6	25.4	26.5	27.9	29.0	28.0	26.4	25.0	15.4
150- 175	25					22.5	22.1	21.3	20.7	20.6	20.8	21.4	22.5	22.8	21.6	20.1	18.8	11.1
175-200	25					18.6	18.1	17.7	17.8	17.4	17.5	18.1	18.6	18.3	17.0	16.0	14.4	7.9
200-225	25					15.7	15.3	14.7	14.6	14.8	14.7	15.3	15.4	15.1	13.5	12.8	11.4	5.9

Equivalent dose rate in the general access scenario for T=2 y, t= 100 d



Fig. A5.2. Detector opening layout to calculations of access dose rate – TRT C removed.

Table A5.2

Equivalent dose rate in the ID access scenario for T	Γ= 2 v	∵t= 5	5 d —	-TRT C	removed
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R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					410.6	460.5	1062.3	4047.9	2349.4	1587.1	2110.2	3358.6	3036.7	2604.9	2468.4	2454.4	1401.2
10- 20	10					358.4	393.9	651.7	1246.3	1083.5	839.7	1041.9	1516.7	1435.7	1274.1	1241.3	1264.8	786.9
20- 30	10					292.1	314.9	423.9	584.6	594.1	536.0	634.6	849.9	838.5	773.6	771.0	796.1	542.9
30- 45	15					243.1	255.0	291.2	345.3	369.4	369.4	425.3	532.8	541.6	517.6	527.3	551.8	388.7
45- 60	15					204.5	210.8	213.1	233.6	252.0	266.0	301.4	359.2	372.9	368.8	378.5	394.7	282.3
60- 75	15					164.2	167.9	168.8	178.7	192.0	205.8	230.9	266.8	280.8	282.0	286.6	291.9	202.5
75-95	20					134.9	136.3	136.2	141.4	150.3	161.6	179.9	202.2	213.8	215.9	214.8	211.9	140.1
95- 115	20					119.2	117.8	113.8	115.2	120.8	129.2	141.3	155.6	165.2	164.6	159.3	154.1	96.6
115- 125	10					108.7	107.2	101.2	101.4	105.6	111.6	121.0	131.7	138.9	137.0	130.4	124.7	75.3
125- 150	25					91.4	90.0	88.2	88.7	91.3	95.6	102.6	110.8	114.5	112.3	105.6	100.4	59.1
150- 175	25					75.5	74.4	73.7	74.0	75.7	78.1	82.8	88.3	89.9	86.2	80.5	76.3	43.0
175-200	25					63.0	62.1	62.3	63.0	63.8	65.6	68.8	71.7	72.2	68.0	63.5	59.6	32.1
200-225	25					53.7	52.6	52.6	53.2	53.5	54.9	57.7	59.4	59.1	54.7	51.0	47.6	24.5

			Equiv.	olont d	oo rote	in the			norio f	or T_ 0	v +_ 10	T h		T	able A	5.2 (cor	ntinuatio	on)
		-	Equiva	alent de	use rate	e in the	ID acc		enano io	J = Z	y, t= 13	5 u — I	RICI	emovec		-		-
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR\dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					274.5	304.4	680.9	2572.2	1485.6	1004.0	1343.4	2161.9	1953.9	1669.9	1583.7	1585.1	924.6
10- 20	10					240.1	260.1	419.8	794.2	688.0	533.5	665.8	976.4	923.5	818.5	802.3	827.7	533.4
20- 30	10					195.1	208.7	275.1	374.6	379.3	342.4	406.7	547.7	539.8	497.3	499.4	524.0	371.3
30- 45	15					164.5	171.7	190.7	223.3	237.6	237.1	273.4	343.4	348.6	332.5	339.9	357.9	258.2
45- 60	15					140.7	144.3	141.2	152.1	163.7	171.6	194.0	231.2	239.8	236.7	243.1	253.6	182.2
60- 75	15					112.6	114.4	112.1	117.4	125.2	133.1	148.7	171.4	180.5	180.8	183.5	186.9	129.7
75- 95	20					92.1	93.2	91.0	93.7	98.3	104.6	115.9	130.3	137.4	138.5	137.4	135.5	89.7
95- 115	20					81.8	80.5	76.0	76.4	79.2	84.1	91.7	100.5	106.2	105.6	102.0	98.7	62.0
115- 125	10					74.8	73.4	67.9	67.1	69.2	72.8	78.6	85.0	89.3	88.0	83.6	79.9	48.5
125- 150	25					62.2	61.2	59.0	59.0	60.0	62.8	66.6	71.6	74.0	72.1	67.7	64.4	38.1
150- 175	25					50.8	49.9	49.2	49.2	49.9	51.5	53.9	57.2	58.1	55.6	51.8	48.9	27.9
175-200	25					42.6	41.6	41.6	41.8	42.1	42.8	44.8	46.9	46.8	43.7	40.9	38.3	20.7
200-225	25					36.0	35.2	35.2	35.1	35.2	36.1	37.9	38.4	38.5	35.3	32.9	30.6	15.9

			Eauiv	alent de	ose rate	e in the	ID acc	ess sce	enario fo	or T= 2	v. t= 30) d —T	RT C re	T emovec	able A	5.2 (coi	ntinuatio	on)
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0-5	5																	
5- 10	5					202.3	222.1	481.9	1796.2	1028.4	694.2	939.2	1529.8	1377.5	1166.5	1110.7	1120.9	666.3
10-20	10					176.8	189.0	297.3	555.3	478.7	371.3	466.8	691.0	651.8	574.7	567.0	593.7	393.9
20- 30	10					143.0	151.4	196.3	263.6	266.1	239.8	286.1	387.3	381.2	349.9	354.3	377.7	278.4
30- 45	15					121.9	126.4	137.3	158.8	167.9	167.2	192.9	243.0	246.2	234.1	241.0	256.9	188.8
45- 60	15					106.2	108.4	102.5	109.4	116.5	121.7	137.4	163.5	169.2	166.7	171.8	179.3	129.9
60- 75	15					84.6	86.0	82.0	84.7	89.4	94.8	105.5	121.1	127.3	127.3	129.4	131.4	91.8
75-95	20					69.0	69.4	66.9	67.6	70.6	74.7	81.9	92.2	97.2	97.3	96.8	95.5	63.7
95- 115	20					61.4	60.2	56.1	55.4	56.9	60.2	65.1	71.3	74.9	74.2	72.1	69.4	44.1
115- 125	10					56.5	55.0	50.1	49.1	50.0	52.2	56.1	60.2	63.1	61.8	59.1	56.2	34.4
125- 150	25					46.7	45.4	43.4	43.2	43.5	45.1	47.5	50.7	52.4	50.9	48.1	45.4	27.1
150- 175	25					37.9	37.1	36.3	36.2	36.6	36.8	38.4	40.9	41.3	39.4	36.8	34.4	19.8
175-200	25					31.6	30.9	30.7	30.5	30.4	30.8	32.1	33.4	33.1	31.1	29.0	27.0	14.8
200-225	25					26.7	25.9	25.4	25.6	25.6	26.0	27.2	27.6	27.4	25.2	23.3	21.5	11.4

									. ,	— •		o 1 -		Т	able A	5.2 (cor	ntinuatio	on)
			Equiva	alent do	se rate	in the	D acce	ess sce	nario to	r = 2	y, t= 10	0 d — I	RICr	emove	d			
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					114.5	125.0	261.1	940.3	529.1	354.5	487.0	805.6	720.3	608.1	585.5	596.0	366.2
10- 20	10					101.6	106.1	160.8	292.5	249.0	192.2	243.7	364.6	342.8	303.2	306.2	328.2	229.2
20- 30	10					81.9	84.7	106.8	140.6	139.9	125.5	150.6	205.0	201.5	186.8	195.5	218.3	178.8
30- 45	15					70.2	72.2	75.5	85.9	89.5	88.6	102.6	128.9	131.3	126.5	134.7	148.8	119.0
45- 60	15					61.7	63.0	57.6	60.2	62.9	65.1	73.7	87.2	90.8	90.7	96.1	102.6	78.9
60- 75	15					49.4	50.0	46.5	47.2	48.9	51.4	56.8	65.1	68.8	69.7	72.3	74.5	54.9
75-95	20					40.8	40.7	38.3	38.4	38.9	40.9	44.5	49.9	52.9	53.5	53.7	53.8	37.7
95- 115	20					36.4	35.3	32.4	31.6	31.9	32.9	35.8	39.0	40.9	40.9	40.0	38.8	25.4
115- 125	10					33.3	32.3	28.7	27.9	28.1	29.0	31.1	33.0	34.6	34.1	32.5	31.2	19.7
125- 150	25					27.7	26.6	25.4	24.6	24.6	25.4	26.4	27.9	29.0	28.0	26.4	25.0	15.4
150- 175	25					22.5	22.1	21.3	20.7	20.6	20.8	21.4	22.5	22.8	21.6	20.1	18.8	11.1
175-200	25					18.6	18.1	17.7	17.8	17.4	17.5	18.1	18.6	18.3	17.0	16.0	14.4	7.9
200-225	25					15.7	15.3	14.7	14.6	14.8	14.7	15.3	15.4	15.1	13.5	12.8	11.4	5.9



Fig. A5.3. Detector opening layout to calculations of access dose rate – TRT C, LAr EndCap removed.

Table A5.3

										<u> </u>		,						
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					393.7	443.3	1044.2	4028.5	2328.1	1563.2	2080.9	3318.0	2975.3	2493.0	2269.4	2165.8	1072.0
10-20	10					342.3	377.5	634.3	1227.6	1063.0	816.6	1013.7	1477.5	1376.1	1171.4	1063.9	1016.2	503.5
20- 30	10					276.8	299.3	407.4	567.0	574.7	514.3	608.1	813.0	782.4	680.6	617.6	588.7	292.1
30- 45	15					229.1	240.8	276.3	329.5	352.1	350.0	401.6	500.0	493.0	438.6	399.1	381.0	188.9
45- 60	15					192.1	198.2	199.9	219.5	236.8	248.9	280.4	330.2	330.6	300.5	275.0	262.9	130.3
60- 75	15					153.1	156.6	156.9	166.2	178.3	190.4	211.8	240.5	242.6	224.1	206.2	197.9	97.9
75-95	20					125.0	126.3	125.8	130.3	138.1	147.6	162.2	178.4	181.1	169.1	157.0	150.9	74.6
95- 115	20					110.5	109.0	104.4	105.1	109.5	116.2	125.3	135.3	137.1	129.3	120.8	116.9	57.7
115- 125	10					100.5	98.9	92.2	91.7	94.7	99.3	106.4	113.2	114.5	108.6	102.0	98.7	48.5
125-150	25					83.4	81.8	79.5	79.3	81.0	84.3	89.6	94.2	95.0	90.5	85.3	82.7	40.7
150- 175	25					67.7	66.5	65.4	65.3	66.5	68.3	71.7	74.8	75.2	71.8	67.9	66.1	32.4
175-200	25					55.8	54.8	54.9	55.3	55.9	57.4	59.5	61.1	61.2	58.6	55.7	54.1	26.5
200-225	25					47.3	46.2	46.2	46.9	47.2	48.2	49.6	51.0	51.0	48.7	46.4	45.1	22.1

Equivalent dose rate in the ID access scenario for T= 2 y, t= 5 d -- TRT C, LAr EndCap removed

Table A5.3 (continuation)

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					263.6	293.2	669.0	2559.4	1471.6	988.1	1323.8	2134.4	1911.5	1591.5	1438.3	1370.5	679.5
10- 20	10					229.4	249.3	408.3	782.0	674.4	518.2	647.0	949.9	882.9	747.3	675.5	643.2	318.9
20- 30	10					185.0	198.4	264.2	362.9	366.5	327.9	388.9	522.8	502.1	434.1	392.4	373.4	185.1
30- 45	15					155.2	162.3	180.7	212.8	226.1	224.1	257.5	321.6	316.4	279.9	253.6	241.6	119.8
45- 60	15					132.4	135.9	132.3	142.8	153.5	160.3	180.2	212.4	212.4	192.0	174.9	167.3	82.9
60- 75	15					105.1	106.8	104.3	109.1	116.2	123.1	136.5	154.7	155.9	143.3	131.4	125.9	62.3
75-95	20					85.6	86.6	84.2	86.5	90.5	95.9	104.9	115.1	116.3	108.4	100.1	96.1	47.5
95- 115	20					76.3	74.9	70.2	70.1	72.2	75.9	81.5	87.3	88.4	82.9	77.2	74.4	36.7
115- 125	10					69.7	68.2	62.4	61.1	62.4	64.9	69.1	73.2	73.8	69.7	65.1	62.9	31.0
125- 150	25					57.3	56.2	53.5	53.0	53.4	55.3	58.3	61.1	61.3	58.1	54.4	52.7	26.0
150- 175	25					45.8	44.8	43.7	43.5	43.9	45.2	46.9	48.6	48.7	46.1	43.4	42.1	20.8
175-200	25					37.8	36.8	36.8	36.9	37.1	37.7	39.0	39.9	39.7	37.5	35.6	34.6	17.0
200-225	25					32.0	31.2	31.3	31.2	31.4	31.9	32.6	33.1	33.2	31.3	29.6	28.9	14.2

Equivalent dose rate in the ID access scenario for T= 2 y, t= 15 d-- TRT C, LAr EndCap removed
Table A5.3 (continuation)

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					194.3	214.0	473.3	1787.0	1018.2	682.7	924.8	1509.3	1345.5	1106.4	995.9	947.6	469.7
10- 20	10					169.2	181.2	289.0	546.4	468.9	360.2	452.9	671.4	621.5	520.8	467.9	445.3	220.7
20- 30	10					135.6	143.9	188.4	255.1	256.7	229.2	273.0	369.0	353.4	302.7	272.2	258.8	128.3
30- 45	15					115.1	119.5	130.1	151.0	159.4	157.6	181.3	227.0	222.7	195.3	176.4	167.9	83.0
45- 60	15					100.1	102.2	96.1	102.5	109.0	113.3	127.3	150.0	149.4	134.2	121.9	116.2	57.4
60- 75	15					79.2	80.5	76.3	78.7	82.9	87.6	96.8	109.2	109.7	100.2	91.7	87.5	43.3
75-95	20					64.4	64.8	62.0	62.6	65.2	68.6	74.3	81.4	82.0	75.7	70.0	66.9	33.1
95- 115	20					57.7	56.3	52.1	51.1	52.1	54.5	57.9	61.8	62.2	57.9	54.1	51.8	25.6
115- 125	10					53.1	51.5	46.3	45.0	45.3	46.6	49.2	51.9	52.1	48.7	45.7	43.8	21.7
125- 150	25					43.3	41.9	39.7	39.0	38.8	39.7	41.5	43.4	43.3	40.8	38.4	36.8	18.2
150- 175	25					34.3	33.4	32.4	32.0	32.2	32.3	33.6	34.7	34.5	32.6	30.5	29.3	14.6
175-200	25					28.1	27.4	27.2	27.0	26.9	27.4	28.0	28.3	28.1	26.6	24.9	24.2	12.0
200-225	25					23.9	23.1	22.7	23.0	23.0	23.1	23.4	23.8	23.5	22.3	20.7	20.2	10.1

Equivalent dose rate in the ID access scenario for T= 2 y, t= 30 d--- TRT C, LAr EndCap removed

Table A5.3 (continuation)

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5																	
5- 10	5					109.6	120.1	255.9	934.6	522.8	347.4	478.1	792.8	700.1	569.7	509.2	482.1	239.0
10- 20	10					97.0	101.3	155.8	287.0	243.0	185.4	235.2	352.4	323.7	268.4	239.4	226.7	112.4
20- 30	10					77.4	80.2	102.0	135.4	134.2	119.0	142.5	193.6	184.2	156.2	139.4	131.9	65.4
30- 45	15					66.0	68.0	71.1	81.1	84.2	82.7	95.3	118.9	116.4	100.9	90.4	85.7	42.4
45- 60	15					58.0	59.2	53.5	55.9	58.2	59.9	67.4	78.7	78.1	69.3	62.4	59.4	29.4
60- 75	15					46.0	46.6	42.9	43.4	44.9	46.9	51.4	57.5	57.5	51.8	47.0	44.8	22.2
75-95	20					37.9	37.8	35.3	35.2	35.6	37.1	39.7	43.1	43.0	39.3	35.8	34.4	16.9
95- 115	20					34.1	32.9	30.0	28.9	28.9	29.4	31.2	32.9	32.8	30.1	27.8	26.7	12.9
115- 125	10					31.2	30.1	26.4	25.3	25.2	25.4	26.6	27.6	27.5	25.4	23.4	22.6	11.0
125- 150	25					25.6	24.5	23.0	21.9	21.6	21.9	22.5	23.2	23.0	21.3	19.7	19.1	9.2
150-175	25					20.2	19.7	18.7	18.0	17.8	17.9	18.4	18.5	18.2	17.0	15.7	15.3	7.4
175-200	25					16.3	15.8	15.5	15.5	15.2	15.3	15.5	15.2	15.0	13.8	13.0	12.5	6.0
200-225	25					14.0	13.6	13.1	13.0	13.1	12.8	12.8	12.9	12.5	11.5	10.9	10.5	5.0

Equivalent dose rate in the ID access scenario for T= 2 y, t= 100 d-- TRT C, LAr EndCap removed



Fig. A5.4. Detector opening layout to calculations of access dose rate – TRT C, LAr EndCap, and VA removed.

Table A5.4

									, •			,	, e.e.,					
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								60.2	26.9	17.8	13.9	9.2	6.2	4.0	2.3	2.3	0.7
5- 10	5					106.5	89.2	70.6	46.5	26.4	17.9	13.9	9.2	6.2	4.1	2.3	2.3	0.7
10- 20	10					85.7	72.8	49.5	36.9	25.6	17.9	13.9	9.2	6.4	4.1	2.3	2.3	0.7
20- 30	10					62.8	56.6	41.9	33.0	24.8	18.1	13.5	9.2	6.6	4.1	2.3	2.3	0.7
30- 45	15					61.8	58.3	39.3	30.5	23.4	18.1	13.0	9.3	6.8	4.0	2.3	2.3	0.7
45- 60	15					63.1	61.2	37.1	28.5	22.2	17.7	12.6	9.2	6.8	4.0	2.3	2.2	0.7
60- 75	15					49.8	48.6	33.9	26.5	21.4	16.9	12.3	9.0	6.7	3.9	2.3	2.2	0.6
75-95	20					41.7	40.2	30.6	24.7	20.0	16.2	12.3	8.4	6.8	3.8	2.3	2.2	0.6
95- 115	20					42.8	39.5	29.0	22.8	18.6	15.3	11.4	8.2	6.5	3.6	2.3	2.2	0.6
115- 125	10					41.4	38.3	27.2	21.5	17.6	14.4	11.2	8.0	6.2	3.6	2.3	2.2	0.5
125- 150	25					32.0	29.4	23.7	19.5	16.1	13.3	10.7	7.7	5.9	3.5	2.2	2.1	0.5
150- 175	25					24.7	22.7	19.3	16.5	14.0	11.6	9.4	7.3	5.6	3.4	2.2	2.0	0.5
175- 200	25					19.1	17.5	16.0	14.3	12.4	10.8	8.9	6.6	5.2	3.2	2.2	1.8	0.5
200-225	25					15.4	14.0	12.8	11.9	10.3	9.0	7.5	6.1	4.8	2.9	2.0	1.7	0.5

Equivalent dose rate in the ID access scenario for T= 2 y, t= 5 d – TRT C, LAr EndCap, and VA removed

Table A5.4 (continuation)

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								51.0	21.0	14.1	10.8	7.2	4.7	3.0	1.8	1.6	0.5
5- 10	5					82.8	70.6	59.0	38.6	20.8	14.2	10.8	7.2	4.7	3.0	1.8	1.6	0.5
10- 20	10					67.7	57.5	40.0	29.8	20.2	14.1	10.8	7.2	4.9	3.0	1.8	1.6	0.5
20- 30	10					49.8	45.1	33.5	25.9	19.4	14.2	10.6	7.2	5.0	2.9	1.8	1.6	0.5
30- 45	15					49.4	46.9	31.0	23.7	18.3	14.0	10.1	7.2	5.1	2.9	1.7	1.6	0.5
45- 60	15					50.8	49.3	29.5	21.9	17.5	13.7	9.7	7.0	5.2	3.0	1.7	1.6	0.5
60- 75	15					39.7	38.4	26.5	20.7	16.7	13.1	9.5	6.8	5.2	3.0	1.7	1.6	0.5
75-95	20					32.9	32.0	23.8	19.4	15.6	12.5	9.4	6.5	5.1	3.0	1.7	1.6	0.5
95- 115	20					33.4	30.8	22.4	17.9	14.4	11.8	8.9	6.3	5.1	2.8	1.7	1.6	0.5
115- 125	10					32.2	29.7	21.1	16.5	13.4	10.9	8.5	6.2	4.8	2.8	1.6	1.6	0.5
125- 150	25					24.7	22.9	18.1	15.0	12.1	10.1	8.1	6.0	4.6	2.7	1.6	1.5	0.5
150- 175	25					18.5	17.0	14.5	12.5	10.6	9.1	7.2	5.5	4.3	2.5	1.6	1.4	0.5
175-200	25					14.5	13.1	12.1	10.9	9.4	8.0	6.7	5.2	4.0	2.3	1.6	1.4	0.5
200-225	25					11.7	10.7	10.0	9.0	7.9	6.9	5.8	4.5	3.8	2.2	1.4	1.3	0.5

Equivalent dose rate in the ID access scenario for T= 2 y, t= 15 d – TRT C, LAr EndCap, and VA removed

Table A5.4 (continuation)

			1		1							· ·		<i>.</i>				
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								46.3	17.9	12.0	8.8	6.1	4.1	2.5	1.6	1.6	0.5
5- 10	5					69.0	59.7	53.5	34.2	17.6	12.0	8.8	6.0	4.1	2.5	1.6	1.6	0.5
10-20	10					57.1	48.4	34.9	25.7	17.2	12.0	8.8	6.0	4.1	2.5	1.6	1.6	0.5
20- 30	10					42.2	38.0	28.8	22.0	16.4	11.9	8.7	6.0	4.3	2.5	1.6	1.6	0.5
30- 45	15					41.7	39.6	26.4	20.2	15.5	11.9	8.4	6.0	4.3	2.3	1.6	1.6	0.5
45- 60	15					43.5	42.1	24.8	18.7	14.8	11.4	8.1	5.9	4.3	2.4	1.6	1.5	0.5
60-75	15					33.7	33.0	22.3	17.4	13.9	11.0	8.1	5.5	4.2	2.4	1.6	1.4	0.5
75-95	20					27.8	26.9	20.0	16.0	13.1	10.5	7.7	5.4	4.2	2.3	1.6	1.4	0.5
95- 115	20					27.9	25.7	18.8	14.8	11.9	9.9	7.3	5.2	3.9	2.1	1.6	1.2	0.5
115- 125	10					26.9	24.8	17.6	13.9	11.3	9.0	6.9	5.1	3.8	2.1	1.6	1.2	0.5
125- 150	25					20.6	18.8	15.0	12.6	10.1	8.2	6.5	4.9	3.7	2.2	1.6	1.2	0.5
150-175	25					15.3	14.1	12.0	10.4	8.9	7.2	5.9	4.6	3.6	2.2	1.4	1.1	0.5
175-200	25					11.9	10.9	9.9	8.9	7.7	6.7	5.5	4.2	3.3	2.1	1.2	1.1	0.5
200-225	25					9.8	8.9	7.9	7.5	6.7	5.7	4.7	3.8	3.0	2.0	1.1	1.0	0.5

Equivalent dose rate in the ID access scenario for T= 2 y, t= 30 d - TRT C, LAr EndCap, and VA removed

Table A5.4 (continuation)

												,		•				
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR\dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								37.5	12.3	8.2	6.0	3.9	2.8	1.6	0.9	0.8	0.3
5- 10	5					45.6	41.2	42.0	26.4	12.3	8.2	6.0	3.9	2.8	1.6	0.9	0.8	0.3
10- 20	10					39.6	33.3	25.4	18.7	11.8	8.3	6.0	3.9	2.9	1.6	0.9	0.8	0.3
20- 30	10					29.4	25.9	20.1	15.6	11.3	8.2	5.9	3.9	2.9	1.6	0.9	0.8	0.3
30- 45	15					28.3	27.0	18.0	13.9	10.5	8.0	5.9	3.8	2.9	1.6	0.9	0.8	0.3
45- 60	15					28.9	28.3	16.9	12.9	9.8	7.6	5.8	3.7	2.8	1.5	0.8	0.8	0.3
60- 75	15					22.7	22.2	15.1	11.9	9.4	7.5	5.5	3.7	2.9	1.5	0.8	0.8	0.3
75- 95	20					19.1	18.3	13.7	11.2	8.7	7.1	5.3	3.7	2.8	1.5	0.8	0.8	0.2
95- 115	20					18.7	17.1	12.9	10.2	8.2	6.4	5.0	3.6	2.7	1.4	0.8	0.8	0.1
115- 125	10					17.8	16.4	11.6	9.3	7.6	6.0	4.8	3.4	2.6	1.4	0.8	0.8	0.1
125- 150	25					13.9	12.6	10.3	8.3	6.8	5.7	4.4	3.3	2.5	1.4	0.8	0.8	0.1
150- 175	25					10.4	9.8	8.2	6.9	5.9	5.0	4.2	3.0	2.3	1.4	0.8	0.8	0.1
175- 200	25					7.9	7.3	6.7	6.1	5.3	4.6	3.9	2.8	2.2	1.1	0.8	0.7	0.1
200-225	25					6.7	6.2	5.5	5.1	4.7	3.9	3.2	2.6	2.0	1.1	0.8	0.6	0.1

Equivalent dose rate in the ID access scenario for T= 2 y, t= 100 d – TRT C, LAr EndCap, and VA removed



Fig. A5.5. Detector opening layout to calculations of access dose rate – TRT C, LAr EndCap, VA, and Pixel Tipe 2 services removed.

Table A5.5 (continuation)

Lyu	Ivalent				0000 30			<u> </u>	<u> </u>	(10, L)		Cap, v	л, апи і		he 7 se		eniove	u
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								54.1	22.4	14.8	12.0	8.2	5.5	3.5	1.9	1.9	0.6
5- 10	5					98.4	81.1	63.1	40.3	21.9	14.9	12.0	8.2	5.5	3.6	1.9	1.9	0.6
10-20	10					77.0	64.1	41.6	30.6	21.1	14.9	12.0	8.2	5.7	3.6	1.9	1.9	0.6
20- 30	10	42.2	41.2	38.3		52.4	46.3	33.1	26.4	20.2	15.1	11.7	8.2	5.9	3.6	1.9	1.9	0.6
30- 45	15	40.5	39.4	35.2		37.2	34.3	28.1	23.6	18.8	15.2	11.2	8.3	6.2	3.5	1.9	1.9	0.6
45- 60	15	43.6	40.4	34.0	31.0	28.8	27.8	24.9	21.6	17.9	14.9	10.9	8.2	6.2	3.5	1.9	1.9	0.6
60- 75	15	46.8	41.5	33.7	29.2	27.1	26.4	23.7	20.3	17.4	14.3	10.7	8.0	6.1	3.5	1.9	1.9	0.5
75-95	20	44.1	40.8	34.5	29.7	27.5	26.3	23.2	19.7	16.6	13.9	10.8	7.5	6.2	3.4	1.9	1.9	0.5
95- 115	20					34.2	31.0	23.8	19.0	15.8	13.3	10.1	7.3	5.9	3.2	1.9	1.9	0.5
115- 125	10					35.1	32.0	23.2	18.4	15.2	12.6	9.9	7.2	5.7	3.2	1.9	1.9	0.4
125- 150	25					27.4	24.9	20.7	17.1	14.1	11.7	9.6	6.9	5.4	3.1	1.9	1.8	0.4
150- 175	25					21.7	19.7	17.2	14.7	12.5	10.4	8.5	6.6	5.1	3.0	1.9	1.7	0.4
175-200	25					17.1	15.5	14.4	12.9	11.2	9.8	8.1	6.1	4.8	2.8	1.9	1.5	0.4
200-225	25					14.0	12.6	11.7	10.9	9.4	8.2	6.8	5.6	4.4	2.6	1.7	1.4	0.4

Equivalent dose rate in the ID access scenario for T= 2 y, t= 5 d- TRT C, LAr EndCap, VA, and Pixel Tipe 2 services removed

Table A5.5 (continuation)

ĽЧ	livalent	003610			10033 3	CENAIL		∠y, ι–	15 u-	$\mathbf{H} \mathbf{U}$		iucap,	٧л, ан		TIPE Z		3 161110	veu
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								45.9	17.2	11.5	9.2	6.3	4.2	2.6	1.5	1.3	0.4
5- 10	5					76.1	63.9	52.8	33.4	17.0	11.6	9.2	6.3	4.2	2.6	1.5	1.3	0.4
10- 20	10					60.4	50.3	33.4	24.5	16.4	11.5	9.2	6.3	4.4	2.6	1.5	1.3	0.4
20- 30	10	32.8	31.9	30.3		41.1	36.4	26.1	20.4	15.6	11.6	9.0	6.3	4.5	2.5	1.5	1.3	0.4
30- 45	15	31.7	30.5	27.3		28.9	26.8	21.6	17.8	14.5	11.6	8.7	6.3	4.6	2.5	1.4	1.3	0.4
45- 60	15	34.1	31.7	26.1	23.7	22.2	21.4	19.2	16.1	13.8	11.4	8.3	6.2	4.7	2.6	1.4	1.3	0.4
60- 75	15	36.1	32.1	26.1	22.5	20.6	19.8	18.0	15.5	13.4	10.9	8.2	6.0	4.7	2.6	1.4	1.3	0.4
75-95	20	33.9	31.7	26.5	22.8	20.9	20.2	17.6	15.2	12.7	10.5	8.1	5.7	4.6	2.6	1.4	1.3	0.4
95- 115	20					26.1	23.6	18.1	14.7	12.0	10.1	7.7	5.6	4.6	2.4	1.4	1.3	0.4
115- 125	10					26.8	24.3	17.7	13.9	11.4	9.4	7.4	5.5	4.3	2.4	1.3	1.3	0.4
125- 150	25					20.7	19.0	15.5	12.9	10.5	8.8	7.2	5.3	4.2	2.4	1.3	1.2	0.4
150- 175	25					15.9	14.5	12.7	10.9	9.3	8.0	6.4	5.0	3.9	2.2	1.3	1.1	0.4
175-200	25					12.7	11.5	10.8	9.7	8.4	7.2	6.0	4.7	3.6	2.0	1.3	1.1	0.4
200-225	25					10.6	9.6	9.1	8.1	7.1	6.2	5.2	4.1	3.4	1.9	1.1	1.0	0.4

Equivalent dose rate in the ID access scenario for T= 2 y, t= 15 d- TRT C, LAr EndCap, VA, and Pixel Tipe 2 services removed

Table A5.5 (continuation)

<u> </u>	uivalem	00361			000333	beenand		· ∠y, ι–	<u> 50 u – </u>	$\mathbf{I} \mathbf{V} \mathbf{I} \mathbf{O},$		ucap,	vA, and				stemov	
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								41.8	14.6	9.8	7.5	5.3	3.6	2.1	1.3	1.3	0.4
5- 10	5					63.1	53.8	48.0	29.7	14.3	9.8	7.5	5.2	3.6	2.1	1.3	1.3	0.4
10-20	10					50.9	42.2	29.2	21.1	13.9	9.8	7.5	5.2	3.6	2.1	1.3	1.3	0.4
20- 30	10	27.6	27.1	25.9		34.6	30.4	22.3	17.2	13.1	9.7	7.4	5.2	3.8	2.1	1.3	1.3	0.4
30- 45	15	26.6	25.6	23.2		24.1	22.3	18.3	15.2	12.2	9.8	7.1	5.2	3.8	2.0	1.3	1.3	0.4
45- 60	15	28.5	26.3	22.0	20.0	18.7	18.0	15.9	13.7	11.6	9.4	6.9	5.2	3.8	2.1	1.3	1.2	0.4
60- 75	15	29.9	26.6	21.8	18.8	17.1	16.8	14.9	12.8	11.0	9.1	6.9	4.8	3.8	2.1	1.3	1.1	0.4
75-95	20	28.0	26.2	22.5	19.0	17.3	16.6	14.5	12.4	10.6	8.8	6.6	4.7	3.8	2.0	1.3	1.1	0.4
95- 115	20					21.5	19.4	15.0	12.0	9.8	8.4	6.3	4.5	3.5	1.8	1.3	0.9	0.4
115- 125	10					22.2	20.1	14.6	11.6	9.5	7.7	5.9	4.5	3.4	1.8	1.3	0.9	0.4
125- 150	25					17.1	15.3	12.7	10.7	8.7	7.1	5.7	4.3	3.3	1.9	1.3	0.9	0.4
150- 175	25					13.0	11.8	10.4	9.1	7.8	6.3	5.2	4.1	3.2	1.9	1.1	0.9	0.4
175-200	25					10.4	9.4	8.8	7.9	6.8	6.0	4.9	3.8	3.0	1.8	0.9	0.9	0.4
200-225	25					8.8	7.9	7.1	6.7	6.0	5.1	4.2	3.4	2.7	1.7	0.9	0.8	0.4

Equivalent dose rate in the ID access scenario for T= 2y, t= 30 d- TRT C, LAr EndCap, VA, and Pixel Tipe 2 services removed

Table A5.5 (continuation)

	valunt u	1030 10			0033 30	Chano		_ y, i—	100 u	$\mathbf{H} \mathbf{U}$		iuoup,	v/, an		TIPC Z		3 101110	vcu
R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5								34.5	10.1	6.7	5.1	3.4	2.5	1.3	0.7	0.6	0.2
5- 10	5					41.7	37.3	38.4	23.4	10.0	6.7	5.1	3.4	2.5	1.3	0.7	0.6	0.2
10-20	10					35.5	29.2	21.6	15.6	9.5	6.8	5.1	3.4	2.6	1.3	0.7	0.6	0.2
20- 30	10	19.6	19.3	18.2		24.4	21.0	15.8	12.4	9.0	6.7	5.0	3.4	2.6	1.3	0.7	0.6	0.2
30- 45	15	18.2	17.7	15.8		16.7	15.6	12.7	10.5	8.3	6.5	5.0	3.3	2.6	1.3	0.7	0.6	0.2
45- 60	15	18.9	17.6	14.9	13.4	12.5	12.3	11.0	9.5	7.6	6.3	4.9	3.2	2.5	1.3	0.6	0.6	0.2
60- 75	15	19.7	17.9	14.7	12.9	11.6	11.3	10.1	8.9	7.5	6.2	4.7	3.2	2.6	1.3	0.6	0.6	0.2
75-95	20	18.8	17.5	15.1	12.9	11.9	11.3	10.0	8.7	7.0	5.9	4.5	3.2	2.5	1.3	0.6	0.6	0.2
95- 115	20					14.3	12.8	10.3	8.3	6.8	5.4	4.4	3.1	2.4	1.2	0.6	0.6	0.1
115- 125	10					14.5	13.2	9.6	7.7	6.4	5.1	4.2	3.0	2.3	1.2	0.6	0.6	0.1
125- 150	25					11.5	10.2	8.7	7.0	5.8	4.9	3.8	3.0	2.2	1.2	0.6	0.6	0.1
150- 175	25					8.8	8.2	7.1	6.0	5.1	4.4	3.7	2.7	2.0	1.2	0.6	0.6	0.1
175-200	25					6.9	6.3	5.9	5.4	4.7	4.1	3.4	2.5	2.0	0.9	0.6	0.6	0.1
200-225	25					5.9	5.4	4.9	4.6	4.2	3.4	2.9	2.3	1.8	0.9	0.6	0.5	0.1

Equivalent dose rate in the ID access scenario for T= 2 y, t= 100 d- TRT C, LAr EndCap, VA, and Pixel Tipe 2 services removed



Fig. A5.6. Detector opening layout to calculations of access dose rate – TRT C, LAr EndCap, VA, Pixel Tipe 2 services, Pixel Detector, and VI removed.

Table A5.6 (continuation)

Equivalent dose rate in the ID access scenario for T= 2 y, t= 5 d- TRT C, LAr EndCap, VA, Pixel Tipe 2 services, Pixel Detector, and VI removed

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0-5	5	31.5	30.8	26.1	23.4	21.9	20.5	18.2	17.1	15.7	11.9	10.5	7.4	4.9	3.0	1.6	1.6	0.5
5- 10	5	31.5	30.9	26.1	23.5	21.9	20.6	18.2	17.1	15.5	12.0	10.5	7.4	4.9	3.1	1.6	1.6	0.5
10- 20	10	32.0	31.2	26.3	23.5	22.0	20.6	18.5	17.2	15.3	12.1	10.5	7.4	5.1	3.1	1.6	1.6	0.5
20- 30	10	33.5	32.1	26.7	23.7	22.2	20.7	18.6	17.3	15.3	12.4	10.2	7.4	5.3	3.1	1.6	1.6	0.5
30- 45	15	34.7	33.3	27.6	23.9	22.2	20.8	19.0	17.3	14.9	12.8	9.8	7.5	5.6	3.0	1.6	1.6	0.5
45- 60	15	39.2	35.9	28.8	24.6	22.2	21.4	19.4	17.2	14.8	12.9	9.6	7.4	5.6	3.0	1.6	1.6	0.5
60- 75	15	43.3	38.0	29.9	25.1	22.9	22.3	19.9	17.1	14.9	12.5	9.5	7.2	5.5	3.0	1.6	1.6	0.4
75-95	20	41.3	38.0	31.6	26.8	24.7	23.5	20.6	17.4	14.7	12.3	9.7	6.8	5.6	3.0	1.6	1.6	0.4
95- 115	20					32.1	29.0	21.9	17.2	14.3	12.0	9.2	6.6	5.4	2.9	1.6	1.6	0.4
115- 125	10					33.4	30.3	21.6	16.9	13.9	11.4	9.0	6.5	5.2	2.9	1.6	1.6	0.3
125- 150	25					26.0	23.5	19.3	15.8	12.9	10.7	8.8	6.3	4.9	2.8	1.6	1.5	0.3
150- 175	25					20.6	18.6	16.1	13.7	11.6	9.6	7.8	6.0	4.6	2.7	1.6	1.5	0.3
175-200	25					16.1	14.6	13.5	12.0	10.4	9.0	7.4	5.6	4.4	2.5	1.6	1.3	0.3
200-225	25					13.2	11.8	10.9	10.1	8.7	7.5	6.2	5.1	4.1	2.3	1.5	1.2	0.3

Table A5.6 (continuation)

Equivalent dose rate in the ID access scenario for T= 2 y, t= 15 d- TRT C, LAr EndCap, VA, Pixel Tipe 2 services, Pixel Detector, and VI removed

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5	23.5	23.2	19.9	17.7	16.3	15.5	13.8	13.0	11.7	9.1	7.9	5.6	3.7	2.3	1.3	1.1	0.3
5- 10	5	23.6	23.2	19.9	17.7	16.3	15.5	13.8	13.0	11.6	9.2	7.9	5.6	3.7	2.3	1.3	1.1	0.3
10- 20	10	23.9	23.7	20.1	17.9	16.4	15.6	13.9	13.0	11.6	9.2	7.9	5.6	3.9	2.3	1.3	1.1	0.3
20- 30	10	25.2	24.0	20.4	18.2	16.5	15.7	14.1	12.8	11.5	9.4	7.8	5.6	4.0	2.2	1.3	1.1	0.3
30- 45	15	26.7	25.3	21.0	18.2	16.7	15.9	14.2	12.7	11.3	9.6	7.6	5.6	4.1	2.2	1.2	1.1	0.3
45- 60	15	30.4	27.9	21.8	18.5	16.8	16.2	14.7	12.6	11.3	9.7	7.2	5.6	4.2	2.3	1.2	1.1	0.3
60- 75	15	33.2	29.2	23.0	19.1	17.3	16.6	15.0	12.9	11.4	9.4	7.2	5.4	4.2	2.3	1.2	1.1	0.3
75-95	20	31.7	29.4	24.2	20.5	18.6	17.9	15.4	13.3	11.1	9.3	7.2	5.1	4.1	2.3	1.2	1.1	0.3
95- 115	20					24.5	22.0	16.6	13.3	10.7	9.0	6.9	5.0	4.1	2.1	1.2	1.1	0.3
115- 125	10					25.4	22.9	16.4	12.7	10.3	8.4	6.7	5.0	3.9	2.1	1.1	1.1	0.3
125- 150	25					19.5	17.8	14.4	11.9	9.6	8.0	6.5	4.8	3.8	2.1	1.1	1.0	0.3
150- 175	25					15.0	13.6	11.8	10.1	8.5	7.3	5.8	4.5	3.6	2.0	1.1	0.9	0.3
175-200	25					11.9	10.7	10.0	9.0	7.7	6.6	5.5	4.2	3.3	1.8	1.1	0.9	0.3
200-225	25					9.9	8.9	8.4	7.5	6.5	5.6	4.7	3.8	3.1	1.7	0.9	0.8	0.3

Table A5.6 (continuation)

Equivalent dose rate in the ID access scenario for T= 2 y, t= 30 d- TRT C, LAr EndCap, VA, Pixel Tipe 2 services, Pixel Detector, and VI removed

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5	19.4	19.0	16.6	14.8	13.4	12.6	11.7	10.7	9.5	7.7	6.4	4.7	3.2	1.8	1.1	1.1	0.3
5- 10	5	19.5	19.1	16.6	14.8	13.5	12.6	11.8	10.6	9.5	7.7	6.4	4.6	3.2	1.8	1.1	1.1	0.3
10-20	10	19.8	19.2	16.8	14.7	13.4	12.6	11.8	10.6	9.5	7.7	6.4	4.6	3.2	1.8	1.1	1.1	0.3
20- 30	10	20.7	20.0	17.1	14.8	13.4	12.8	11.8	10.5	9.4	7.8	6.3	4.6	3.4	1.8	1.1	1.1	0.3
30- 45	15	22.1	21.0	17.6	15.2	13.6	12.9	11.8	10.6	9.3	8.0	6.1	4.6	3.4	1.8	1.1	1.1	0.3
45- 60	15	25.2	22.9	18.2	15.4	14.0	13.4	12.0	10.6	9.3	7.9	6.0	4.6	3.4	1.9	1.1	1.0	0.3
60- 75	15	27.4	24.1	19.1	15.8	14.2	13.9	12.3	10.5	9.2	7.8	6.0	4.3	3.4	1.9	1.1	0.9	0.3
75-95	20	26.1	24.3	20.5	17.0	15.3	14.7	12.7	10.8	9.2	7.7	5.8	4.2	3.4	1.8	1.1	0.9	0.3
95- 115	20					20.1	18.0	13.7	10.8	8.7	7.5	5.6	4.0	3.1	1.6	1.1	0.7	0.3
115- 125	10					21.0	18.9	13.4	10.5	8.5	6.9	5.3	4.0	3.0	1.6	1.1	0.7	0.3
125- 150	25					16.1	14.4	11.8	9.8	7.9	6.4	5.1	3.8	3.0	1.7	1.1	0.7	0.3
150- 175	25					12.2	11.0	9.6	8.4	7.1	5.7	4.7	3.7	2.9	1.7	0.9	0.7	0.3
175-200	25					9.7	8.7	8.1	7.3	6.2	5.5	4.4	3.4	2.8	1.6	0.7	0.7	0.3
200-225	25					8.2	7.3	6.5	6.1	5.5	4.6	3.8	3.1	2.5	1.5	0.7	0.6	0.3

Table A5.6 (continuation)

Equivalent dose rate in the ID access scenario for T= 2 y, t= 100 d– TRT C, LAr EndCap, VA, Pixel Tipe 2 services, Pixel
Detector, and VI removed

R/Z,		280	280- 290	290- 315	315- 340	340	340- 350	350- 365	365- 380	380- 405	405- 430	430- 480	480- 530	530- 580	580- 630	630- 660	660- 670	670
cm	dR∖dZ	0	10	25	25	0	10	15	15	25	25	50	50	50	50	30	10	0
0- 5	5	13.1	12.6	11.0	9.8	8.9	8.3	7.8	7.2	6.1	5.1	4.3	3.0	2.2	1.1	0.6	0.5	0.1
5- 10	5	13.1	12.6	11.0	9.8	8.9	8.3	7.8	7.2	6.1	5.1	4.3	3.0	2.2	1.1	0.6	0.5	0.1
10-20	10	13.3	12.9	11.3	9.7	9.1	8.4	7.8	7.1	6.1	5.2	4.3	3.0	2.3	1.1	0.6	0.5	0.1
20- 30	10	14.1	13.6	11.4	9.9	9.2	8.4	7.8	7.2	6.2	5.2	4.2	3.0	2.3	1.1	0.6	0.5	0.1
30- 45	15	14.9	14.2	11.6	9.9	9.1	8.8	7.9	7.1	6.1	5.2	4.2	2.9	2.3	1.1	0.6	0.5	0.1
45- 60	15	16.5	15.1	12.1	10.1	9.1	8.9	8.1	7.1	5.9	5.2	4.2	2.8	2.2	1.1	0.5	0.5	0.1
60-75	15	17.9	16.0	12.7	10.7	9.4	9.2	8.2	7.2	6.1	5.2	4.0	2.8	2.3	1.1	0.5	0.5	0.1
75-95	20	17.3	16.0	13.6	11.3	10.4	9.8	8.6	7.4	6.0	5.1	4.0	2.8	2.3	1.1	0.5	0.5	0.1
95- 115	20					13.2	11.7	9.3	7.3	5.9	4.8	3.9	2.7	2.2	1.0	0.5	0.5	0.0
115- 125	10					13.7	12.4	8.8	7.0	5.7	4.5	3.7	2.6	2.1	1.0	0.5	0.5	0.0
125- 150	25					10.8	9.5	8.0	6.4	5.2	4.4	3.4	2.6	2.0	1.0	0.5	0.5	0.0
150- 175	25					8.2	7.6	6.5	5.5	4.6	3.9	3.3	2.5	1.8	1.0	0.5	0.5	0.0
175-200	25					6.4	5.8	5.4	4.9	4.2	3.7	3.0	2.3	1.8	0.8	0.5	0.5	0.0
200-225	25					5.4	4.9	4.5	4.2	3.8	3.1	2.7	2.1	1.6	0.8	0.5	0.4	0.0

Addendum 6



Fig. A6.1 Detector opening layout to calculations of access dose rate – EndCap removed on one side.

Table A6.1

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5			20.8	20.7	19.9	19.1	18.7	18.8	18.5	17.7	16.4	16.9	14.9	13.1	11.3
5- 10	5			20.8	20.8	19.9	19.1	18.6	18.9	18.5	17.8	16.4	16.9	14.9	13.1	11.3
10- 20	10			21.1	20.7	19.9	19.2	18.6	19.0	18.5	18.0	16.7	16.8	15.0	13.2	11.3
20- 30	10			21.8	21.3	20.1	19.2	18.7	19.1	18.6	18.0	17.4	16.9	15.1	13.3	11.3
30- 40	10			22.2	21.7	20.4	19.5	19.1	19.1	18.4	18.1	17.6	17.1	15.3	13.5	11.4
40- 50	10			23.0	22.2	20.6	19.5	19.8	19.1	18.5	18.3	17.7	17.2	15.5	13.6	11.6
50- 65	15			24.0	23.0	20.8	19.7	19.8	19.2	18.6	18.3	17.9	17.3	15.9	13.9	11.7
65- 80	15			24.3	23.3	20.9	19.7	19.0	19.3	18.8	18.5	18.2	17.8	16.4	14.3	12.0
80- 95	15			23.9	22.8	20.7	19.8	19.3	19.6	19.3	19.0	18.9	18.5	18.0	15.4	12.5
95- 110	15			22.7	22.2	20.8	20.3	20.2	20.9	20.6	20.2	20.2	20.0	19.7	17.5	13.6

Equivalent dose rate in the ID access scenario for T= 100 d, t= 5 d -- EndCap removed on one side

Table A6.1 (continuation)

Ec	luivale	ent dos	e rate	in the l	D access	s scenari	o for T=	= 100 d,	t= 15 c	1 E	EndCap	removed	d on on	e sid	e

	R/Z,		0- 40	40- 80	80	80-90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
	cm	dR∖dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
(0-5	5			15.0	14.9	14.5	14.0	13.8	13.3	12.9	12.3	11.7	11.4	10.7	9.3	7.7
ł	5- 10	5			15.1	15.2	14.5	14.0	13.7	13.3	12.9	12.3	11.7	11.4	10.7	9.3	7.7
	10- 20	10			15.4	15.3	14.5	14.1	13.7	13.4	13.0	12.3	11.8	11.5	10.6	9.3	7.8
1	20- 30	10			16.0	15.6	14.9	14.4	13.8	13.4	13.0	12.3	12.1	11.6	10.6	9.3	7.9
	30- 40	10			16.3	15.9	15.0	14.3	13.8	13.4	12.9	12.5	12.1	11.7	10.8	9.4	7.9
4	40- 50	10			17.1	16.3	15.3	14.7	14.0	13.4	13.0	12.6	12.3	11.9	10.9	9.5	8.0
ł	50- 65	15			17.8	16.9	15.2	14.5	14.1	13.6	13.2	12.6	12.4	12.2	11.3	9.8	8.1
(65-80	15			17.9	17.0	15.5	14.6	14.1	13.8	13.4	13.0	12.8	12.6	11.8	10.2	8.5
1	80- 95	15			17.7	16.7	15.2	14.6	14.1	14.1	13.7	13.7	13.4	13.3	12.6	10.8	8.8
9	95- 110	15			16.8	16.4	15.5	15.0	15.0	14.7	14.8	14.7	14.8	14.8	14.1	12.4	9.7

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5			12.2	12.0	11.5	11.3	10.8	10.2	9.9	9.4	9.2	9.0	8.2	6.9	6.0
5- 10	5			12.3	12.1	11.8	11.3	10.8	10.2	9.9	9.5	9.2	9.1	8.2	6.9	6.0
10- 20	10			12.4	12.2	11.8	11.4	10.8	10.1	9.9	9.5	9.2	9.1	8.2	6.9	6.0
20- 30	10			12.8	12.6	11.9	11.4	10.9	10.2	10.0	9.5	9.3	9.1	8.3	7.0	6.0
30- 40	10			13.2	12.9	12.1	11.5	11.0	10.3	10.0	9.7	9.4	9.2	8.5	7.2	6.0
40- 50	10			13.8	13.2	12.3	11.5	11.1	10.5	10.1	9.8	9.4	9.3	8.5	7.2	6.1
50- 65	15			14.5	13.8	12.5	11.6	11.2	10.6	10.2	10.0	9.8	9.5	8.7	7.4	6.2
65- 80	15			14.5	13.7	12.4	11.6	11.3	10.8	10.5	10.2	10.1	9.8	9.0	7.8	6.3
80- 95	15			14.2	13.7	12.3	11.5	11.3	11.1	10.8	10.8	10.8	10.5	9.7	8.4	6.6
95- 110	15			13.7	13.1	12.6	12.3	12.1	11.7	11.6	11.7	11.8	11.8	11.1	9.8	7.4

Table A6.1 (continuation) Equivalent dose rate in the ID access scenario for T= 100 d, t= 30 d -- EndCap removed on one side

Table A6.1 (continuation)

Eq	luivale	nt dose	e rate i	n the ID	access	scenario	o for T=	100 d, t=	: 100 d	EndCap	remove	d on one	e side

R/Z,		0- 40	40- 80	80	80-90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5			7.7	7.4	7.1	6.9	6.7	6.3	5.8	5.7	5.5	5.2	4.8	4.2	3.3
5- 10	5			7.7	7.6	7.1	7.0	6.8	6.3	5.8	5.7	5.5	5.2	4.8	4.2	3.3
10- 20	10			7.8	7.7	7.2	7.0	6.8	6.2	5.8	5.7	5.5	5.2	4.8	4.3	3.3
20- 30	10			8.0	7.9	7.5	7.3	6.9	6.3	5.9	5.7	5.5	5.3	4.8	4.3	3.3
30- 40	10			8.3	8.1	7.5	7.3	6.8	6.3	5.9	5.9	5.7	5.4	4.8	4.4	3.4
40- 50	10			8.8	8.4	7.7	7.3	6.9	6.4	6.0	6.1	5.8	5.6	4.9	4.4	3.5
50- 65	15			9.2	8.7	7.7	7.1	6.7	6.5	6.1	6.1	5.8	5.7	5.1	4.4	3.6
65- 80	15			9.3	8.9	7.7	7.3	6.8	6.3	6.3	6.1	6.0	5.8	5.3	4.5	3.7
80- 95	15			9.1	8.7	7.8	7.5	6.9	6.7	6.6	6.5	6.4	6.3	5.8	5.0	3.9
95- 110	15			8.5	8.4	7.9	7.3	7.4	7.2	7.1	7.1	7.1	6.9	6.5	5.8	4.3

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5			38.2	37.4	35.5	34.3	33.8	32.0	31.3	30.8	29.8	28.9	26.4	23.4	19.4
5- 10	5			38.3	37.8	36.0	35.0	34.2	32.1	31.2	30.9	29.5	28.9	26.5	23.4	19.5
10- 20	10			38.7	38.1	36.7	35.3	34.3	32.8	31.4	31.0	29.6	28.9	26.5	23.4	19.5
20- 30	10			39.7	39.0	36.9	35.5	34.3	33.0	32.0	31.4	30.1	28.9	26.6	23.6	19.6
30- 40	10			40.7	39.8	37.4	35.6	34.3	33.2	32.1	31.3	30.5	29.0	26.9	23.8	20.0
40- 50	10			42.5	41.1	37.6	35.8	34.5	33.1	32.1	31.4	31.0	29.5	27.6	24.0	20.2
50- 65	15			44.1	42.2	38.0	35.9	34.6	33.2	32.2	31.5	31.0	30.4	28.1	24.7	20.5
65- 80	15			44.2	42.3	37.9	35.7	34.5	33.5	32.4	32.1	31.8	31.2	29.5	25.9	21.3
80- 95	15			43.2	41.4	37.5	35.7	34.7	34.1	33.9	33.9	33.4	32.9	31.3	27.5	22.1
95- 110	15			41.4	40.3	38.2	37.2	37.0	36.5	36.3	36.3	36.5	36.3	35.0	31.5	24.3

Table A6.1 (continuation) Equivalent dose rate in the ID access scenario for T= 10 y, t= 5 d -- EndCap removed on one side

Table A6.1 (continuation)

Ec	quival	ent dos	se rate	in the I	D acces	s scenar	io for T	= 10	y, t=	15 d	I E	EndCa	p r	removed	on on	e sic	le

R/Z,		0- 40	40- 80	80	80-90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5			31.9	31.3	29.6	28.4	27.6	26.6	26.1	25.3	24.5	23.6	21.8	19.1	16.0
5- 10	5			32.1	31.7	29.7	28.4	27.6	26.6	26.1	25.3	24.6	23.6	21.8	19.1	16.0
10- 20	10			32.4	32.0	30.4	29.2	27.8	26.7	26.0	25.3	24.6	24.0	21.8	19.2	16.1
20- 30	10			33.2	32.6	30.9	29.7	28.4	27.0	25.9	25.4	24.6	24.2	21.8	19.5	16.3
30- 40	10			34.2	33.4	31.1	29.8	28.8	27.8	26.8	25.8	24.7	24.4	22.1	19.6	16.5
40- 50	10			35.7	34.6	31.5	29.9	29.0	27.8	27.0	26.4	25.0	24.5	22.7	19.8	16.8
50- 65	15			37.1	35.6	31.8	30.1	29.0	27.9	26.9	26.4	26.1	25.0	23.4	20.3	17.0
65- 80	15			37.1	35.4	31.8	29.9	28.9	28.2	27.4	26.6	26.5	26.2	24.5	21.3	17.5
80- 95	15			36.1	34.6	31.3	30.0	29.5	28.8	28.3	28.2	28.2	27.4	26.0	22.9	18.4
95- 110	15			35.2	34.2	32.5	31.5	31.3	30.9	30.5	30.3	30.7	30.5	29.3	26.3	19.9

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5			28.7	28.4	27.3	26.3	24.6	23.6	22.9	22.1	21.6	20.6	19.0	16.8	14.1
5- 10	5			28.7	28.5	27.3	26.3	25.0	23.6	22.8	22.1	21.6	20.6	19.0	16.8	14.0
10- 20	10			29.1	28.7	27.3	26.4	25.4	23.7	23.0	22.1	21.6	20.8	19.1	16.9	14.0
20- 30	10			29.7	29.3	27.6	26.4	25.6	24.2	22.9	22.1	21.8	21.3	19.2	17.0	14.2
30- 40	10			30.6	30.0	27.9	26.5	25.7	24.7	23.8	22.7	21.8	21.4	19.4	17.1	14.5
40- 50	10			32.0	30.8	28.3	26.7	25.5	24.7	24.0	23.3	22.2	21.6	19.8	17.3	14.6
50- 65	15			33.1	31.8	28.5	26.8	25.8	24.8	24.0	23.4	23.1	22.1	20.7	17.8	14.8
65- 80	15			33.2	31.5	28.3	26.8	25.7	24.9	24.1	23.7	23.6	23.1	21.6	18.7	15.1
80- 95	15			32.9	31.5	28.4	27.1	26.5	25.8	25.4	25.1	24.7	24.3	23.0	20.2	15.8
95- 110	15			31.6	30.7	29.0	28.2	27.8	27.5	27.1	27.1	27.3	27.2	25.8	23.4	17.5

Table A6.1 (continuation) Equivalent dose rate in the ID access scenario for T= 10 y, t= 30 d -- EndCap removed on one side

Table A6.1 (continuation)

Equivalent dose rate in the ID access scenario for T= 10 y, t= 100 d EndCap remove	/ed on one side
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	R/Z,		0- 40	40- 80	80	80-90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
	cm	dR∖dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
(D- 5	5			22.4	22.2	21.3	20.6	20.0	18.6	17.8	17.3	17.3	16.2	14.9	13.0	10.8
4	5- 10	5			22.6	22.2	21.3	20.6	20.0	18.6	17.8	17.3	17.2	16.1	14.9	13.0	10.8
	10- 20	10			22.9	22.6	21.7	20.8	20.1	18.9	17.7	17.2	16.9	16.3	15.1	13.0	11.0
1	20- 30	10			23.6	23.0	21.8	20.9	20.4	19.4	18.3	17.4	16.9	16.5	15.1	13.1	11.0
	30- 40	10			24.1	23.6	22.0	21.0	20.4	19.4	18.7	18.0	17.0	16.5	15.3	13.4	11.1
4	40- 50	10			25.2	24.3	22.4	21.0	20.2	19.5	18.6	18.2	17.6	16.7	15.5	13.5	11.2
!	50- 65	15			26.2	25.1	22.3	21.2	20.4	19.4	18.8	18.2	18.0	17.5	16.0	14.1	11.5
(65-80	15			26.2	24.9	22.4	20.9	20.1	19.4	18.9	18.6	18.5	18.3	16.8	14.7	11.7
ł	80- 95	15			26.4	25.3	22.8	21.6	21.1	20.5	20.0	19.9	19.7	19.1	18.0	16.0	12.4
9	95- 110	15			25.1	24.5	23.0	22.3	21.9	21.6	21.4	21.2	21.6	21.7	20.3	18.3	13.5



Fig. A6.2 Detector opening layout to calculations of access dose rate - Inner Detector removed

Table A6.2

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	10.7	10.7	10.7	10.7	10.7	10.7	10.7	11.5	11.7	11.4	10.7	11.4	10.4	9.1	8
5- 10	5	10.7	10.7	10.7	10.7	10.7	10.7	10.7	11.5	11.7	11.5	10.7	11.4	10.4	9.1	8
10- 20	10	10.7	10.7	10.7	10.7	10.7	10.7	10.7	11.6	11.7	11.7	11	11.5	10.4	9.1	8
20- 30	10	10.7	10.7	10.7	10.7	10.7	10.7	10.7	11.7	11.7	11.7	11.5	11.6	10.4	9.1	8
30- 40	10	10.7	10.7	10.7	10.7	10.7	10.7	11	11.7	11.7	11.7	11.7	11.7	10.5	9.2	8
40- 50	10	10.7	10.7	10.7	10.7	10.7	10.8	11.6	11.7	11.7	11.7	11.7	11.6	10.6	9.2	8.1
50- 65	15	10.7	10.7	10.7	10.7	10.7	10.8	11.5	11.7	11.7	11.7	11.7	11.5	10.7	9.3	8.1
65- 80	15	10.7	10.7	10.7	10.7	10.7	10.7	10.8	11.7	11.7	11.7	11.7	11.7	10.8	9.4	8.2
80- 95	15	10.7	10.7	10.7	10.7	10.7	10.7	10.7	11.6	11.7	11.7	11.7	11.7	11.6	9.6	8.2
95- 110	15	10.6	10.6	10.6	10.7	10.7	10.7	10.8	11.7	11.7	11.7	11.7	11.7	11.8	10	8.4

Equivalent dose rate in the ID access scenario for T= 100 d, t= 5 d -- Inner Detector removed

Table A6.2 (continuation)

Equivalent dose rate in the	e ID access scenario for	T= 100 d, t= 15 d	I Inner Detector removed

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	7.6	7.6	7.6	7.6	7.8	7.8	7.8	7.8	7.8	7.9	7.7	7.7	7.1	6.2	5.2
5- 10	5	7.6	7.6	7.6	7.7	7.8	7.8	7.8	7.8	7.8	7.9	7.7	7.7	7.1	6.2	5.2
10- 20	10	7.7	7.7	7.7	7.7	7.8	7.8	7.8	7.9	7.9	7.9	7.7	7.7	7.1	6.2	5.3
20- 30	10	7.7	7.7	7.7	7.7	7.8	7.8	7.8	7.9	7.9	7.8	7.8	7.8	7.1	6.2	5.3
30- 40	10	7.7	7.7	7.7	7.7	7.8	7.8	7.8	7.9	7.9	7.9	7.8	7.8	7.2	6.2	5.3
40- 50	10	7.7	7.7	7.7	7.7	7.9	7.9	7.9	7.9	7.9	8	7.9	7.8	7.3	6.2	5.3
50- 65	15	7.7	7.7	7.7	7.7	7.8	7.9	7.9	8	8	8	8	8	7.4	6.3	5.4
65- 80	15	7.7	7.7	7.7	7.7	7.8	7.9	7.9	8	8.1	8.1	8.1	8.1	7.6	6.4	5.5
80- 95	15	7.8	7.8	7.8	7.8	7.8	7.9	7.9	8.1	8.2	8.3	8.3	8.2	7.8	6.5	5.5
95- 110	15	7.8	7.8	7.8	7.8	7.9	7.9	8	8.1	8.3	8.4	8.5	8.5	8	6.8	5.6

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR∖dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	6	6	6	5.9	5.9	6	6	6	6	5.9	5.9	5.8	5.3	4.5	3.9
5- 10	5	6	6	6	6	6	6	6	6	6	6	5.9	5.9	5.3	4.5	3.9
10- 20	10	6	6	6	6	6	6	6	6	6	6	5.9	5.9	5.3	4.5	3.9
20- 30	10	6	6	6	6	6	6	6	6.1	6.1	6	5.9	5.8	5.3	4.5	3.9
30- 40	10	6	6	6	6	6	6	6	6.1	6.1	6.1	6	5.9	5.4	4.6	3.9
40- 50	10	6.1	6.1	6.1	6.1	6.1	6	6	6.1	6.2	6.2	6	5.9	5.5	4.6	3.9
50- 65	15	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.2	6.2	6.2	6	5.6	4.7	4
65- 80	15	6.1	6.1	6.1	6.1	6.1	6.1	6.2	6.2	6.2	6.3	6.3	6.2	5.7	4.8	4
80- 95	15	6.2	6.2	6.2	6.2	6.2	6.2	6.2	6.3	6.3	6.5	6.5	6.4	5.9	4.9	4
95- 110	15	6.2	6.2	6.2	6.2	6.3	6.3	6.4	6.4	6.5	6.6	6.7	6.7	6.2	5.1	4.1

Table A6.2 (continuation) Equivalent dose rate in the ID access scenario for T= 100 d, t= 30 d -- Inner Detector removed

Table A6.2 (continuation)

Equivalent dose rate in t	he ID access sce	nario for T= 100 d,	t= 100 d In	ner Detector removed

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	3.7	3.6	3.7	3.6	3.6	3.7	3.6	3.7	3.6	3.6	3.6	3.4	3.2	2.7	2.3
5- 10	5	3.7	3.7	3.7	3.7	3.6	3.7	3.7	3.7	3.6	3.6	3.6	3.4	3.2	2.7	2.3
10- 20	10	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.6	3.6	3.6	3.4	3.2	2.8	2.3
20- 30	10	3.7	3.7	3.7	3.7	3.7	3.8	3.7	3.7	3.7	3.6	3.6	3.5	3.2	2.8	2.3
30- 40	10	3.7	3.7	3.7	3.7	3.7	3.8	3.8	3.7	3.7	3.7	3.6	3.5	3.2	2.8	2.3
40- 50	10	3.7	3.7	3.7	3.7	3.7	3.8	3.8	3.8	3.8	3.8	3.7	3.6	3.2	2.8	2.4
50- 65	15	3.7	3.7	3.7	3.7	3.7	3.7	3.8	3.8	3.8	3.8	3.8	3.7	3.3	2.8	2.4
65- 80	15	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.8	3.9	3.9	3.9	3.8	3.4	2.9	2.4
80- 95	15	3.8	3.9	3.8	3.9	3.9	3.9	3.9	3.9	3.9	4	4	3.9	3.6	3.1	2.4
95- 110	15	3.9	3.9	3.9	3.9	4	4	4	4	4	4.2	4.2	4.2	3.8	3.3	2.5

													Tabl	e A6.2 (d	continua	tion)
		Εqι	uivalent	dose i	ate in tl	<u>ne ID ac</u>	cess sce	enario fo	<u>r T= 10 y</u>	<u>′, t= 5 d -</u>	<u>- Inner D</u>	etector	removed	<u> </u>		
R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR∖dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	20.4	20.4	20.4	20	19.5	19.5	20.2	19.7	20	20.3	20.1	20	18.4	16.2	13.8
5- 10	5	20.4	20.4	20.4	20.3	19.9	20.2	20.5	19.8	19.9	20.4	19.8	20	18.4	16.2	13.9
10- 20	10	20.4	20.4	20.4	20.4	20.5	20.5	20.5	20.4	20.1	20.5	19.8	20	18.4	16.2	13.9
20- 30	10	20.4	20.4	20.4	20.4	20.5	20.5	20.5	20.6	20.7	20.8	20.2	19.9	18.5	16.4	14
30- 40	10	20.4	20.4	20.4	20.4	20.5	20.5	20.5	20.6	20.7	20.7	20.6	19.9	18.7	16.4	14.2
40- 50	10	20.4	20.4	20.4	20.4	20.4	20.5	20.6	20.6	20.6	20.7	20.8	20.3	19.2	16.5	14.3
50- 65	15	20.4	20.4	20.4	20.4	20.4	20.5	20.5	20.6	20.6	20.6	20.7	20.6	19.4	16.8	14.5
65- 80	15	20.4	20.4	20.4	20.4	20.4	20.4	20.5	20.5	20.5	20.6	21	20.9	20	17.3	14.7
80- 95	15	20.3	20.3	20.3	20.3	20.4	20.4	20.4	20.7	21.2	21.6	21.7	21.4	20.6	17.9	14.9
95- 110	15	20.3	20.3	20.3	20.3	20.7	21.1	21.4	21.4	21.5	21.9	22.4	22.4	21.5	19	15.5

Table A6.2 (continuation) . _____

	Equi	valent dose	e rate in t	he ID ac	cess sce	enario for	T= 10 y	, t=	15 d	Inner	Detector	remove
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R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	17.1	17.1	17.1	16.7	16.1	16.2	16.2	16.2	16.5	16.6	16.4	15.9	15.0	13.3	11.2
5- 10	5	17.1	17.1	17.1	17.0	16.2	16.2	16.2	16.2	16.5	16.6	16.4	15.9	15.0	13.3	11.2
10- 20	10	17.1	17.1	17.1	17.1	16.9	16.8	16.3	16.3	16.4	16.5	16.4	16.3	15.0	13.4	11.2
20- 30	10	17.1	17.1	17.1	17.1	17.1	17.2	16.9	16.5	16.4	16.5	16.5	16.6	15.0	13.4	11.3
30- 40	10	17.1	17.1	17.1	17.1	17.1	17.2	17.2	17.3	17.1	16.9	16.5	16.6	15.1	13.5	11.4
40- 50	10	17.1	17.1	17.1	17.1	17.1	17.2	17.2	17.3	17.3	17.4	16.7	16.6	15.4	13.5	11.6
50- 65	15	17.1	17.1	17.1	17.1	17.1	17.2	17.2	17.2	17.3	17.3	17.3	16.9	15.9	13.7	11.6
65- 80	15	17.0	17.0	17.0	17.1	17.1	17.1	17.1	17.2	17.2	17.3	17.4	17.4	16.3	14.1	11.9
80- 95	15	17.0	17.0	17.0	17.0	17.0	17.2	17.4	17.4	17.7	18.0	18.1	17.8	16.9	14.7	12.1
95- 110	15	17.7	17.7	17.7	17.7	18.0	18.0	18.0	18.1	18.1	18.3	18.8	18.7	17.8	15.7	12.5

Table A6.2 (continuation)

R/Z,		0- 40	40- 80	80	80- 90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	15.1	15.1	15.1	15.1	15.1	15.1	14.2	14.2	14.5	14.5	14.4	13.9	13.0	11.5	9.8
5- 10	5	15.1	15.1	15.1	15.1	15.1	15.1	14.6	14.2	14.4	14.5	14.4	13.9	13.0	11.5	9.7
10- 20	10	15.1	15.1	15.1	15.1	15.1	15.1	15.1	14.3	14.4	14.5	14.4	14.1	13.0	11.5	9.7
20- 30	10	15.1	15.1	15.1	15.1	15.1	15.1	15.2	14.8	14.4	14.4	14.5	14.5	13.0	11.6	9.9
30- 40	10	15.1	15.1	15.1	15.1	15.1	15.1	15.2	15.3	15.3	14.9	14.5	14.6	13.2	11.6	10.0
40- 50	10	15.0	15.0	15.0	15.0	15.1	15.1	15.2	15.2	15.3	15.3	14.6	14.6	13.4	11.7	10.0
50- 65	15	15.0	15.0	15.0	15.0	15.1	15.1	15.2	15.2	15.2	15.3	15.3	14.8	14.0	11.9	10.1
65- 80	15	15.0	15.0	15.0	15.0	15.0	15.1	15.1	15.1	15.2	15.2	15.4	15.4	14.3	12.4	10.3
80- 95	15	15.5	15.5	15.5	15.5	15.5	15.6	15.7	15.8	15.8	15.9	16.0	15.8	14.9	12.9	10.5
95- 110	15	15.9	15.9	15.9	15.9	15.9	16.0	16.0	16.0	16.1	16.4	16.8	16.7	15.7	14.0	11.0

Equivalent dose rate in the ID access scenario for T= 10 y, t= 30 d -- Inner Detector removed

Table A6.2 (continuation)

Equiv	/alent of	dose ra	ate in th	e ID aco	cess scer	hario for	T= 10 y	, t= 100	d	Inner	Detector	remove	d

R/Z,		0- 40	40- 80	80	80-90	90- 100	100- 110	110- 120	120- 140	140- 160	160- 180	180- 200	200- 240	240- 280	280- 320	320- 360
cm	dR\dZ	40	40	0	10	10	10	10	20	20	20	20	40	40	40	40
0- 5	5	12.0	12.0	12.0	12.0	12.0	12.0	12.0	11.5	11.3	11.4	11.7	11.1	10.4	9.2	7.7
5- 10	5	12.0	12.0	12.0	12.0	12.0	12.0	12.0	11.5	11.3	11.4	11.6	11.1	10.4	9.2	7.7
10- 20	10	12.0	12.0	12.0	12.0	12.0	12.0	12.0	11.7	11.2	11.3	11.2	11.3	10.5	9.2	7.9
20- 30	10	12.0	12.0	12.0	12.0	12.0	12.0	12.0	12.1	11.8	11.5	11.3	11.4	10.5	9.2	7.9
30- 40	10	11.9	11.9	11.9	11.9	12.0	12.0	12.1	12.1	12.2	12.0	11.3	11.4	10.6	9.3	8.0
40- 50	10	11.9	11.9	11.9	11.9	12.0	12.0	12.1	12.1	12.1	12.2	11.8	11.4	10.8	9.4	8.0
50- 65	15	11.9	11.9	11.9	11.9	11.9	12.0	12.0	12.1	12.1	12.1	12.2	11.9	11.0	9.7	8.2
65- 80	15	11.9	11.9	11.9	11.9	11.9	11.9	12.0	12.0	12.0	12.1	12.2	12.3	11.4	10.0	8.3
80- 95	15	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.8	12.8	12.9	12.9	12.6	11.9	10.6	8.6
95- 110	15	12.8	12.8	12.8	12.8	12.8	12.8	12.9	12.9	13.0	13.1	13.5	13.6	12.8	11.5	8.9